

MULGA ROCK URANIUM PROJECT

RESULTS OF HYDROGEOLOGICAL INVESTIGATIONS AND NUMERICAL MODELLING, MULGA ROCK URANIUM PROJECT

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VERSION	AUTHOR	REVIEW	ISSUED
15-002	PHW	JRP	19/05/2015
15-002a	PHW	JRP	29/05/2015
15-002b	PHW	JRP	4/06/2015
15-002c	MJT		23/10/2015
15-002d	MJT		29/10/2015

1 INTRODUCTION

The Mulga Rock Uranium Project (MRUP) lies approximately 240km east-north-east of Kalgoorlie-Boulder in the Shire of Menzies (Figure 1). The area is remote, located on the western flank of the Great Victoria Desert, comprising a series of large, generally parallel sand dunes, with inter-dunal swales and broad flat plains.

Access to the Project area is limited and is only possible using four-wheel-drive vehicles. The nearest residential town to the Project is Laverton which lies approximately 200km to the north-west. Other regional residential communities include Pinjin Station homestead located approximately 100km to the west, Coonana Aboriginal community situated approximately 130km to the south-south-west, Kanandah Station homestead positioned approximately 150km to the south-east and the Tropicana Gold Mine lying approximately 110km to the north-east of the Project (Figure 2).

The MRUP covers approximately 102,000 hectares on granted mining tenure (primarily M39/1080 and M39/1081) within Unallocated Crown Land. It includes two distinct mining centres, Mulga Rock East (MRE) comprising the Princess and Ambassador resources, and Mulga Rock West (MRW) comprising the Emperor and Shogun resources, which are approximately 20km apart (Figure 3). MRE contains over 65% of the total recoverable uranium and is of a higher grade than MRW. Mining will commence at MRE, which will include the location of the processing plant. Up to 4.5 Million tonnes per annum (Mtpa) of ore will be mined using traditional open cut techniques, crushed, beneficiated and then processed at an acid leach and precipitation treatment plant to produce, on average, 1,360 tonnes of uranium oxide concentrate (UOC) per year over the life of the Project. The anticipated Life-of-Mine (LOM) is up to 16 years, based on the currently identified resource.

This report presents the results of geological and hydrogeological investigations in the planned mining area, as well as numerical modelling to determine dewatering pumping rates and the potential impacts of groundwater reinjection, to support an application to the Department of Water (DoW) for licences to take and reinject water. The model can also be used to assess the impacts of tailings disposal.

2 PREVIOUS INVESTIGATIONS

There are many publications describing palaeodrainages and palaeochannel aquifers in Western Australia such as the one that hosts the Mulga Rock deposits. These include Van der Graaff *et al.* (1977); de Broekert and Sandiford (2005); Magee (2009); and English *et al.* (2012).

GRC (1984) reviewed all available data for PNC Exploration Pty Ltd (PNC) which held the Mulga Rock Uranium Project then, and carried out hydrogeological assessments for the mine water supply, dewatering of the Emperor, Shogun and Ambassador deposits, and potential environmental impacts.

Following the above study, a programme of drilling, bore construction and test-pumping was completed, and a reconnaissance was made for a source of low-salinity water (GRC, 1985). Six additional sites were drilled to explore for low-salinity water (GRC, 1986), but with little success.

Douglas *et. al.* (1993) completed a detailed investigation of the hydrochemistry of groundwater from the Ambassador deposit as well as the chemistry and mineralogy of the lignite.

Rockwater (2010, and 2013) conducted dewatering and water-supply investigations for the MRUP. This report updates and expands the information contained in those reports. Rockwater (2015) prepared a separate report on the planned low-salinity (Kakarook North) borefield.

3 HYDROGEOLOGICAL SETTING

3.1 CLIMATE

The MRUP is located in the Great Victoria Desert and has an arid climate with hot dry summers and cool to mild winters. The nearest long-term climate station is at Edjudina (BoM Station 012027), 145 km to the west of the Ambassador deposit. Average rainfall data for the station (1900 to 2014) are given in Table 1.

Table 1: Average Monthly Rainfall (mm) Edjudina (BoM Station 012027)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
22.4	28.2	26.1	19.6	22.0	22.1	19.2	16.7	9.7	11.8	14.0	12.8	222.6

Most of the rain falls in irregular thunderstorm events or during the passage of the remnants of cyclones, with some frontal systems in winter. Daily rainfalls have been up to 98 mm (in February). No other climate data are available for the station.

The MRUP has maintained climate stations at the airstrip and at the Emperor and Shogun deposits since March 2009. A suite of climatic measurements has been made including rainfall, maximum and minimum air temperature, and pan evaporation.

Rainfall at the MRUP airstrip from 2010 to November 2014 can be compared with those at Edjudina in Table 2.

Table 2: Comparison of Annual Rainfall, Edjudina and Mulga Rock Airstrip

Year	Total Rainfall (mm)	
	Edjudina	Mulga Rock Airstrip
2010	222	173
2011	503	433
2012	337	129
2013	284	170
2014 to Nov.	469	160

The comparison in annual rainfall amounts over the period shown in Table 2 suggests that the climate at the MRUP is substantially drier than at Edjudina. Monthly rainfall data for the three MRUP climate stations are shown in Table 3. These also show a general decrease in rainfall from west (Emperor) to east (Airstrip).

Pan evaporation at the MRUP airstrip station from Dec-13 to Nov-14 was significantly lower than the average for Kalgoorlie (Luke, Burke and O'Brien, 1988), as shown in Table 4.

Table 3: Monthly Rainfall (mm) at the MRUP Climate Stations

Month	Airstrip					Emperor					Shogun				
	2010	2011	2012	2013	2014	2010	2011	2012	2013	2014	2010	2011	2012	2013	2014
January	9.3	58.7	23.6	15.2	65.7	0	108.2	55.4	20.8	128.8	3	105.8	62.6	15.2	116.6
February	10.3	191.3	13.7	7.5	31.3	12.6	252.4	23	3.8	51.8	15	247.4	21.6	10.2	49.2
March	5.9	9.3	20.7	36.6	3.3	3.6	17	47.4	70	11.8	11.2	18.2	48.8	58.2	12.2
April	31.3	20.3	0.7	8.6	0.9	38.2	28.8	0.2	14.6	21.4	53	33.8	0.2	16.6	12
May	8	11.2	2.6	18.7	17.2	7.3	17.4	2.6	18.2	38.4	9.1	19.8	3	31	31.6
June	7.8	57.2	6.9	4.5	4.6	7.8	85.2	10	5.8	6.6	9.6	82.2	13.2	7.2	7.2
July	8.8	21	2.1	8.1	2.5	13.2	38.4	2.4	14.7	4	12	36.2	3.4	13	4
August	55.1	1.9	0.6	2.1	0.4	86.8	3	1.4	3.4	1.2	79.2	3	0.8	1.8	1.2
September	27.4	2.1	0.6	5.8	5.1	36.4	5.6	1	13.2	7.6	36.2	4	0.8	10	6.8
October	1.5	36.7	3.8	0.9	9	0.6	61.4	9.4	1.2	19.2	1.8	59.2	6.4	2.8	17.4
November	1.9	12.2	35.1	47.9	21.6	2	24.4	48	65.4	30	1	24.2	50.8	57.2	32
December	7.7	12.7	17.5	15	N/A	7.4	28.8	53.8	16.8	N/A	9	22.8	28.4	16	N/A
Annual Total	175	434.6	127.9	170.9	161.6	215.9	670.6	254.6	247.9	320.8	240.1	656.6	240	239.2	290.2

Table 4: Comparison between Average Pan Evaporation at Kalgoorlie and the MRUP (2014)

	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Year
MRUP (2014)	306	280	225	211	150	91	81	90	140	206	255	276	2309
Kalgoorlie (Av.)	431	346	306	199	133	93	103	130	181	271	326	424	2943

Maximum and minimum air temperatures at the three MRUP weather stations are shown with monthly rainfalls in Figure 4. The temperatures are very similar at all three stations. In 2014, average maximum air temperatures ranged from 18.6 °C in June to 34.6 °C in January; and average minimum temperatures ranged from 1.1 °C in July to 18.0 °C in January.

3.2 REGIONAL GEOLOGICAL SETTING

Mineral exploration holes drilled by Vimy and its predecessor PNC, as well as other companies including Uranerz and Paladin, have shown that the Mulga Rock palaeodrainage is about 8 to 10km wide. The eastern arm of the palaeochannel is probably continuous over a length of at least 65 km, and is interpreted in plans and sections in Uranerz (1986) to be hydraulically connected to a trunk palaeochannel that follows Ponton Creek to the south and is downstream of the confluence of the Lake Raeside, Lake Rebecca and Roe palaeochannels (Fig. 5).

The palaeodrainage skirts a southerly extension of the Gunbarrel Basin, which contains sediments of Carboniferous to Pleistocene age, and is bounded by crystalline rocks of the Yilgarn Craton of Archaean age to the west and the Albany Fraser Province of Proterozoic age to the east (Fig. 5).

3.3 LOCAL GEOLOGY

The geology of the eastern part of the MRUP, from information provided by Vimy, can be summarised as follows.

Ambassador is a sediment-hosted uranium deposit. This deposit, together with the other MRUP deposits, occurs within the Narnoo Basin, a local name for the host structure. The mineralisation is primarily in geochemically reduced sediments of Eocene age, preserved within a complex set of sedimentary troughs overlying an extensive paleodrainage referred to as the Mulga Rock palaeochannel, which is probably an isolated oxbow channel of the Lake Raeside regional paleodrainage.

The reduced sediments that contain the Ambassador and other deposits are part of a sedimentary package named the Narnoo Basin Sequence. This sequence consists of multiple fining-upwards units including sandstone, claystone (typically carbonaceous) and lignite which were deposited in alluvial and lacustrine environments.

Sedimentation within the Eocene palaeochannel is interpreted as a transgressive sequence. The lowest part of the sequence is dominated by medium to coarse, marginally carbonaceous sands. These sands are mostly devoid of clay and are highly transmissive to groundwater flow. The central portion of the sequence is dominated by fine textured, organic-rich sediments (highly carbonaceous fine sands, lignitic clays and lignite) containing humic macerals of low reflectance (huminite). These fine textured, sediments occur at and near the maximum flooding surface of the transgression. The upper portion of the sediments are dominated by stacked beds of reverse graded (upward coarsening) sands that represent the progradational portion of the transgression.

The main sequence of Late Eocene lacustrine sediments correlates regionally with the third-order transgressive sequences of the Tortachilla cycle (~39 Ma) whilst the youngest Late Eocene sediment correlates with the Tuketja (~36 Ma) transgressive cycle.

Cretaceous sediments are dominant in the north-eastern part of the Ambassador deposit and also occur around the deposit margins. Although superficially similar to the late-Eocene palaeochannel sediments, they do not have the regular transgressive sequence of the later sediments and are characterised by beds of black, mature forms of carbonaceous material such as inertinite and glassy vitrinite. The Cretaceous sediments are probably remnants of a formerly deeply buried sequence that covered much of southern Australia prior to the Late Cretaceous (Albian-Maastrichtian) uplift.

Overlying the Narnoo Basin Sequence is a succession of oxidised sediments which at Ambassador are about 36 to 55 m thick. Pre-Cretaceous and Eocene basement in the Ambassador area consists of a Carboniferous sedimentary succession, as well as Paleoproterozoic metasediments to the east of the Gunbarrel fault. The Carboniferous sediments are assigned to the Paterson Formation and understood to be part of the Gunbarrel Basin.

Mineralisation is believed to have formed via biogenic processes, through the fixation of metals in solution that were mobilised in the course of repeated weathering episodes, resulting in the leaching of the upper part of the Eocene and thick sections of Cretaceous sediments up-gradient of the deposits. This weathering is akin to acid-sulphate weathering processes, oxidising sulphides and organic matter and organic carbon resulting in very aggressive groundwater conditions (low pH and elevated temperature), and thereby mobilising metals and metalloids (including silica) from the overburden. The remnant, highly altered material is typically strongly bleached and characterised by a kaolinite fraction of notably high crystallinity (due to dissolution and recrystallisation of the clay).

The uranium mineralisation is assumed to be similar in nature to that studied at Ambassador via multiple recent spectral, mineralogical, deportment and metallurgical studies, showing that the bulk of the uranium is in a hexavalent ionic state and adsorbed onto organic matter, with a negligible fraction contained in refractory minerals.

Similarly, the majority of base metals in the deposits are expected to be bound to organic matter, with a significant fraction in sulphate phases and a lesser fraction in supergene sulphide phases.

3.4 HYDROGEOLOGY

The water table at the Ambassador deposit is 29 m to 49 m deep, and generally lies within fine-grained, carbonaceous sediments of Eocene age; and in the north-east, of Cretaceous age. The mineralised zones are mainly just below the water table, but some extend down into the coarse-grained sediments towards the base of the palaeochannel (see the geological sections in Appendix I).

Reduced groundwater levels within the palaeochannel that have been measured at various times are shown in Fig. 6, with values shown for representative bores that were used to calibrate the groundwater model described in Section 5 below. They show that in most of the Narnoo Basin/paleochannel the water table is very flat, at an elevation of about 288 to 290 m AHD, and that there is very little flow into the basin (or recharge) and out of the basin (discharge). Hydraulic gradients suggest there is minor flow into the basin from the north-eastern tributary that includes the Ambassador deposit; and a small component of flow into the basin from the north-west.

Limited data suggest there is flow from north to south in the western arm under a low hydraulic gradient. There is also indicated to be flow to the south in the eastern arm, south of about 6655000 mN – the steeper hydraulic gradient there is attributed to a narrowing of the channel containing coarse-grained sediments and lower transmissivity as indicated by Uranerz Section 92,500 N, which is at about 6655700 mN (GDA) (Appendix I). There, much of the channel is filled with fine-grained sediments.

Water-level measurements taken in April 2014 in the Ambassador area (Fig. 7) show that the water table is very flat in Ambassador East at about 299 m AHD; and with a low hydraulic gradient from 291 m to 293 m AHD in Ambassador West. There is a relatively steep gradient between these two parts of Ambassador due to the presence of a high of Permian sediments separating the Eocene sediments in each area. This is shown by the Long Section N30 in Appendix I.

Seasonal and annual water-level variations are very small, showing there is very little recharge to the aquifer and no extraction or significant flow out of the basin. Groundwater levels were monitored every one to three months in 38 bores in the Ambassador area from 2010 to 2014. Most of the August 2012 measurements were in error, presumably due to a faulty probe. Without those measurements, the range in water-level fluctuations in the bores was from 0.05 m to 0.76 m, and averaged 0.25 m. The higher ranges probably included some measurement errors and the impacts of pumping for sampling, and so the actual range and average would have been lower.

The results of pumping tests of three bores screened in the basal Eocene palaeochannel sediments (Section 4) indicate that these sediments are moderately to highly permeable, with

hydraulic conductivities ranging from 9 to 140 m/d. The low value is typical of these sediments where tested elsewhere in the Eastern Goldfields. The high values at bores NWB1 and 2 in the planned injection area reflect the local gravels screened by the bores. Hydrogeological sections through these bores are presented in Figs 8 and 9. The section lines are shown in Fig. 6.

The fine-grained sediments higher in the palaeochannel, generally associated with the mineralised zones, will have low hydraulic conductivity as shown by the results of slug tests (Section 4.3).

The groundwater is unconfined at the water table, but confined below by the fine-grained sediments above and within the basal sands and gravels.

3.5 GROUNDWATER CHEMISTRY

Douglas *et. al.* (1993) concluded that groundwater at the MRUP differs from that in other Yilgarn palaeochannels, having low oxidation potentials with anomalous isotope effects and low concentrations of a number of trace elements. All of these differences were attributed to the high organic content of sediments at the site. They also noted that groundwater at Ambassador, in a tributary palaeochannel, is geochemically distinct from that in the main palaeochannel, which includes the Emperor and Shogun deposits. The main palaeochannel contains groundwater that is more saline, depleted in K, Ca and Sr, and enriched in Al, Fe and Mn relative to Ambassador. Conversely, Ambassador groundwater is significantly enriched in dissolved HCO_3 , PO_4 , Ba, U and W; and is depleted in dissolved Si. This is consistent with younger groundwater flowing down the Ambassador channel into the main palaeochannel system.

Douglas *et. al.* (1993) also state that the geochemistry of groundwater in the Ambassador mineralized zone may relate to interactions between groundwater and solid organic matter, and/or the inflow of water from a different source. The latter possibility is supported by the lower salinity at Ambassador.

The chemistry of water samples taken from each of the project areas is discussed below. Salinities are shown in Fig. 10, pH in Fig. 11, and a trilinear (Piper) diagram showing major ion composition is given in Fig. 12. Water from all the MRUP deposits is of similar ionic composition (Fig. 12), although the water from Ambassador tends to have proportionately higher sodium and chloride and lower magnesium and sulphate than water from some of the other deposits.

3.5.1 Ambassador/Princess

Water samples have been analysed at various times for different suites of parameters from 97 drillholes in total at the Ambassador and Princess deposits. The results of all the analyses are given in Appendix II, and the results from some of the separate sampling events for the Ambassador deposit are described below.

1984 to 1991 Samples

Water samples collected from Bores 1 and 7 at the end of pumping tests in 1984 were analysed for major components (GRC, 1985). Water samples airlifted from 13 drillholes in and near the Ambassador deposit in 1990 and 1991 were also analysed for major components as well as a wide range of metals and rare earth elements (Douglas *et. al.* 1993).

The results of the major component analyses and some other common elements are given in Table 5.

The analyses show that the water ranges in salinity from 7,500 to 37,600 mg/L TDS. It is moderately acidic to neutral with pH ranging from 4.3 to 7.0 (generally 5.5 to 6.6); and is of a sodium chloride type with elevated magnesium and sulphate. Metals and other elements that were analysed for (most are not shown in Table 5) were generally at low concentrations. Exceptions were moderate concentrations of iron in several holes (up to 16 mg/L); and high bromine concentrations (up to 23 mg/L). Uranium concentrations were mostly below the limit of detection (0.002 mg/L), with a maximum of 0.038 mg/L.

Oxidation potentials (Eh) range from -167 to 335 mV and are generally greater than 100 mV indicating potentially oxidising conditions. It is likely that the low pH in hole CD1515 resulted from oxidation of sulphides, and increased rates of oxidation will almost certainly occur when the lignite is dewatered.

The areal distribution of the salinity data for all the deposits and sampling programmes is shown in Figure 10. Salinity increases to the south-west in the direction of groundwater flow, mostly from 20,000 to 40,000 mg/L TDS. Salinity also tends to increase with sample depth with moderate correlation, although the main water-bearing zones in each hole have not been identified.

Two holes, CD1366 and CD1409, had much lower salinities than in the other holes. Douglas *et. al.* (1993) consider that this resulted from contamination with rainwater in CD1366; and CD1409 has a high bicarbonate concentration and low sulphate that suggests that the water is young and that there is a high rate of recharge from rainfall/runoff.

Table 5: Results of Major Component Analyses (and Common Metals) 1984

Hole/Bore	pH	Eh (mV)	TDS (mg/L)	Na (mg/L)	K (mg/L)	Ca (mg/L)	Mg (mg/L)	Cl (mg/L)	HCO3 (mg/L)	SO4 (mg/L)	NO3 (mg/L)	Fe (mg/L)	Mn (mg/L)	Br (mg/L)	Sr (mg/L)	Si (mg/L)
Bore 1	6.5	ND	37,609	11,100	260	800	1,400	19,800	89	4,150	10	12.8	ND	ND	ND	ND
RC1148	5.98	129	22,678	6,800	248	532	742	11,800	86	2,490	ND	0.4	0.2	23.1	6.9	21
Bore 7	5.8	ND	36,771	11,000	250	770	1,280	19,600	10	3,850	11	16.2	ND	ND	ND	ND
RC1213	5.46	148	12,506	3,769	138	246	350	6,730	24	1,250	ND	0.46	0.22	10.6	3.3	21
RC1152	5.91	143	19,522	5,645	231	450	700	10,400	30	2,060	ND	0.15	0.13	20.7	6.3	22
RC1151	6.36	144	14,784	4,392	169	319	467	7,810	104	1,560	ND	0.88	0.24	15	4	15.4
RC1419	6.85	173	14,535	4,185	204	300	522	7,430	283	1,730	ND	6.3	0.05	20.3	3.4	6.3
CD1500	6.01	293	18,459	5,276	207	415	651	9,820	107	2,020	ND	1.02	0.27	16.6	4.1	4
CD1498	6.58	335	32,875	9,646	383	858	1,176	16,600	303	4,040	ND	0	0.06	23.3	11.6	7.6
CD1247	7.01	213	26,887	7,939	308	626	856	14,000	382	2,950	ND	0.19	0.05	20.4	5.1	4.6
CD1515	4.27	147	35,984	11,278	250	708	1,212	19,000	0	3,520	ND	0.18	1.34	14.7	7.9	2.8
RC1216	6.45	9	25,376	7,717	249	515	681	13,400	339	2,630	ND	5.1	0.17	13	4.1	1.6
RC1177	6.58	171	27,343	8,236	263	683	754	14,200	191	3,090	ND	7.8	0.28	15.1	5.9	3.2
CD1409	6.58	-167	7,519	2,285	66	174	262	4,070	1,231	56	ND	0.22	0.6	3.3	1.7	2.9
CD1366	6.46	80	8,461	2,271	84	461	290	4,210	ND	1,140	ND	0.34	0.32	4.9	2.2	4.6

Samples from 2010 to 2014

Water samples were airlifted from 10 holes in the Ambassador deposit in March 2010 and analysed for major components and a range of other elements and metals (Table 6). Many other holes in the area were sampled in 2012 to 2014 (Appendix II). The results are similar to the 1984 analyses, with salinity ranging from 700 to 80,000 mg/L TDS; pH 3.0 to 8.0; and Fe <0.2 to 56 mg/L. Salinities within the Princess and Ambassador deposits generally range from 20,000 to 30,000 mg/L TDS. Most of the higher salinities, around 60,000 mg/L TDS, are for drillholes about 5 km west of Ambassador but are included with the Ambassador data here.

Minor elements and metals other than iron that were analysed for were generally at low concentrations or below the limits of detection, including uranium. There were some elevated metal concentrations in holes that had low pH. Bromine concentrations ranged from 3 to 23 mg/L; and strontium 2 to 12 mg/L.

Water samples taken from the Princess deposit have been measured in the field in 2012 and 2013 for salinity and pH. The water is acidic, with pH generally ranging from 5.0 to 6.5. Lower pHs of around 3 have been measured in one hole, NNA5623. Salinities are lower than most at Ambassador, ranging from 8,700 to 21,400 mg/L TDS, as the deposit is up-gradient of Ambassador.

3.5.2 Emperor and Shogun Deposits

Water samples have been collected and analysed from 161 drillholes in these deposits, mostly in 1984 and 2012.

Groundwater salinity at Emperor and Shogun ranged from 13,000 to 139,700 mg/L TDS (GRC, 1984) with the highest salinities in the south, and the lowest salinities towards the margins of the palaeochannel to the north or west (Fig. 10) suggesting possible recharge in these areas of less-saline water. The salinity increases with depth, and is generally more saline than at the Ambassador deposit.

The water from the bores at Emperor and Shogun is more acidic than at Ambassador, with pH of 3.8 to 5.0. It is of sodium chloride type with moderately high magnesium and sulphate concentrations.

The Piper trilinear diagram indicates that the portions of the major ions are similar to seawater (Fig. 12). Of the water samples collected from drillholes in 2012 to 2014 (Appendix II) many had low pH in the range 3 to 4 (minimum 2.9 and maximum 6.2), and salinity ranging from 6,100 to 95,500 mg/L TDS. Most salinities are greater than 50,000 mg/L TDS.

Table 6: Results of Major Component Analyses (and Other Elements and Metals) 2010

Hole/Bore Hole/Sample Depth Date Analysed	Units	NNA5027 82 26/03/2010	NNA5198 64 26/03/2010	NNA5393 73 26/03/2010	NNA5127 65 26/03/2010	NNA5140 51 26/03/2010	NNA5086 75 26/03/2010	NNA5103 66 26/03/2010	NNA5199 55 26/03/2010	NNA5155 51 26/03/2010	NNA5107 69 26/03/2010
pH	pH Units	4.1	3.5	4.2	5.5	6.4	6.8	4.3	4.2	6.7	4.8
Conductivity @25°C	µS/cm	17780	23060	31200	31400	27420	47800	41700	45000	28390	44700
TDS (Calculated)	mg/L	10668	13836	18720	18840	16452	28680	25020	27000	17034	26820
Soluble Iron, Fe	mg/L	0.844	50.813	6.526	0.203	<0.2	<0.2	0.76	5.885	<0.2	<0.2
Sodium, Na	mg/L	3038	4116	5748	5710	4898	8651	7602	8197	5087	8130
Potassium, K	mg/L	101	128	185	187	171	349	257	316	180	292
Calcium, Ca	mg/L	197	274	416	463	357	604	580	614	362	620
Magnesium, Mg	mg/L	301	336	548	531	422	900	772	833	488	834
Chloride, Cl	mg/L	5311	7558	11235	10922	8689	17219	13693	16462	9677	15717
Carbonate, CO ₃	mg/L	<1	<1	<1	<1	<1	<1	<1	<1	<1	<1
Bicarbonate, HCO ₃	mg/L	<5	<5	<5	49	9	32	<5	<5	31	<5
Sulphate, SO ₄	mg/L	1355	1633	2237	2227	1751	3317	2875	3273	1827	3553
Nitrate, NO ₃	mg/L	0.35	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Cation/Anion balance	%	-2.5	-5	-6.3	-5.2	-2.1	-6.3	-1.9	-6.9	-4.6	-5.8
Sum of Ions (calc.)	mg/L	10303	14045	20368	20089	16297	31071	25778	29695	17652	29147
Soluble Arsenic, As	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Boron, B	mg/L	1.252	1.011	1.611	1.409	1.208	2.712	1.722	2.126	1.352	1.688
Soluble Barium, Ba	mg/L	0.038	0.052	0.035	0.055	0.07	0.051	0.066	0.094	0.053	0.067
Soluble Beryllium, Be	mg/L	<0.005	0.02	0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Cadmium, Cd	mg/L	<0.0005	0.001	0.003	0.024	0.0009	0.007	0.013	<0.001	<0.0005	0.319
Soluble Chromium, Cr	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	0.013	<0.01	<0.005	<0.01
Soluble Copper, Cu	mg/L	0.032	0.021	0.018	0.013	0.024	0.018	0.628	0.016	0.005	1.904
Soluble Cobalt, Co	mg/L	0.075	0.719	1.052	0.625	0.148	0.199	3.958	0.653	0.026	2.292
Soluble Lead, Pb	mg/L	0.015	0.041	<0.005	<0.005	0.006	<0.01	0.345	<0.01	<0.005	3.077
Soluble Molybdenum, Mo	mg/L	<0.005	<0.005	<0.005	0.012	0.035	<0.01	<0.01	<0.01	0.008	<0.01
Soluble Manganese, Mn	mg/L	3.208	1.367	1.021	1.246	0.532	1.964	1.608	1.299	0.562	2.345
Soluble Nickel, Ni	mg/L	0.055	1.153	1.888	0.627	0.181	0.377	3.83	1.719	0.023	2.905
Antimony, Sb	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Tin, Sn	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Selenium, Se	mg/L	<0.005	0.007	<0.005	0.009	<0.005	<0.01	0.104	<0.01	<0.005	<0.01
Soluble Zinc, Zn	mg/L	0.08	6.647	3.252	0.266	0.162	0.918	5.256	7.779	0.074	12.888
Soluble Uranium	mg/L	<0.005	<0.005	0.028	0.032	<0.005	<0.01	0.019	<0.01	<0.005	0.068
Vanadium	mg/L	<0.005	<0.005	<0.005	<0.005	0.009	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Mercury, Hg	mg/L	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001	<0.0001

Iron concentrations range from <0.05 mg/L to 55 mg/L in recent samples (below the limit of reporting in 2014) and up to 190 mg/L in the 1984 samples. Prior to 2014, bromine (four analyses) ranged from 23 to 71 mg/L; and strontium 7.7 and 8.8 mg/L (two samples). In 2014 these elements were below the limit of reporting in all seven samples analysed. Other elements and metals that were analysed were at low levels or below levels of detection. Uranium was above the level of detection in five samples, with one high value (0.35 mg/L) from the Shogun costean in 1983. One sample from drillhole MSW002 had an anomalously high zinc concentration (26 mg/L) in May 2012, but was low (0.76 mg/L) in the October 2012 sample.

3.5.3 ReInjection Area

Water samples were analysed from 17 bores in the ReInjection Area in 2014 and 2015 – with two to four samples analysed from 12 of the bores. The results are included in Appendix II.

The water is moderately acidic, with pH ranging from 4.0 to 6.9, and is generally between 4.5 and 5.0. It is of a sodium chloride type, with relatively high magnesium and sulphate concentrations. Salinity ranges from 20,000 to 73,000 mg/L TDS and averages 51,500 mg/L TDS; generally significantly higher than for groundwater in the Ambassador/Princess area.

There is a good correlation between sample depth and salinity (Fig. 13). Seepage from in-pit tailings will infiltrate to shallow groundwater of similar salinity to that at the Ambassador deposit. The zone where any seepage would reach the water table includes reactive carbon-rich layers that will tend to fix any metals in the leachate.

Where analysed, metals and trace elements in groundwater in the injection area were at low levels or below the limits of reporting. There were some elevated boron concentrations of 4.2 to 7.2 mg/L in seven of the bores.

4 BORE CONSTRUCTION AND PUMPING TESTS

Many mineral exploration holes and holes drilled to delineate the deposits have been cased with 50 mm uPVC casing and are used for groundwater-level and water quality monitoring. In addition, a number of production bores have been drilled in the project area for potable and process water supply, dewatering testing, and for road construction. These are described below and production bore locations are shown in Figure 14.

4.1 DRILLING AND BORE CONSTRUCTION

GRC (1985) supervised the construction and testing of seven bores (MRWB1–7) in the project area for PNC in 1984; four of these were low-yielding, including MRWB5 which was used to determine the vertical permeability of sediments beneath the mineralised zone at Shogun. Details of that bore and the higher-yielding bores are given in Table 7.

Bore MRWB6 near the Emperor deposit has collapsed, and was replaced by two bores MSWB02 and 03 constructed to provide water for road construction (MWES, 2011) for the Tropicana Gold Project.

Bores NWB1 and NWB2 were constructed as test-injection bores, south of the Ambassador deposit in the palaeochannel sediments. Construction details and logs for these bores are given in Appendix III.

Table 7: Summary of Production Bore Details

Bore	mE	mN	RLGL	Date Drilled	TD (mbgl)	Casing	Screened Interval (m)	Aquifer Depth	SWL (mbtc)	TDS
	(MGA)		mAHD							(mg/L)
MRWB4	557595	6691810		1984	71	130 mm uPVC	63-67.5	45.5-71	31.9	69,500
MRWB5	563440	6687600		1984	67	195 mm uPVC	44.2-46.2	44-62	30.2	59,100
MRWB6	557176	6690643	316	1984	74.5	195mm uPVC	58.5-70.5m	56-70.5	27.9	89,300
MRWB7	575480	6679975		1984	100	195 mm uPVC	68.5-92.5	65-97.5	34.0	36,800
MSWB02	557225	6690545	316	2011	72	155mm uPVC	54-72m	54-72m	28.3	90,000
MSWB03	556958	6690702	317	2011	78	155mm uPVC	54-76m	54-76m	29.1	91,000
NWB1	575552	6671190	328.2	2015	108	155 mm uPVC	36-42; 66-102	60-104	40.0	58,000
NWB2	575363	6670210	346.1	2015	114	155 mm uPVC	30-48; 84-102	74-114	57.9	65,000

4.2 PUMPING TESTS

The bores listed in Table 7 have all been test-pumped to determine pumping capacities and aquifer parameters. The PNC and Tropicana bore tests are described in GRC (1985) and MWES (2011), respectively, and the parameters derived from the test results are given in Table 8.

The tests on bores NWB1 and NWB2 are described below and the results are summarised in Table 8. The pumping test plots are included in Appendix III.

Table 8: Results of Pumping and Recovery Tests

Bore	mE	mN	Rec. Yield (kL/d)	T (m ² /d)	KH (m/d)	KV (m/d)	SC
	(MGA)						
MRWB4	557595	6691810	150	15	3.5		
MRWB5	563440	6687600	0	ND	ND	0.01-0.03	0.00025
MRWB6	557176	6690643	2100	450	37.5		
MRWB7	575480	6679975	3400	210	9		0.0002
MSWB02	557225	6690545	690	2330, 819	129, 45.5		ND
MSWB03	556958	6690702	690	1050	47.5		ND
NWB1	575552	6671190	1000*	4900, 5500	136-161		0.0004-0.0054
NWB2	575363	6670210	1000*	2500-5300	69-147		0.0002, 0.0009

* Yield limited by casing diameter

4.2.1 Bore NWB1

Bore NWB1, which intersects basal palaeochannel sands, was test-pumped by Harrington Drilling from 15th to 18th March 2015.

The initial test was a step-rate test with four one-hour steps at 430, 620, 790 and 920 kL/d. The purpose of the test was mainly to select a suitable rate for the constant-rate test, although that rate was limited by the capacity of the pump. The results were also analysed to determine bore efficiency: the efficiency decreased from 48 % in step 1 with a pumping rate of 430 kL/d to 30 % in step 4 with a pumping rate of 920 kL/d. A summary of the results is given in Appendix III.

The bore was then pumped at 1,210 kL/d for 48 hours. Water levels were monitored in the pumped bore; in bore NGW37 located 78 m to the south; and in NGW54C located 56 m north of NWB1. Drawdowns could not be monitored in NWB1 for the first 200 minutes of the test due to a bend in the access tube, and then fluctuated around 0.5 m to the end of the test. The drawdowns in the two monitoring bores followed straight-line trends on a semi-logarithmic scale for the first 800 minutes, typical of a laterally extensive aquifer. The drawdowns then stabilised, with minor fluctuations, indicating inter-aquifer leakage (Appendix III).

At the end of the test, water-level recovery was monitored in the three bores for a period of 80 minutes (NWB1) to 120 minutes (monitoring bores).

Drawdown and recovery plots for the bores are included in Appendix III. They were analysed using the Jacob method and Theis recovery method to determine aquifer transmissivity (T) and storativity (S). The transmissivity values were divided by the total screened interval in NWB1 (36 m) to determine average hydraulic conductivity (K) of the screened interval, which includes sand beds and any interbedded clayey layers. The results are given in Table 9.

Table 9: Results of Pumping and Recovery Tests, NWB1

Obs. Bore	Distance (m)	Constant Rate Test		Recovery Test		K Av. (m/d)	
		T (m ² /d)	S	T (m ² /d)	S	CR Test	Recovery
NWB1	0	ND	ND	5,400	ND	ND	150
NGW37	75.5	5,500	0.0005	5,800	0.0054	153	161
NGW54C	52	4,900	0.0004	8500??	0.013??	136	ND

The results indicate that the aquifer is highly permeable, and more permeable near NWB1 and NGW37 than at NGW54C. The aquifer is confined with low values of storativity.

Measurements of salinity, temperature and pH were made on the pumped water at the start of the constant-rate test, and then every four hours. The results are given in Table 10.

Table 10: Physico-Chemical Measurements made during NWB1 Test

Time Since Test Start (Hours)	TDS (mg/L)	Temp (°C)	pH
0	65,400	23.7	3.90
3	68,600	23.5	3.79
7	69,200	24.2	3.98
11	69,200	23.3	3.97
15	69,100	21.8	3.99
19	70,700	20.5	3.99
23	68,600	22.3	4.01
27	68,800	23.8	4.02
31	67,600	24.0	3.98
35	67,800	23.2	3.97
39	68,700	22.6	4.02
43	69,200	21.7	4.07
47	68,400	21.7	4.07

The results show that both pH and salinity fluctuated during the test, but possibly increased overall. The results of the laboratory analyses show that salinity was slightly lower at the end of the test than at the start.

Water samples taken at the beginning and end of the test were analysed by SGS laboratories. Salinity decreased slightly from 66,000 mg/L TDS at the start to 65,000 mg/L TDS at the end. The water was of a sodium chloride type; with elevated magnesium, sulphate and boron concentrations. Metal concentrations were low or below the reporting limits. Laboratory pH values were 4.0 (start) and 4.1 (end) showing the water to be acidic.

4.2.2 Bore NBW2

Bore NBW2, which also intersects basal palaeochannel sands, was test-pumped by Harrington Drilling from 12th to 15th March 2015.

The initial test was a step-rate test with four one-hour steps at 340, 600, 770 and 940 kL/d. The purpose of the test was mainly to select a suitable rate for the constant-rate test, although again that rate was limited by the capacity of the pump. Groundwater levels rose during the first step indicating the bore was still being developed. The results were analysed to determine bore efficiency: the efficiency decreased from 51 % in step 1 with a pumping rate of 340 kL/d to 28 % in step 4 with a pumping rate of 940 kL/d. A summary of the results is given in Appendix III.

The bore was then pumped at 950 kL/d for 48 hours. Water levels were monitored in the pumped bore; in bore NGW30 located 52 m to the south; and in NGW55 located 23 m north of NBW2. The water-level in the production bore drew down relatively rapidly in the first five minutes, and then declined very gradually to only about 0.3 m at the end of the test. Drawdowns in the two monitoring bores were relatively steep for the first 50 minutes, and then were very flat before steepening slightly towards the end of the test (Appendix III). These results show that the aquifer is highly permeable, and that the rate of drawdown was reduced by inter-aquifer leakage.

At the end of the test, water-level recovery was monitored in the three bores over a period of 60 minutes.

Drawdown-time and recovery plots for the bores are included in Appendix III. They were analysed using the Jacob method and Theis recovery method to determine aquifer transmissivity (T) and storativity (S). The transmissivity values were divided by the total screened interval in NBW2 (36 m) to determine average hydraulic conductivity (K) of the screened interval. The results are given in Table 11.

Table 11: Results of Pumping and Recovery Tests, NBW2

Obs Bore	Distance (m)	Constant Rate Test		Recovery Test		K Av. (m/d)	
		T (m ² /d)	S	T (m ² /d)	S	CR Test	Recovery
NBW2	0	2,500	ND	3,500	ND	69	97
NGW30	49.5	5,300	0.0002	ND	ND	147	ND
NGW55	32	4,500	0.0009	3,800	ND	125	106

The results indicate that the aquifer is highly permeable, particularly near NGW30 and to a lesser degree, NGW55. The aquifer is confined with low values of storativity.

Measurements of salinity, temperature and pH were made on the pumped water at the start of the constant-rate test, and then every four hours. The results are given in Table 12.

Table 12: Physico-Chemical Measurements made during NWB1 Test

Time Since Test Start (Hrs)	TDS (mg/L)	Temp (°C)	pH
0.5	61,700	22.6	3.82
4	60,200	25.2	3.97
8	60,200	25.4	3.93
12	62,000	23.3	4.02
16	62,100	22.7	4.07
20	61,100	21.0	4.11
24	62,000	22.8	4.06
28	58,600	26.1	4.03
32	59,700	25.7	3.98
36	60,100	24.4	4.07
40	61,600	23.9	4.13
44	61,500	23.1	4.08
48	61,300	23.4	4.08

The results show that both pH and salinity fluctuated during the test, and pH possibly increased overall. The results of the laboratory analyses show that salinity was slightly lower at the end of the test than at the start.

Water samples taken at the beginning and end of the test were analysed by SGS laboratories. Salinity decreased slightly from 59,000 mg/L TDS at the start to 58,000 mg/L TDS at the end. The water was of a sodium chloride type; with elevated magnesium, sulphate and boron concentrations. Metal concentrations were low or below the reporting limits. Laboratory pH values were 4.5 (start) and 4.4 (end) showing the water to be acidic.

4.3 SLUG TESTS AND LOW-FLOW PUMPING TESTS

Fifty-five slug (falling-head) permeability tests, and five low-flow recovery tests following pumping for sampling, were conducted by Vimy on monitoring bores in the Ambassador/Princess area.

The slug tests consisted of introducing a slug of water, generally 20 litres, and monitoring the rate of water level decline using pressure transducers and data loggers. The data were analysed using the method of Bouwer and Rice (1976).

The low-flow recovery tests consisted of monitoring water-level recovery following pumping. The results were analysed using the method of Theis (1935).

The results of the tests are given in Table 13. Where there was no measurable water-level recovery during the tests, the permeability (hydraulic conductivity, K) is recorded as being very low. Where the water-level recovery was too rapid to be measured during the slug tests, the permeability was recorded as being high (> 5 m/d).

5 NUMERICAL GROUNDWATER MODELLING

A numerical groundwater model was constructed of the planned mining and re-injection areas, and run to estimate the dewatering requirements and the impacts of pumping, re-injection and tailings seepage. It is based on the conceptual hydrogeological model, described below.

5.1 CONCEPTUAL HYDROGEOLOGICAL MODEL

The Mulga Rock deposits lie within an oxbow basin/palaeochannel that remains after the capture of three trunk palaeochannels by the Ponton Creek palaeochannel.

The Mulga Rock palaeochannel is probably still hydraulically connected to the Ponton Creek palaeochannel some 65 km to the south along the eastern arm.

The water table is about 50 m deep, and is overlain by mainly fine-grained sediments, except along the eastern arm south of Ambassador where there is a substantial thickness of unsaturated sand (e.g. Figs. 8 and 9). The mineralised zones are mainly just below the water table and in fine-grained carbonaceous sediments. Sand and gravel beds of Eocene age become more common towards the base of the palaeochannel. These basal sands and gravel have moderate to high permeability and form the main zone of groundwater flow.

The water table is very flat-lying in the “Narnoo Basin” which contains the Mulga Rock deposits, showing there is little groundwater flow into, and out of the basin. Hydraulic gradients indicate there is probably minor groundwater flow into the basin from the north-west and north, and from the north-east along a tributary channel which contains the Ambassador deposit. The flow in Eocene sands along the tributary channel is greatly restricted by a basement high between the western and eastern parts of the Ambassador deposit.

Table 13: Results of Slug and Low-Flow Pumping (Recovery) Tests

Bore	mE	mN	Test Type	Open depth (m)	SWL (m bgl)	K (m/d)	Model Layer
NND5029	575965	6681554	Low-flow rec	52.5	36.91	0.2	1,2
NND5030	575544	6681137	Low-flow rec	54.1	35.37	> 0.3	1,2
NND5031	579499	6682610	Low-flow rec	54.7	33.66	0.007	1,2
NNA5198	575539	6682048	Low-flow rec	51.7	35.92	0.003	1,2
NNA5227	576237	6680967	Low-flow rec	41.4	27.84	V. Low	1,2
NNA5177	576185	6682159	Slug Test	43.7	39.61	V Low	1
NNA5178	576216	6682140	Slug Test	41.6	39.11	0.01	1
NNA5198	575539	6682048	Slug Test	55.7	35.38	0.02	1,2
NNA5200	578614	6682405	Slug Test	39.6	37.10	V Low	1
NNA5201	578623	6682398	Slug Test	42.5	37.67	V Low	1
NNA5209	577232	6682510	Slug Test	40.8	40.85	0.00	1
NNA5210	577308	6682464	Slug Test	41.9	41.19	High	1
NNA5211	577374	6682425	Slug Test	41.0	40.60	?	1
NNA5213	577174	6682539	Slug Test	43.0	41.85	0.02	1
NNA5214	577099	6682591	Slug Test	43.1	43.11	High	1
NNA5215	577027	6682625	Slug Test	58.3	43.35	V Low	1,2
NNA5219	577144	6682792	Slug Test	41.5	33.47	V Low	1
NNA5220	577210	6682754	Slug Test	41.5	35.78	V Low	1
NNA5221	576271	6681162	Slug Test	42.3	33.87	V Low	1
NNA5222	576337	6681123	Slug Test	38.7	37.67	V Low	1
NNA5226	576155	6681009	Slug Test	43.1	35.58	V Low	1
NNA5227	576236	6680967	Slug Test	41.4	38.64	V Low	1
NNA5228	576293	6680926	Slug Test	45.9	38.94	V Low	1
NNA5229	576367	6680885	Slug Test	45.0	36.92	V Low	1
NNA5230	576434	6680844	Slug Test	38.1	36.75	0.07	1
NNA5231	576556	6680766	Slug Test	38.9	31.11	V Low	1
NNA5232	576493	6680799	Slug Test	26.8	19.35	V Low	1
NNA5234	576019	6680570	Slug Test	42.8	36.78	0.05	1
NNA5235	575004	6679932	Slug Test	52.9	39.34	0.11	1,2
NNA5236	574933	6679974	Slug Test	46.2	38.37	0.18	1
NNA5238	574792	6680063	Slug Test	40.5	40.49	High	1
NNA5239	574714	6680104	Slug Test	55.3	41.39	V Low	1,2
NNA5240	574645	6680151	Slug Test	50.3	40.29	0.25	1
NNA5289	579988	6682770	Slug Test	31.0	30.88	0.04	1
NNA5301	580153	6682866	Slug Test	29.9	22.61	V Low	1
NNA5321	579933	6682698	Slug Test	40.9	32.06	V Low	1
NNA5465	575179	6680575	Slug Test	40.3	32.70	0.27	1
NNA5589	580088	6684614	Slug Test	40.8	42.59	0.38?	1
NNA5614	578964	6683963	Slug Test	48.0	41.38	0.11	1
NNA5623	578774	6684324	Slug Test	46.0	42.46	0.15	1
NNA5628	579432	6683938	Slug Test	47.5	37.62	0.07	1
NNA5630	579451	6684166	Slug Test	44.5	44.50	V Low	1
NNA5634	579135	6684302	Slug Test	45.4	43.75	0.16	1
NNA5639	579741	6684370	Slug Test	53.2	48.48	0.08	1
NNA5641	579005	6683723	Slug Test	60.8	44.64	0.13	1,2
NNA5644	578770	6683872	Slug Test	50.1	44.87	0.17	1
NNA5647	578838	6683579	Slug Test	42.0	39.19	V Low	1
NNA5740	579643	6684560	Slug Test	53.5	41.99	0.32	1,2
NNA5749	579238	6683679	Slug Test	40.6	36.23	0.19	1
NNA5753	578490	6684007	Slug Test	52.5	43.25	0.12	1
NND5028	576087	6681735	Slug Test	47.6	37.30	0.61	1
NND5029	575965	6681554	Slug Test	52.3	36.81	1.28	1,2
NND5030	575544	6681137	Slug Test	55.6	35.30	1.91	1,2
NND5032	578632	6682382	Slug Test	51.5	38.50	1.10	1,2
NND5033	579138	6682819	Slug Test	49.1	40.83	2.72	1
NND5034	576399	6681300	Slug Test	46.0	39.85	2.15	1
NND5035	576053	6682472	Slug Test	46.4	37.30	1.71	1
NND5036	576591	6682391	Slug Test	50.7	39.24	1.16	1
NND5037	578682.0	6682609	Slug Test	44.6	35.90	0.97	1
NND5038	579231	6682522	Slug Test	51.4	39.26	2.30	1,2
NND5039	579796	6682656	Slug Test	51.2	34.04	1.05	1,2
NND5040	580034	6682734	Slug Test	43.6	32.93	0.32	1
NND5041	580092	6682899	Slug Test	37.8	32.67	0.32	1
NND5077	576148	6682189	Slug Test	49.8	39.67	V Low	1
NND5078	577076	6682606	Slug Test	53.2	48.60	1.52	1

Groundwater possibly flows from the basin to the south along the western arm of the palaeochannel; and probably also south along the eastern arm, although the flow rate is low and is restricted by the mainly fine-grained sediments in at least part of the palaeochannel (Section Line 92,500 N, Uranerz 1986), about 25 km south of Ambassador.

Groundwater in the palaeochannel is saline to hypersaline and generally acidic, and contains low metal concentrations.

5.2 DESCRIPTION OF NUMERICAL MODEL

A numerical groundwater model has been constructed of the Mulga Rock palaeochannel. It consists of a rectangular grid of 142 rows, 104 columns and three layers covering an area of 45 km east–west by 65 km north–south (Fig. 15). Cell sizes are 500 m by 500 m in general, and 250 m by 250 m in the Ambassador area.

Layer 1 represents fine-grained sediments near the water table; Layer 2 consists of interbedded sands and clays and admixtures; and Layer 3 the basal sand/gravel. The base of Layer 3 i.e. the base of the palaeochannel (Eocene sediments) and the top of the Eocene sediments were defined from data provided by Vimy for the numerous holes drilled for the Mulga Rock Uranium Project; and from the Uranerz geological sections.

The model was utilises Processing Modflow Pro version 8.0.2 (Simcore Software, 2010), which includes Modflow, finite difference groundwater modelling software designed by the U.S. Geological Survey (McDonald and Harbaugh, 1988).

5.3 MODEL PARAMETERS

The model was initially set up with parameters determined from the pumping and slug tests; and assumed values based on grain sizes and our experience in modelling similar hydrogeological environments. The parameters, particularly horizontal hydraulic conductivity of the main aquifer, Layer 3, were varied in the calibration of the model. Parameters adopted on calibration of the model are given in Table 14.

Table 14: Adopted Aquifer Parameters

Parameter	Units	Layer 1	Layer 2	Layer 3
Horiz. Hydraulic Cond.	m/d	0.02-0.7	0.2-9	0.2-140
Vert. Hydraulic Cond.	m/d	0.01	0.1	0.5
Specific Yield	v/v	0.05	0.1	0.1
Storage Coefficient	v/v	NA	0.0004	0.0004
Recharge	m/d	0, 0.000001		

Horizontal hydraulic conductivity values were predominantly 0.1 m/d in Layer 1, 1 m/d in Layer 2, and 9 m/d in Layer 3. Values in Layer 1 in the Ambassador area were altered to utilise the results of the low-flow pumping tests and slug tests described in Section 4.3 above. In Layer 2, a variety of values were used in the Ambassador area depending on sand content in the zones to be mined, and the results of slug tests from deeper drillholes; and a low value of 0.2 m/d was adopted for the basement high between the two parts of the deposit. In Layer 3, there were higher values (70–140 m/d) in the planned injection area; and some lower values in the southern part of the eastern arm, and in the north-eastern tributary channel, particularly at the basement high at Ambassador as for Layer 2.

Recharge was assumed to be zero for much of the modelled area, except for a very low rate of 0.000001 m/d on the north-western edge of the basin and in part of the north-eastern tributary.

5.4 MODEL CALIBRATION

The model was first calibrated in steady-state mode to groundwater levels measured at various times in representative bores/holes over the Mulga Rock area. This was achieved by varying horizontal hydraulic conductivity of the main, basal sand aquifer (Layer 3), and to a much lesser degree, recharge in small areas in the north-west and north-east. The parameters adopted for the minor aquifers/aquitards and aquicludes of Layers 1 and 2 have negligible impact on the calibration; and storativity (specific yield and storage coefficient) is not part of a steady-state simulation.

A comparison between measured and model-calculated water levels is shown in Figure 16. There is a close correspondence and the root mean square error for all the calibration bores is 2.22 %, much lower than the 5 % limit recommended in the 2000 groundwater modelling guidelines (Middlemis, 2000), and 5 % or 10 % (if achievable) given in the more-recent guidelines (Barnett et. al., 2012).

The model was then calibrated in transient mode by simulating the bore NWB1 and 2 pumping tests. For the early data, (the first 10 to 60 minutes) a good match was achieved between calculated and observed drawdowns in the monitoring bores during the tests (Figs. 17 to 20) with a confined storage coefficient of 0.0008, at the upper end of the range of values indicated from the pumping test results. Although all the calculated drawdowns are within 0.16 m of the measured values, there is a divergence in the later stages of the test as the calculated values cannot replicate the reduced drawdowns resulting from inter-aquifer leakage, and they are also increased by the impact of boundaries to the aquifer. With long-term pumpage the effects of leakage are expected to disappear and the palaeochannel boundaries will increase the rate of drawdown.

5.5 MODEL SIMULATION AND RESULTS

The mine water balance dated 18 May 2015 has the following key components:

- Pit Dewatering flows to the processing plant are 96.8 kL/hr (2,323 kL/d);
- Water pumped from (low-salinity) borefield is 151.7 kL/hr (3,641 kL/d)
- Extraction from Tropicana mine's bore located in the Emperor pit (MSWB02) was included at a rate of 50 kL/d (the average for the period (July 2011 to November 2014); and
- Tailings seepage is 28.6 kL/hr (686 kL/d).

Any excess water from dewatering, plus 2.2 kL/hr reject water from the desalination plant, will be reinjected at the borefield south of Ambassador.

The mine plan for the Ambassador and Princess deposits is as shown in Fig. 21 and mine plans for the Emperor and Shogun deposits are shown in Fig. 22, and each area was subdivided into assumed annual pit areas. Modflow's Drain package was used to simulate dewatering with annual stress periods, with drain elevations set at the elevations of the planned base of mining which is presented in Fig. 23 for the Ambassador and Princess deposits and in Fig. 24 for the Emperor and Shogun deposits. Drain conductances are based on horizontal hydraulic conductivity values at the drain positions and model cell sizes.

Modflow's Well package was used to simulate: (1) tailings seepage from previously mined pits; (2) reinjection in years where average dewatering flows exceeded 2,323 kL/d and (3) extraction from the Tropicana bore.

Model-calculated average flows for each year are given in Table 15.

The results indicate that the maximum dewatering flows will be in Year 10 when an area is mined down to 255 m AHD on the western side of Ambassador West. There are also relatively high flows in Year 3 when a low area is mined on the northern side of Ambassador East. In those years, surplus water will be injected. In the other years all dewatering water will be used for processing ore or dust suppression.

Table 15: Calculated Dewatering Flows and Injection Rates

Year	Annual Dewatering Vol. (kL)	Av. Flow (kL/d)	Av. Injected (kL/d)	Dewatering Location
1	105,846	290	0	Princess & Ambassador
2	411,761	1,128	0	
3	1,419,378	3,889	1,566	
4	89,190	244	0	
5	800,239	2,192	0	
6	486,206	1,332	0	
7	91,326	250	0	
8	115,725	317	0	
9	58,490	160	0	
10	1,497,545	4,103	1,780	
11	73,520	201	0	
12	103,414	283	0	Emperor
13	486,181	1,332	0	
14	607,460	1,664	0	
15	633,905	1,737	0	Emperor & Shogun
16	395,128	1,083	0	

Model-calculated groundwater level drawdowns at the end of Year 10 are shown in Figs 25 and 26 for model Layers 1 (surficial) and 3 (basal Eocene sand), respectively. They indicate drawdowns around the area of active mining will extend about 3.6 km to the south, with a low mound in the area of tailings seepage. The rise in water levels around the reinjection borefield is less than 1 m. At the end of Year 16, drawdowns are around the western mining area (the Emperor and Shogun deposits), with drawdowns extending about 3.9 km to the south of the Emperor pit and negligible drawdown at the Shogun deposit due to the relatively shallow depth of mining (Figs. 27 and 28). Maximum model-calculated drawdowns at each mining location and at the injection borefield are also presented in Figure 29 and show that the effects of dewatering will be localised during mining.

The model was then run to simulate the movement of conservative particles in the groundwater from a point at the southern end of the mining area (representing tailings seepage), and from the southern injection bore NWB2. The movement from both points would be very slow due to the low hydraulic gradients, with the groundwater only moving 2.8 km and 2.2 km, respectively, in 1,000 years (Fig. 30). In an expected worst case with double the horizontal hydraulic conductivities, and with 1,816 kL/d injected via NWB2 in the second-to-last year of mining, the distances travelled in 1,000 years would be 9 km and 4 km, respectively (Fig. 30).

5.6 SENSITIVITY ANALYSIS

The modelling described in Section 5.5 above was repeated to determine the impact on dewatering flow rates of the various model parameters. The value of each parameter was doubled and then halved in turn, which is about the expected maximum variation that is likely to occur.

The results are given in Table 16. They show that the model is most sensitive to horizontal hydraulic conductivity (KH) followed by specific yield (SY) and vertical hydraulic conductivity (KV). It is insensitive to the confined storage coefficient, recharge and drain conductance.

Table 16: Results of Sensitivity Analysis

Case	Total Volume Pumped (kL)	Difference	
		(kL)	%
Adopted	7,375,314	0	0
KH*2	9,914,636	2,539,323	34.4%
KH/2	5,588,461	-1,786,853	-24.2%
KV*2	8,369,283	993,970	13.5%
KV/2	6,381,852	-993,462	-13.5%
SY*2	9,594,769	2,219,456	30.1%
SY/2	6,066,511	-1,308,803	-17.7%
SC*2	7,442,535	67,222	0.9%
SC/2	7,366,360	-8,954	-0.1%
Rech.*2	7,403,267	27,953	0.4%
Rech./2	7,386,573	11,260	0.2%
Drain Cond.*2	7,339,324	-35,990	-0.5%
Drain Cond./2	7,353,616	-21,698	-0.3%

In a likely worst case with double the adopted horizontal hydraulic conductivities, dewatering flows could be 34% higher overall than the calculated flows, and up to 50 % higher in the high-flow years when mining intersects the deep Eocene sands.

5.7 DISCUSSION OF MODELLING RESULTS

Although the model is well calibrated to steady-state conditions, aquifers in the area have not been stressed except by short-term pumping tests, and so there are few data available for transient calibration. The modelling results should, therefore, be taken as best estimates – actual dewatering pumping rates could be significantly different to those predicted.

Groundwater levels and pumping rates should be closely monitored once mining and dewatering commences, and the data used after six to twelve months of pumping to re-calibrate the model and to update the predictions.

6 POTENTIAL ENVIRONMENTAL RECEPTORS

6.1 QUEEN VICTORIA SPRING

The Queen Victoria Spring Nature Reserve lies down-gradient of the MRUP: the northern boundary of the reserve is 14 km south of the planned injection borefield and 24 km south of the Ambassador deposit.

The Queen Victoria Spring was first encountered by a European by Giles in September 1875 (Giles, 1889). At that time, it was “150 yards in circumference and two to three feet deep and was surrounded by numerous native wells”. He believed it to be a permanent body of water that was supplied by drainage of the sand hills that surround it, and that rests on a substratum of impervious clay.

The presence of numerous wells is a good indication that the spring was not a permanent feature. In April 1896, Carnegie (1898) visited the spring and found that it and all the native wells were dry. He managed to obtain sufficient water by digging a shallow well in the base of the spring.

The spring was said by Giles to be surrounded by clumps of “funereal pines”, presumably sheoaks that would have been sustained by this shallow, perched groundwater.

The spring can be seen as a small oval-shaped depression on Google Earth at 555170 mE, 6633710 mN at an elevation of about 323 m AHD, and looks to have been dry when the image was taken on 4 October 2013.

The spring is interpreted to be a local, ephemeral, perched water source, located 14 km from the nearest water injection site for the MRUP. It is not, therefore, an environmental receptor that could be impacted by the planned mining at Mulga Rock.

6.2 PALAEOCHANNEL AQUIFER

The palaeochannel aquifer and overlying sediments contain saline to hypersaline groundwater. The water table is too deep, and the groundwater too saline to support vegetation; and it is very unlikely that there will be any other users of the groundwater within the area that could be impacted during mining and within 1,000 years thereafter.

Groundwater at the planned injection borefield has salinity of about 60,000 mg/L TDS, compared with about 20,000 to 30,000 mg/L TDS at the Ambassador and Princess deposits. Provided the pH is similar, any excess water that is reinjected should be of better quality than the receiving water.

Groundwater in the planned mining areas has the potential to become more acidic – this should be addressed in environmental investigations; as well as any treatment required for tailings, and for water to be reinjected.

7 CONCLUSIONS

Most of the sediments to be mined are fine-grained and of low permeability, and so dewatering flow rates will be low. Some high dewatering flows will be required when deep mineralised zones associated with Eocene sands are mined. Much or all of the dewatering water will be used in the processing plant. This will be supplemented by low-salinity water from the Kakarook North borefield and water recycled from the in-pit beneficiation plant.

Any water reinjected into the palaeochannel aquifer is expected to be of lower salinity than the receiving water, and should be of better quality provided the pH is controlled if necessary.

Seepage from in-pit tailings will infiltrate to groundwater of similar salinity to that at the Ambassador deposit. The zone where seepage would reach the water table includes reactive carbon-rich layers that will tend to fix any metals in the leachate.

The results of numerical groundwater flow and flow-path modelling indicate that the impacts of dewatering, tailings seepage and any reinjection will be localised during mining, and should not extend further than three to four kilometres south of the mining area or the reinjection borefield within 1,000 years of the end of mining. Even in a worst case, any water introduced to the palaeochannel aquifer is indicated to not extend further than 4 km south of the injection borefield over that period due to very low hydraulic gradients.

Dated: 29 October 2015

Rockwater Pty Ltd

M J Taylor
Senior Hydrogeologist

P H Wharton
Principal

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FIGURES

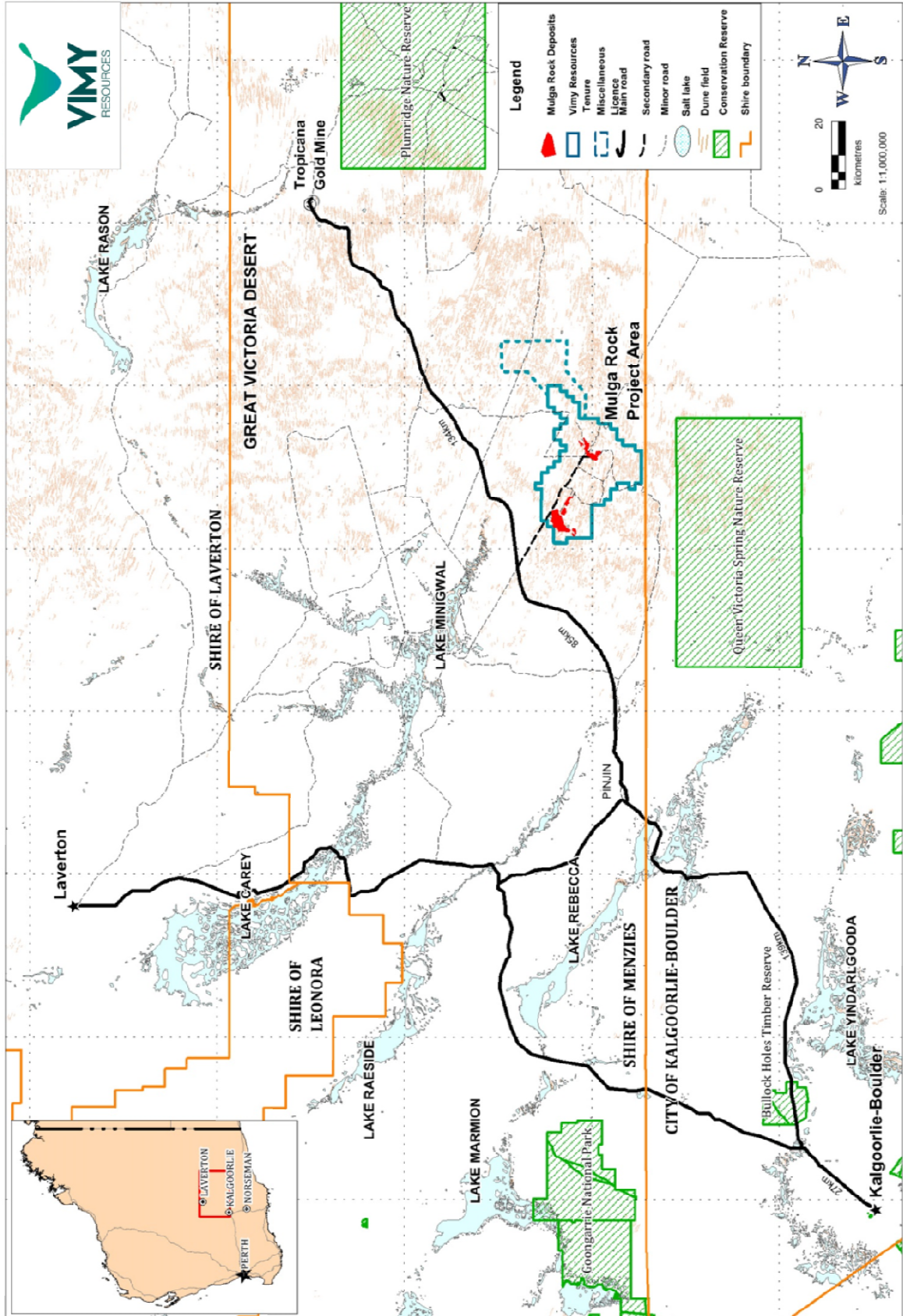


figure 1.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock
 DATE: June 2015
 Dwg No: 345.0/15/1-1

LOCATION OF THE MULGA ROCK
 URANIUM PROJECT

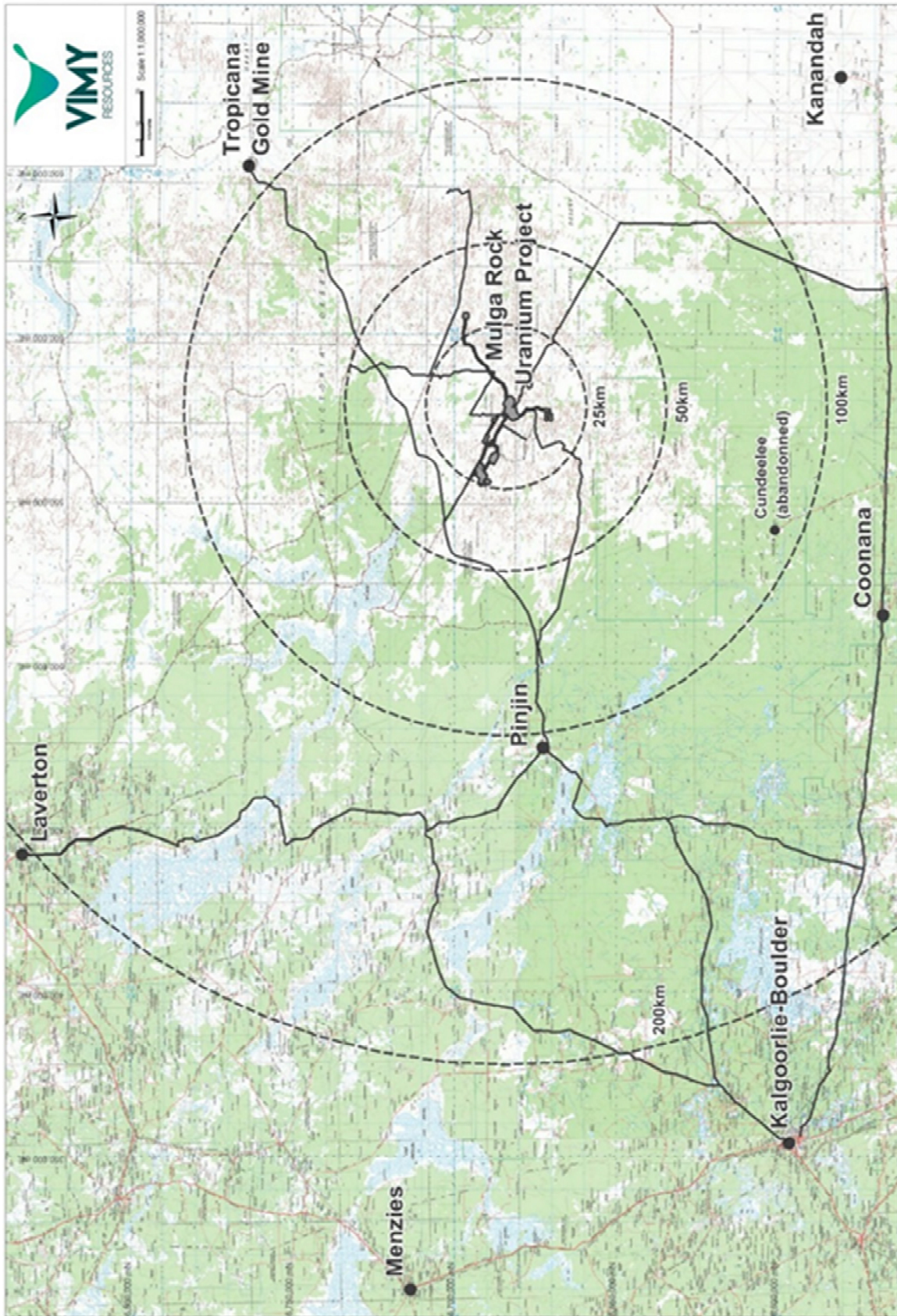


figure 1.srf

CLIENT: Vimy Resources
PROJECT: Mulga Rock
DATE: June 2015
Dwg No: 345.0/15/1-2

MRUP AND NEARBY COMMUNITIES

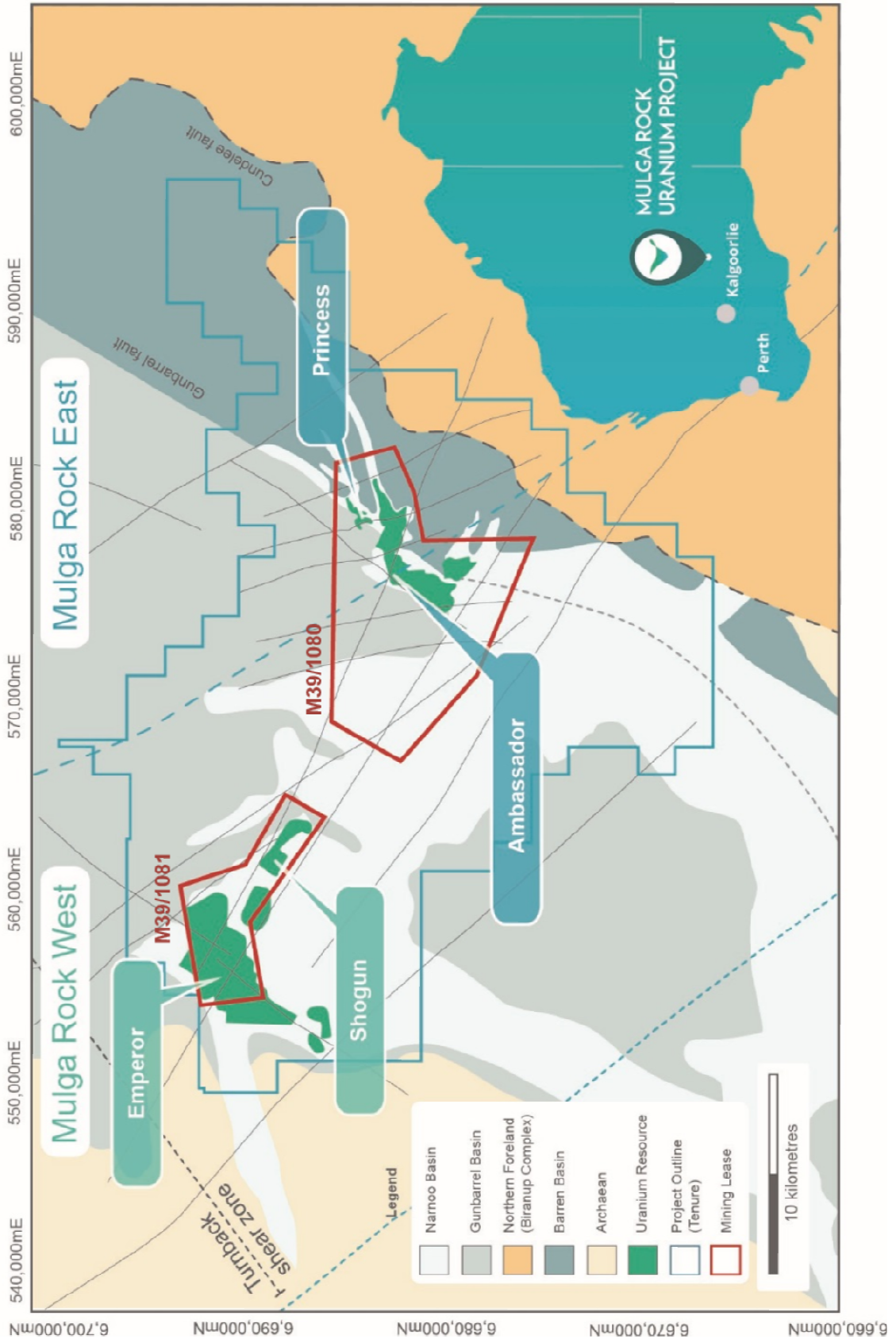
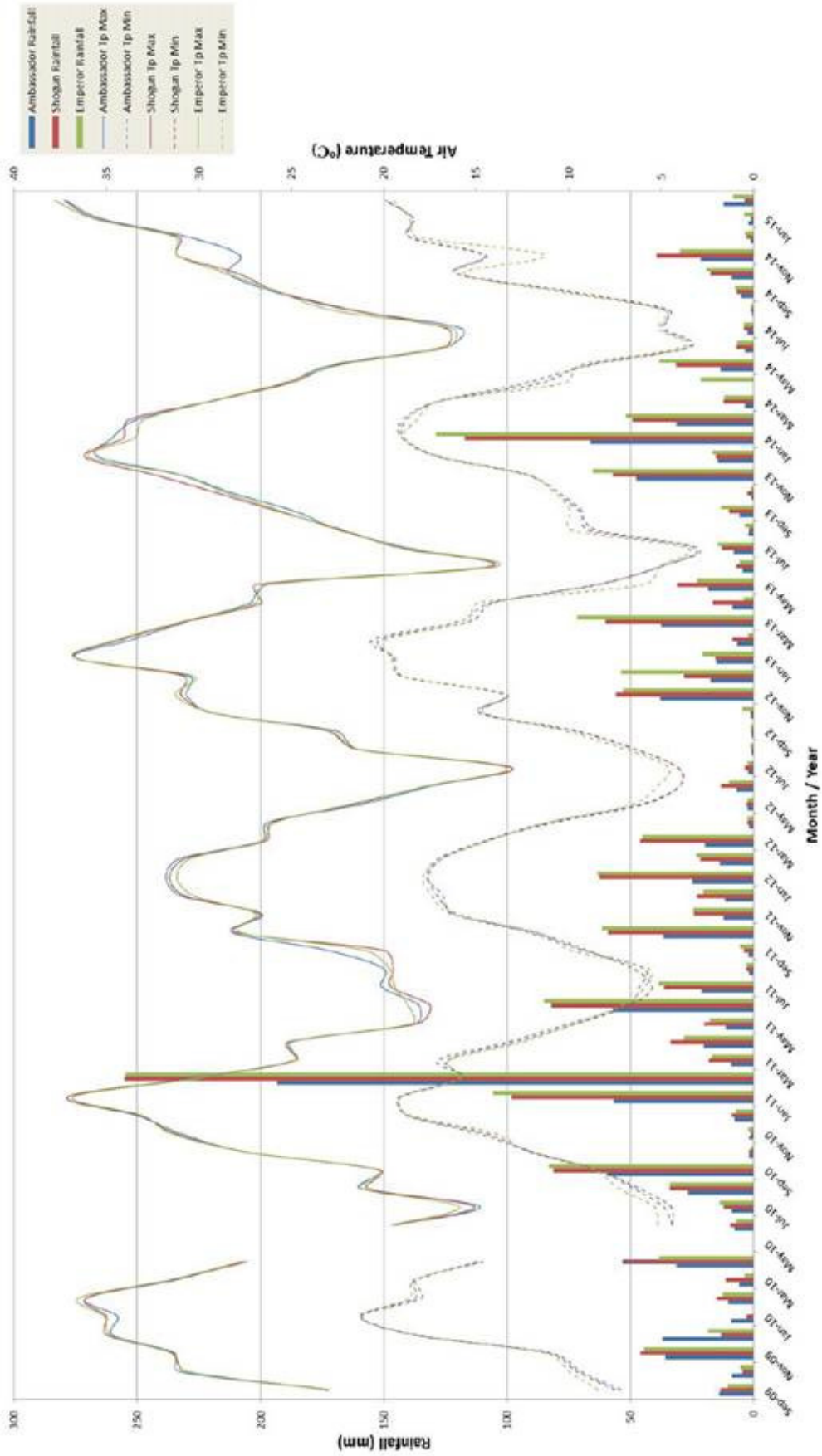


figure 3.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock
 DATE: June 2015
 Dwg No: 345.0/15/1-3

MRUP MINING CENTRES AND
 ASSOCIATED RESOURCES

Figure 4



rainfalls & temp.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: May 2015
 Dwg No: 345.0/15/2-4

MAXIMUM & MINIMUM TEMPERATURES, AND MONTHLY RAINFALLS, MULGA ROCK WEATHER STATIONS

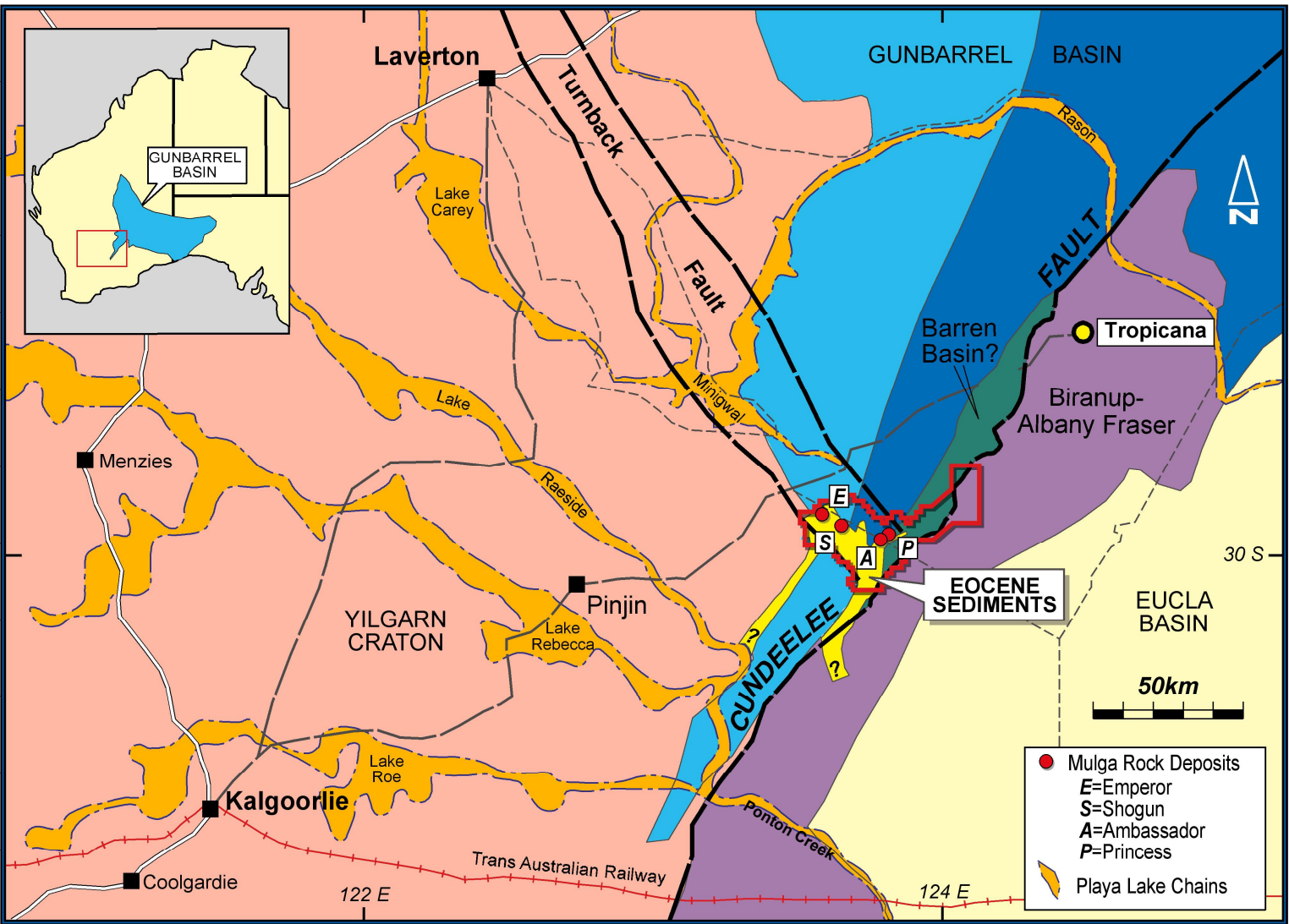


Figure 5

geological setting.srf

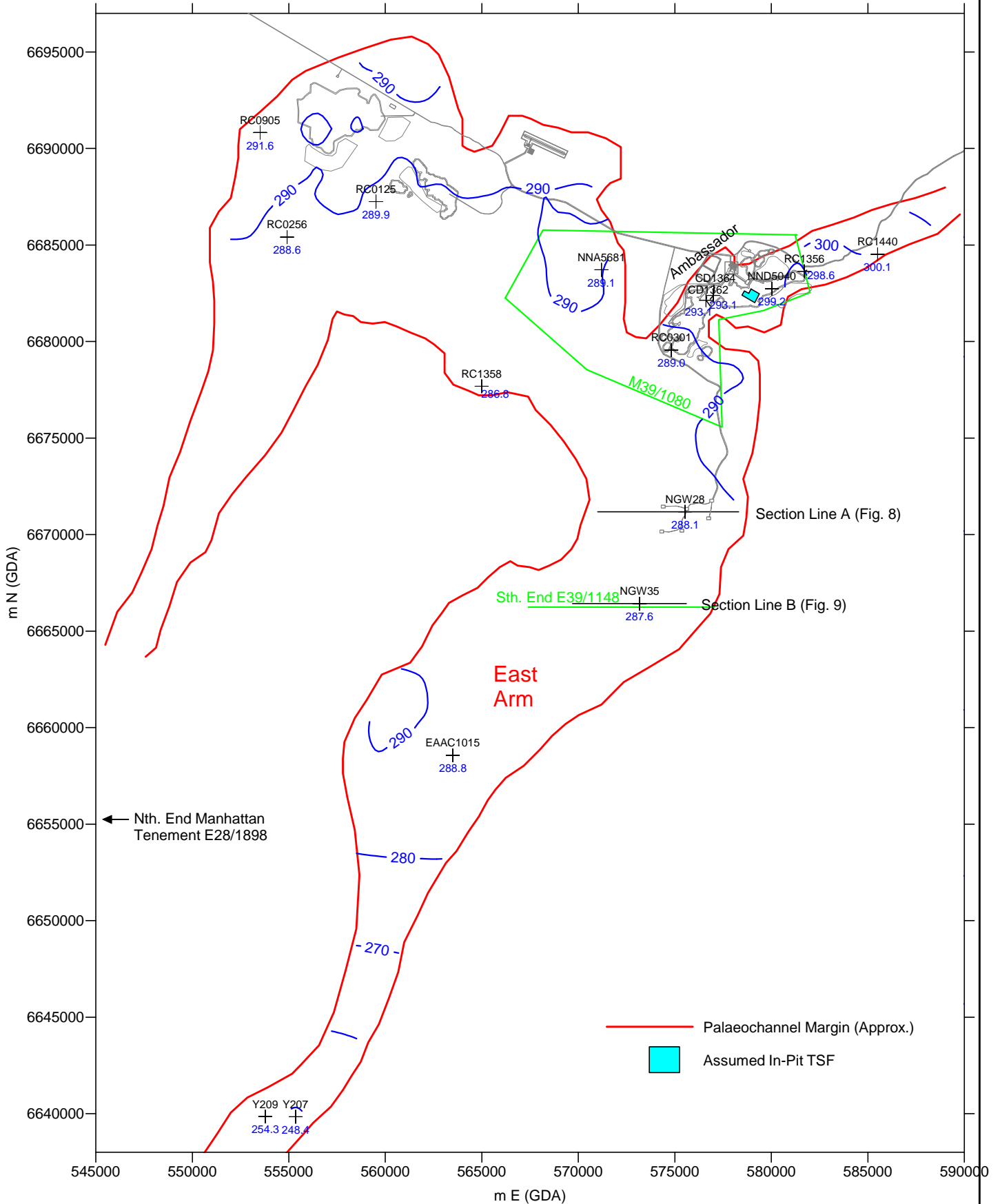
CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology

DATE: May 2015

Dwg No: 345.0/15/2-5

REGIONAL GEOLOGICAL SETTING

Figure 6



Surfer/15-02 Rev2d/Fig6: rtwis & calib bores.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 Dwg No: 345.0/15/2-6

REDUCED GROUNDWATER LEVELS (m AHD) MEASURED
 IN ALL BORES AT VARIOUS TIMES (CONTOURS),
 AND IN CALIBRATION BORES (POST VALUES)

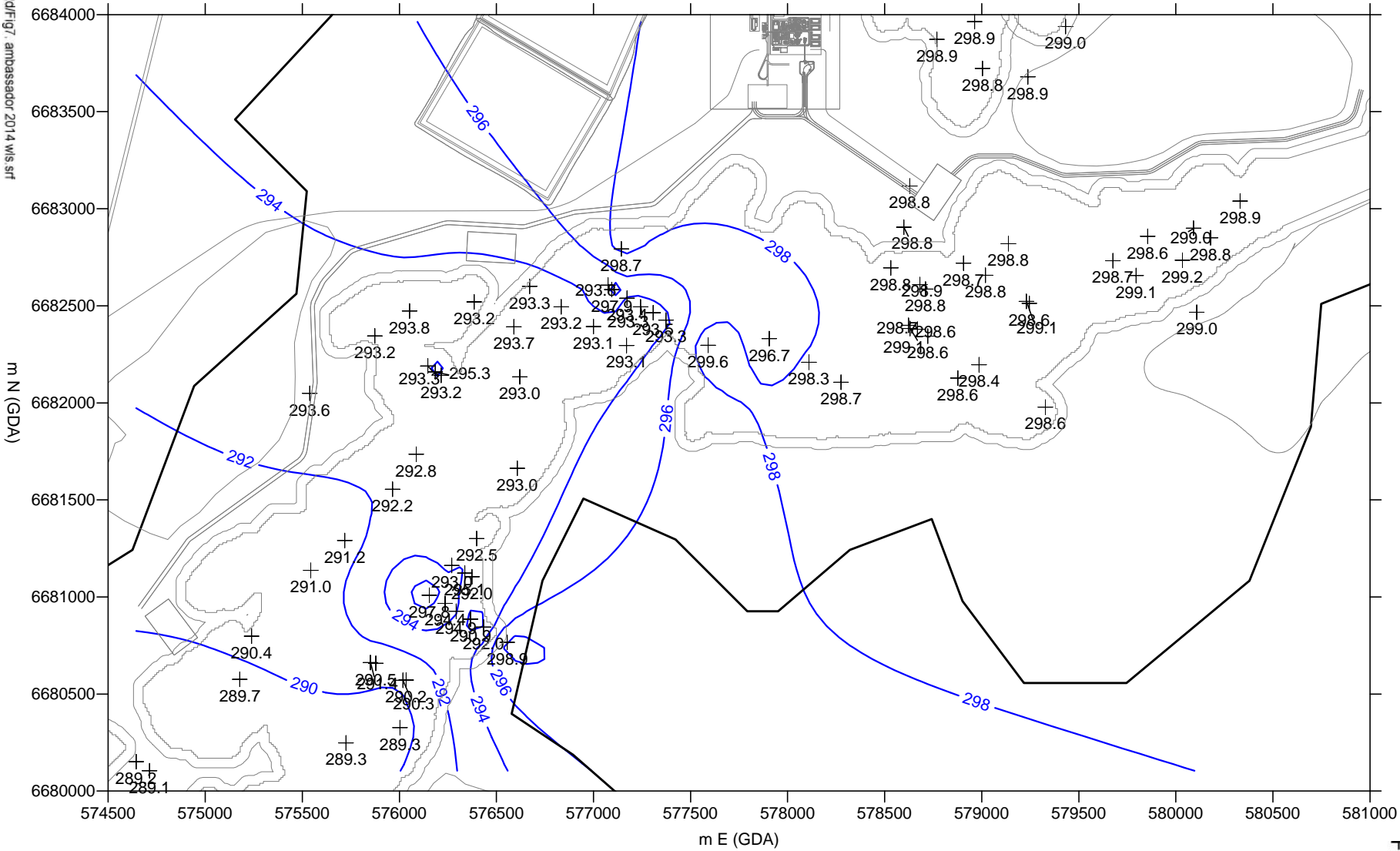


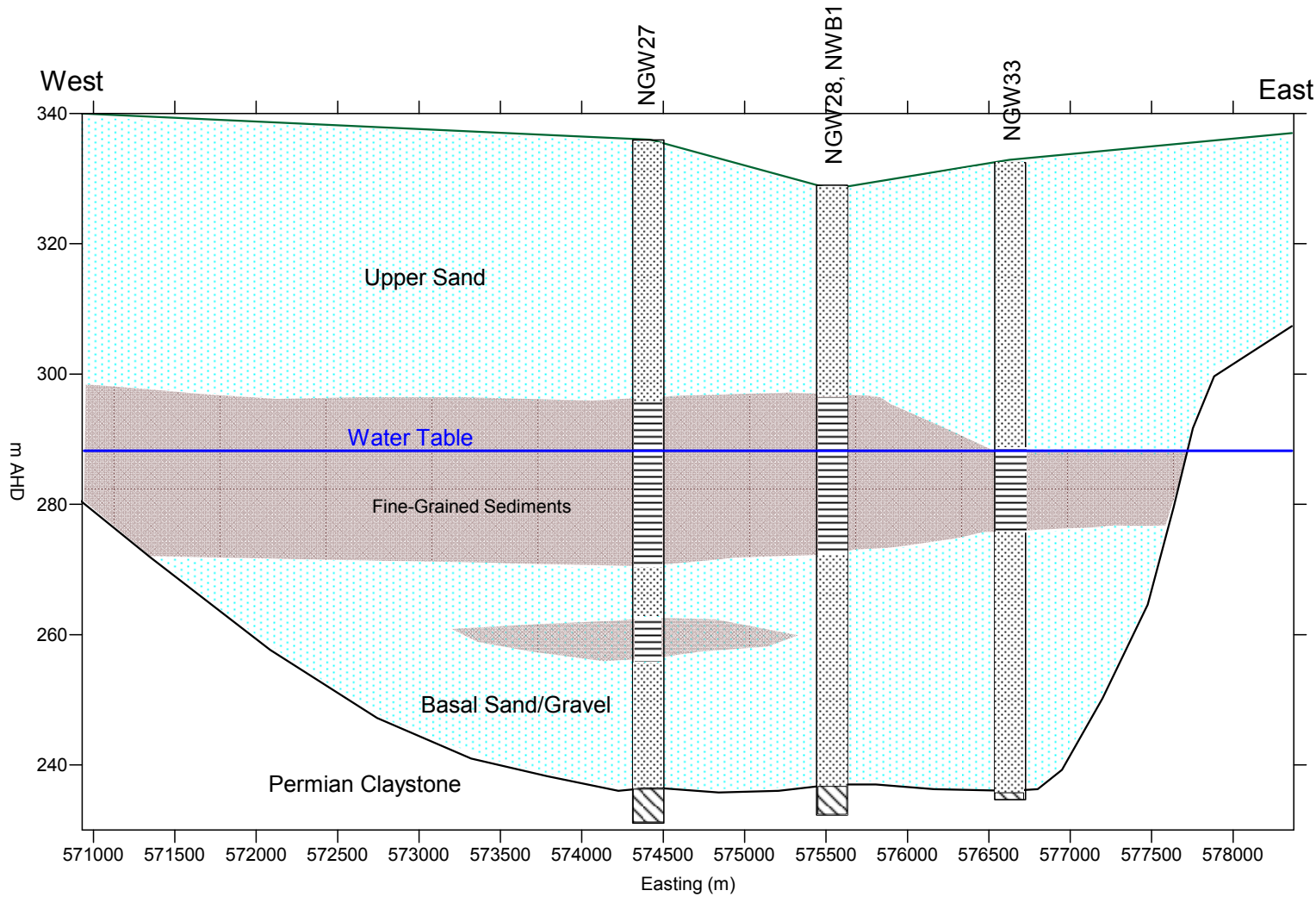
Figure 7

345-0/Surfer/15-02 RevZdr/fig7_ambassador 2014 m/s.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 DWG No: 345.0/15/2-7

GROUNDWATER LEVELS (m AHD) MEASURED
 APRIL 2014, AMBASSADOR DEPOSIT





40 X Vertical Exaggeration

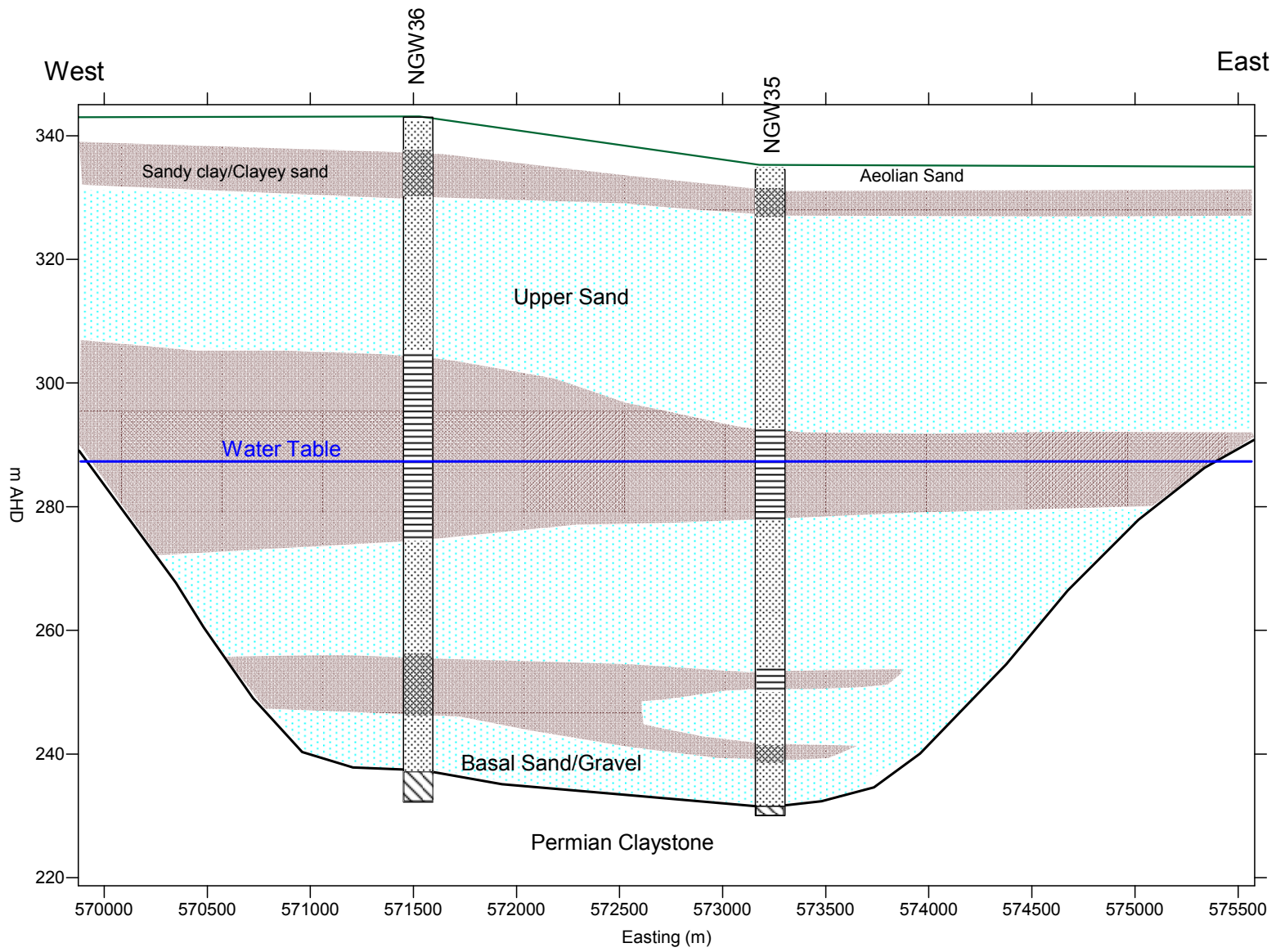
Figure 8

section Line A.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: April 2015
 Dwg No: 345.0/15/2-8

HYDROGEOLOGICAL CROSS-SECTION
 INJECTION BOREFIELD AT NWB1 (LINE A)





30 X Vertical Exaggeration

Figure 9

section Line B.srf

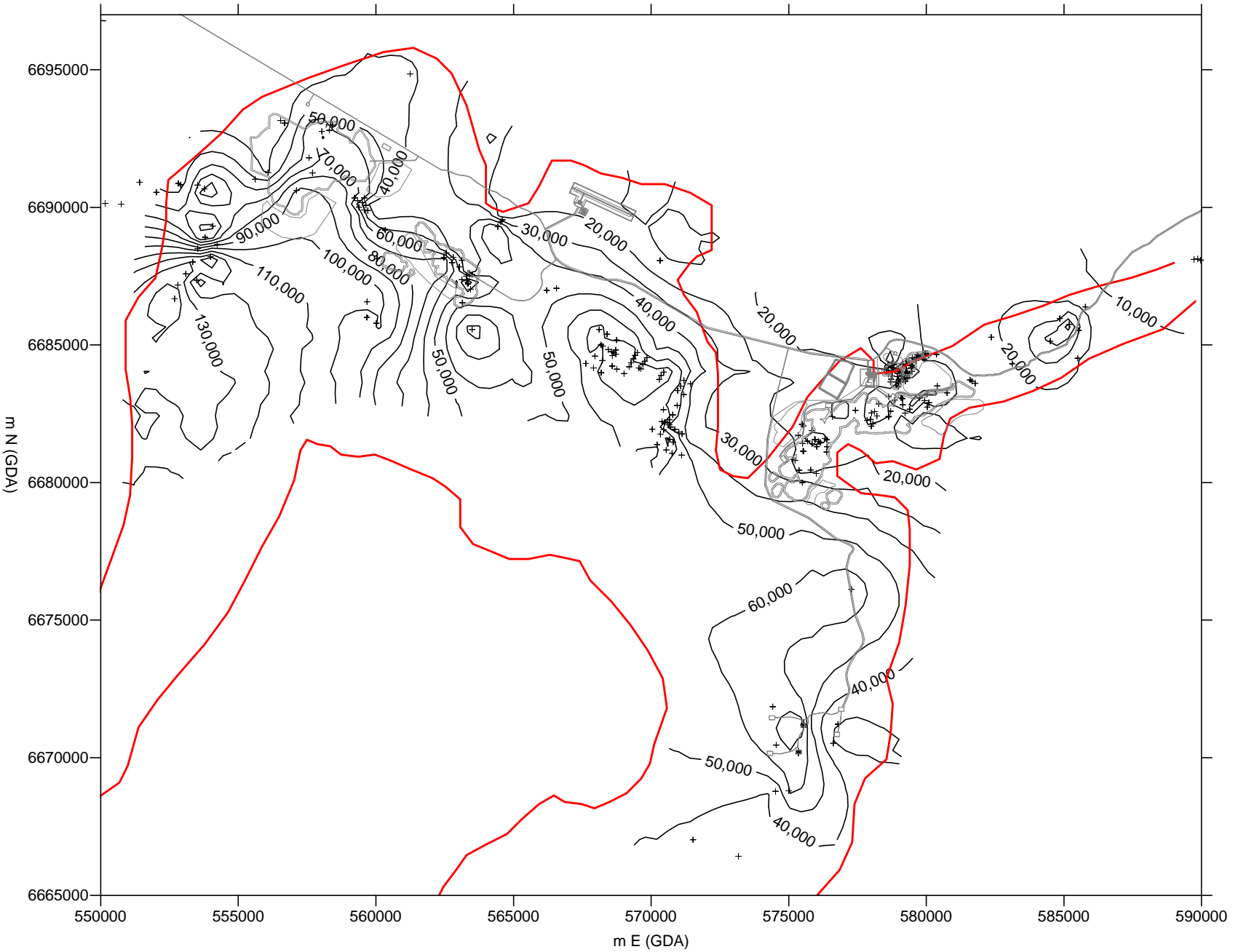
CLIENT: Vimy Resources

PROJECT: Mulga Rock Hydrogeology

DATE: April 2015

Dwg No: 345.0/15/2-9

HYDROGEOLOGICAL CROSS-SECTION
SOUTH OF INJECTION BOREFIELD, LINE B



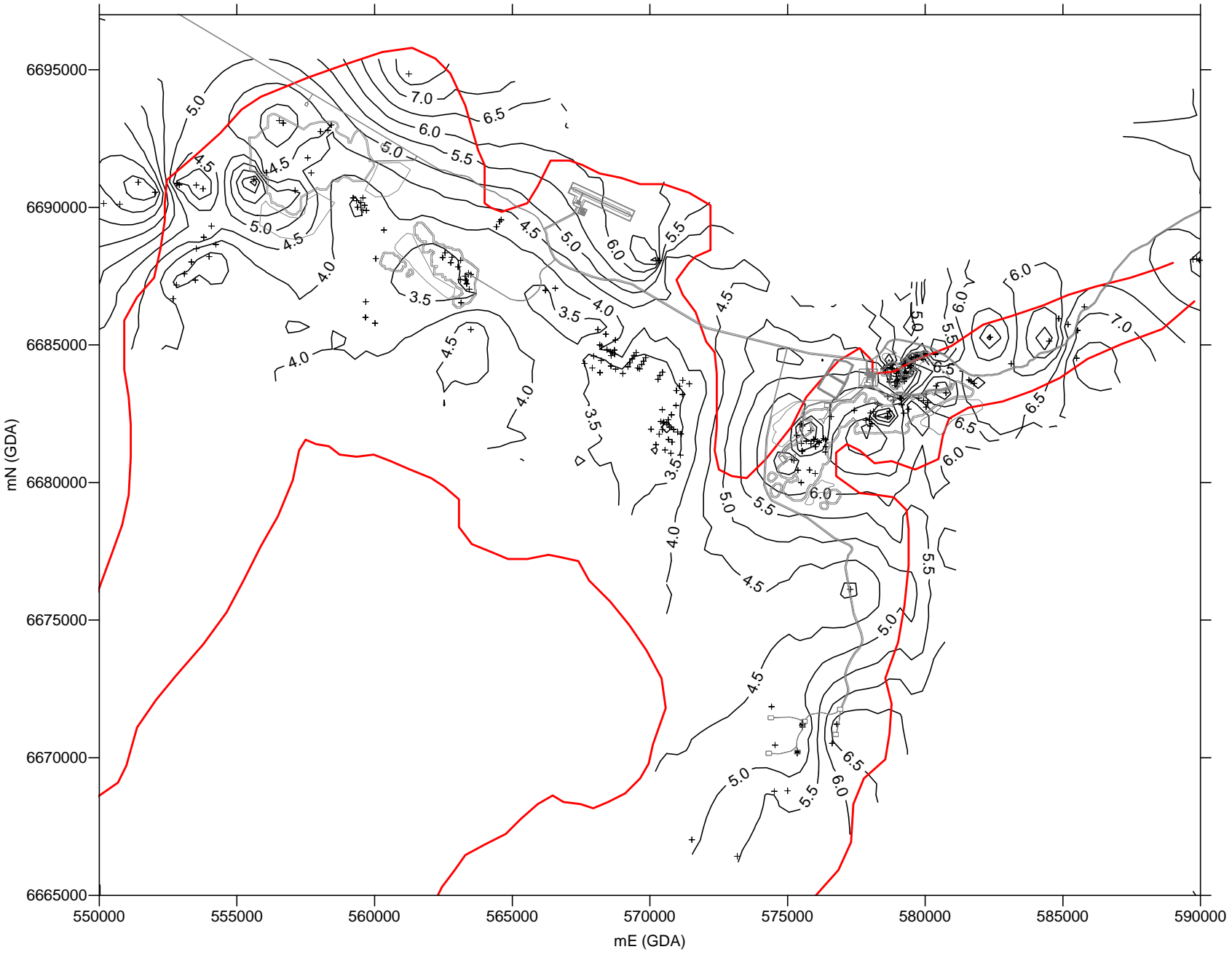
345-0/Surfer/15-02 Rev2.dwg Fig 10 salinity.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 Dwg No: 345.0/15/2-10

SALINITIES (mg/L TDS) MEASURED AT
 VARIOUS TIMES



Figure 10



345-01/urfer/15-02 Rev2d/fig11.pH.srf

CLIENT: Vimy Resources

PROJECT: Mulga Rock Hydrogeology

DATE: October 2015

Dwg No: 345.0/15/2-11

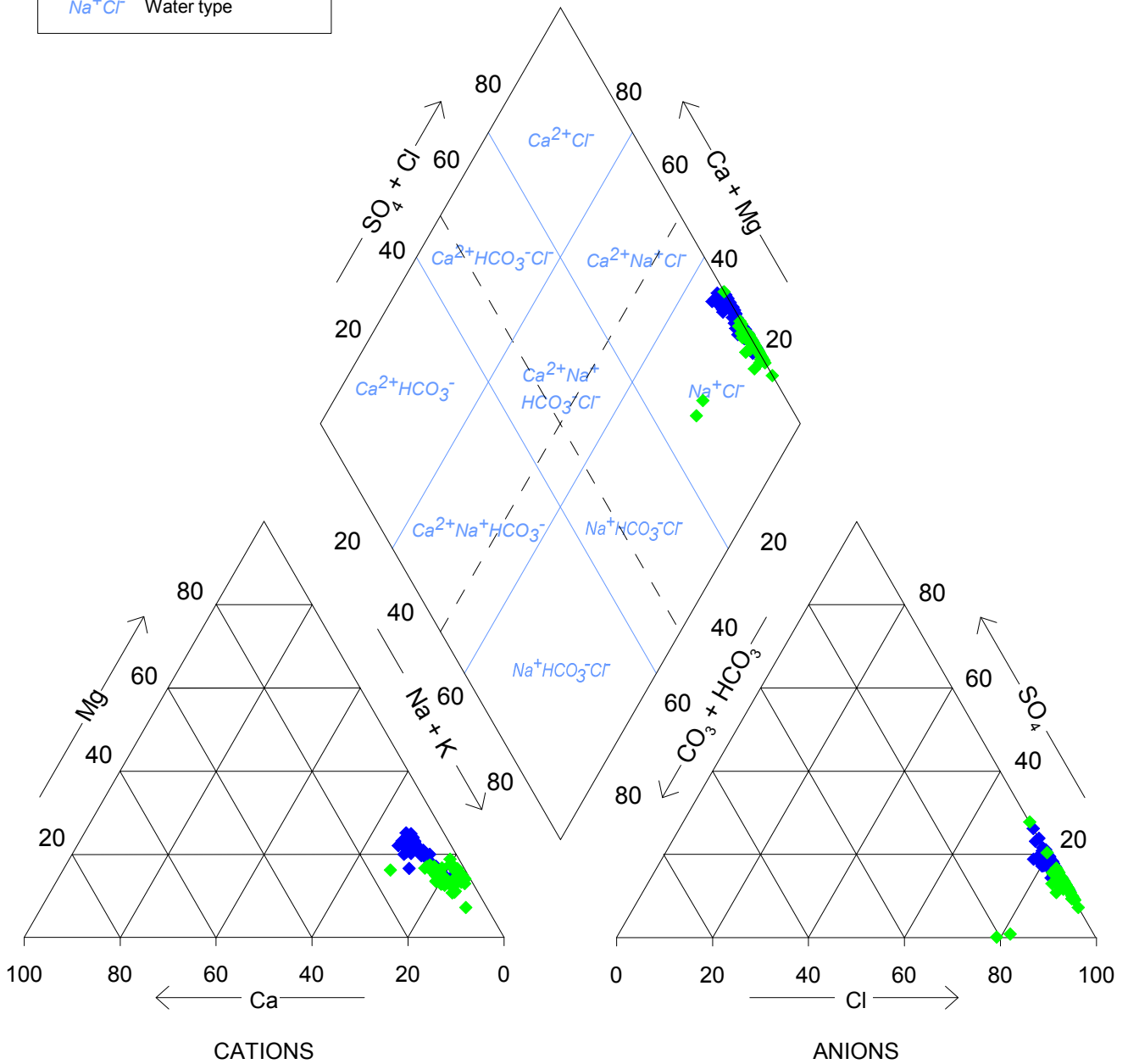
PH MEASURED AT VARIOUS TIMES

Figure 11

Figure 12

Legend

- ◆ Ambassador Sites
- ◆ Other Sites
- Na⁺Cl⁻ Water type



Piper Ambassador.grf

CLIENT: Vimy Resources Ltd
 PROJECT: Mulga Rock Hydrogeology
 DATE: May 2015
 Dwg. No: 345-0/15/02-12

**PIPER DIAGRAM
 OF GROUNDWATER SAMPLES
 MULGA ROCK DEPOSITS**



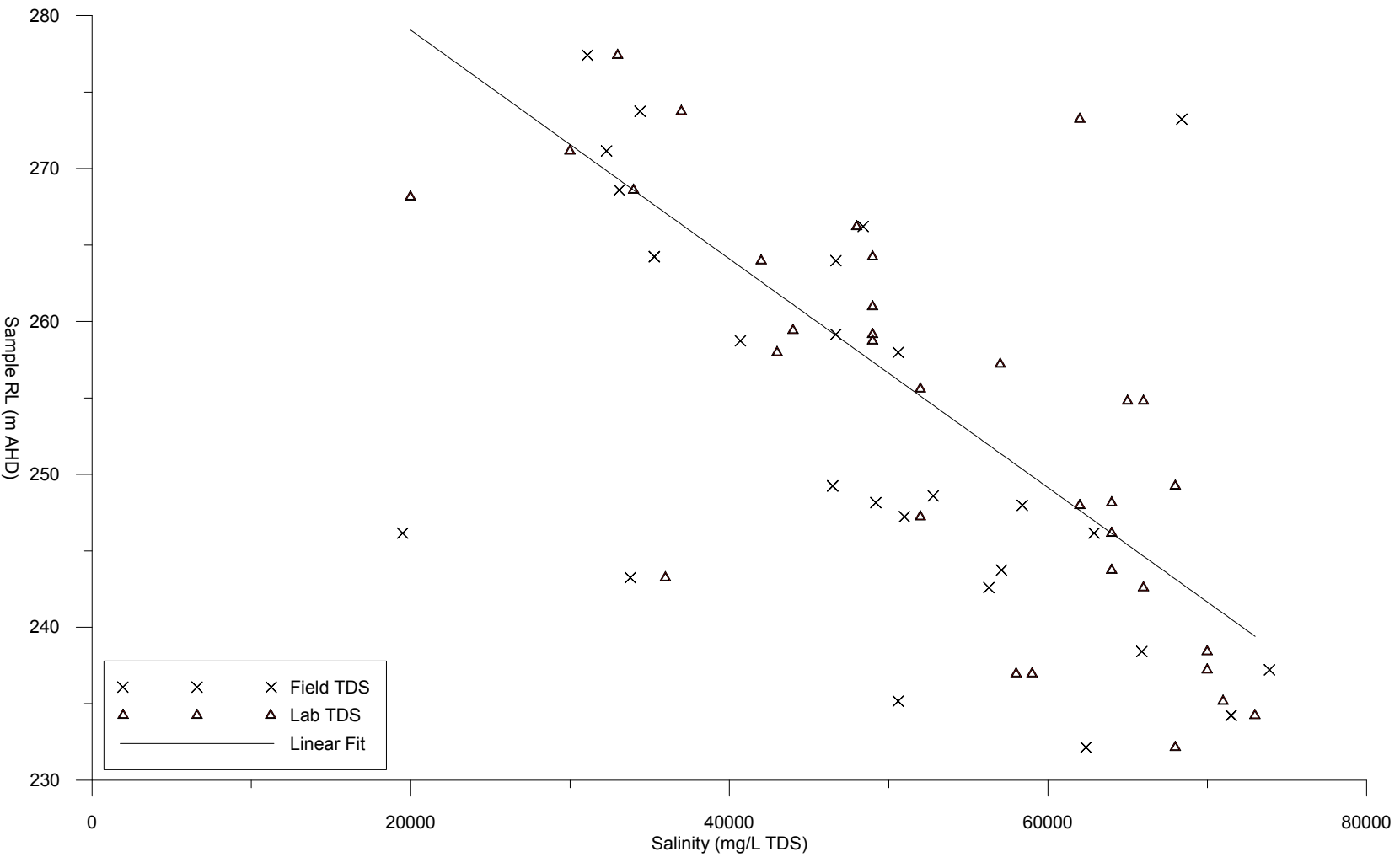


Figure 13

Injection_tds_vs_depth.grf

Client: Vimy Resources

Project: Mulga Rock

Date: May 2015

Dwg. No: 345-0/15/2-13

REINJECTION AREA: SALINITY VERSUS

SAMPLING DEPTH

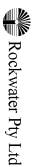
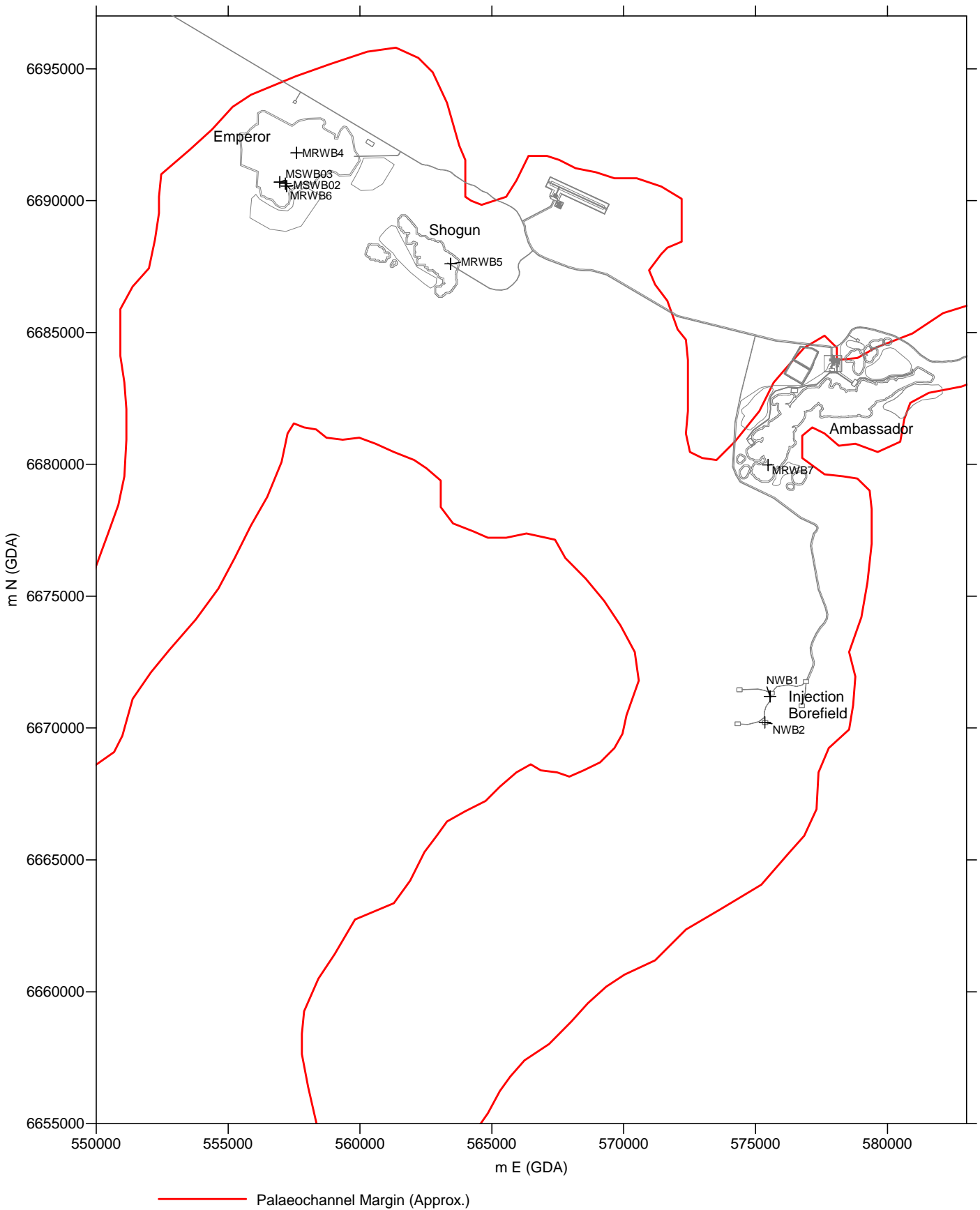


Figure 14

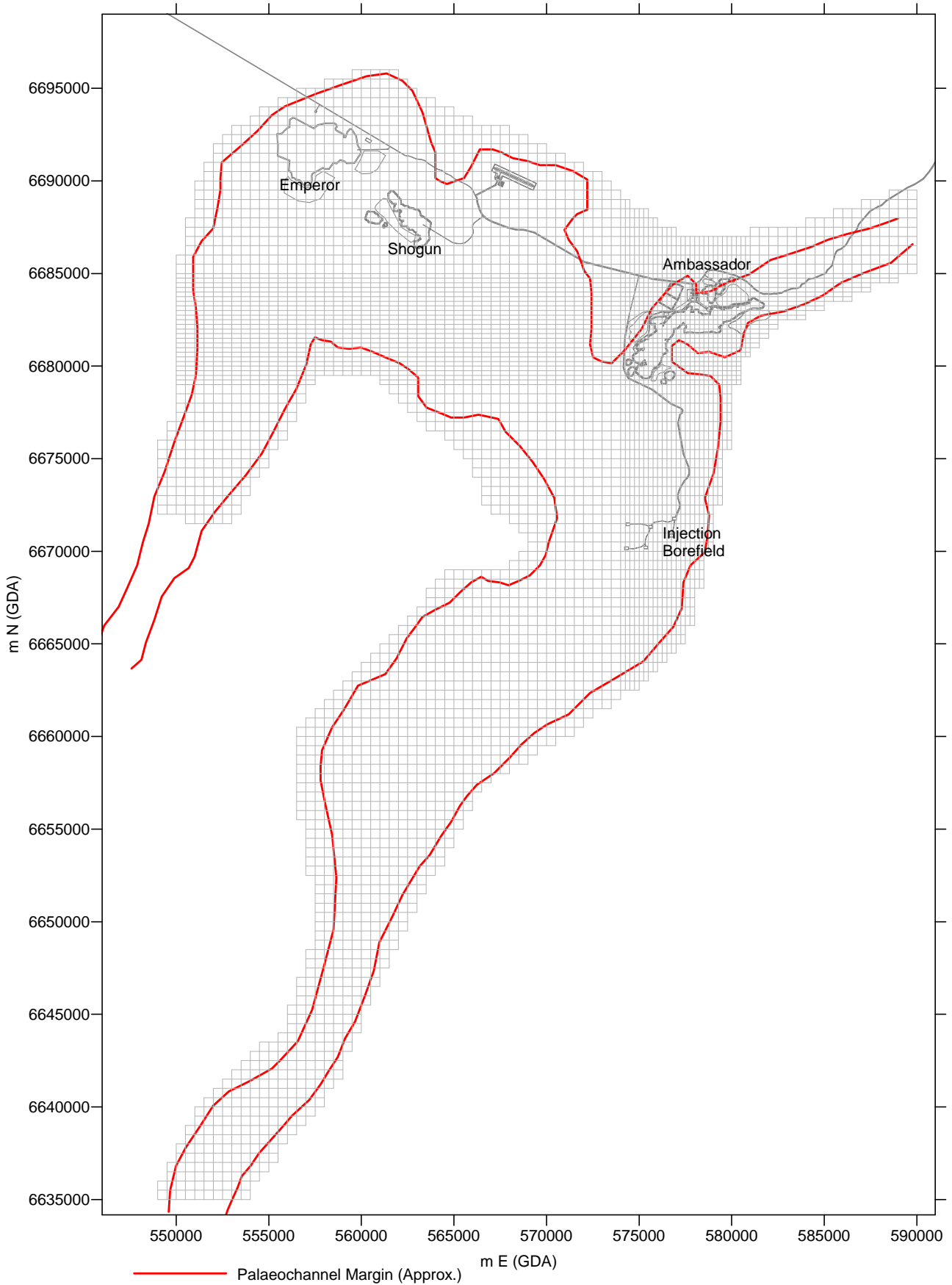


345-0/Surfer/15-02 Rev2d/FIG14. production bores.srf

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-14

PRODUCTION BORE LOCATIONS

Figure 15

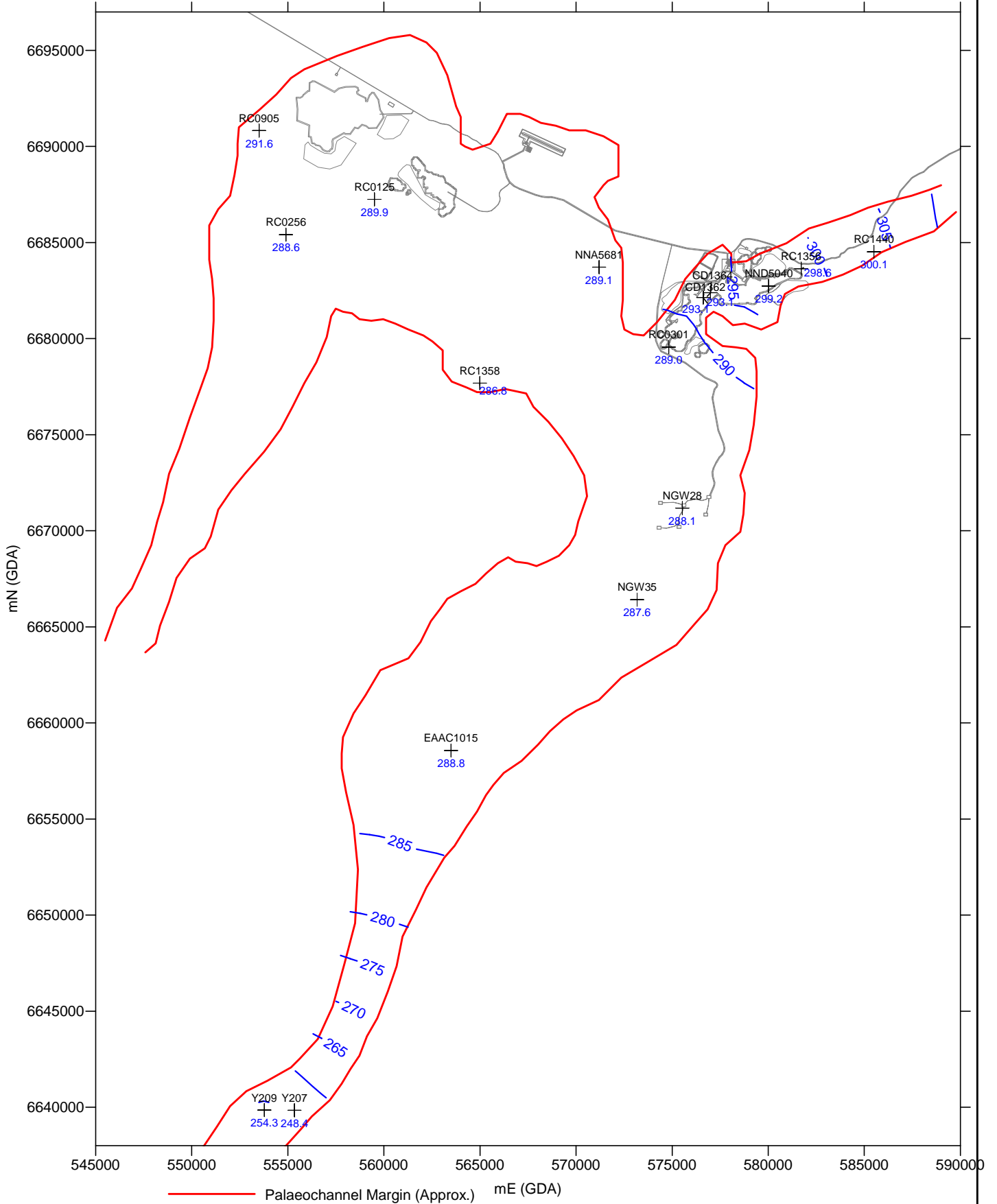


345-0/Surfer/15-02 Rev2d/FIG15.model grid.srf

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-15

MODEL GRID

Figure 16

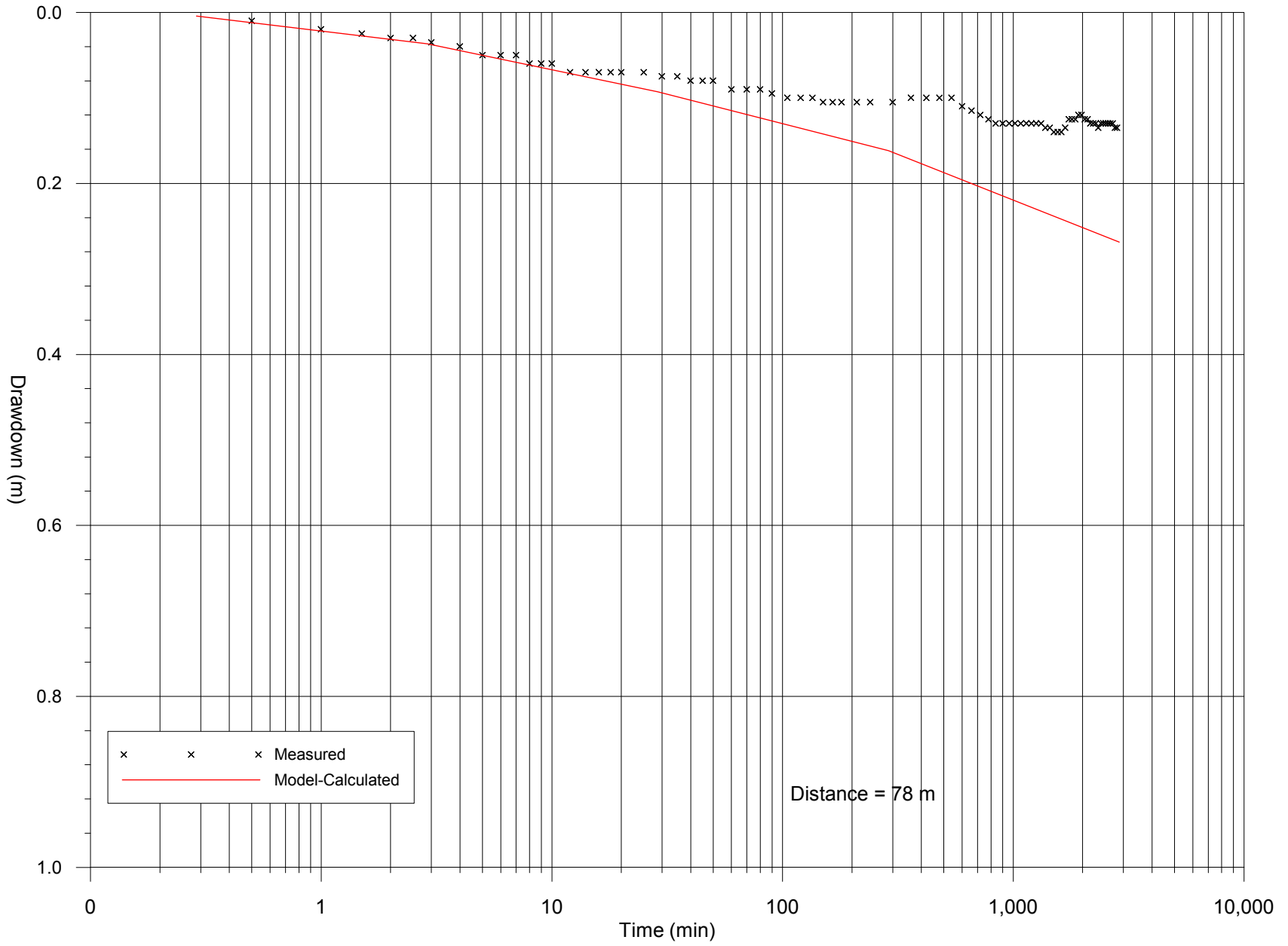


345.0/Surfer/15-02 Rev2d/FIG16. ss calib results.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 Dwg No: 345.0/15/2-16

COMPARISON BETWEEN GROUNDWATER LEVELS (m AHD)
 MEASURED AT VARIOUS TIMES (POST VALUES),
 AND MODEL-CALCULATED LEVELS (CONTOURS)

Figure 17



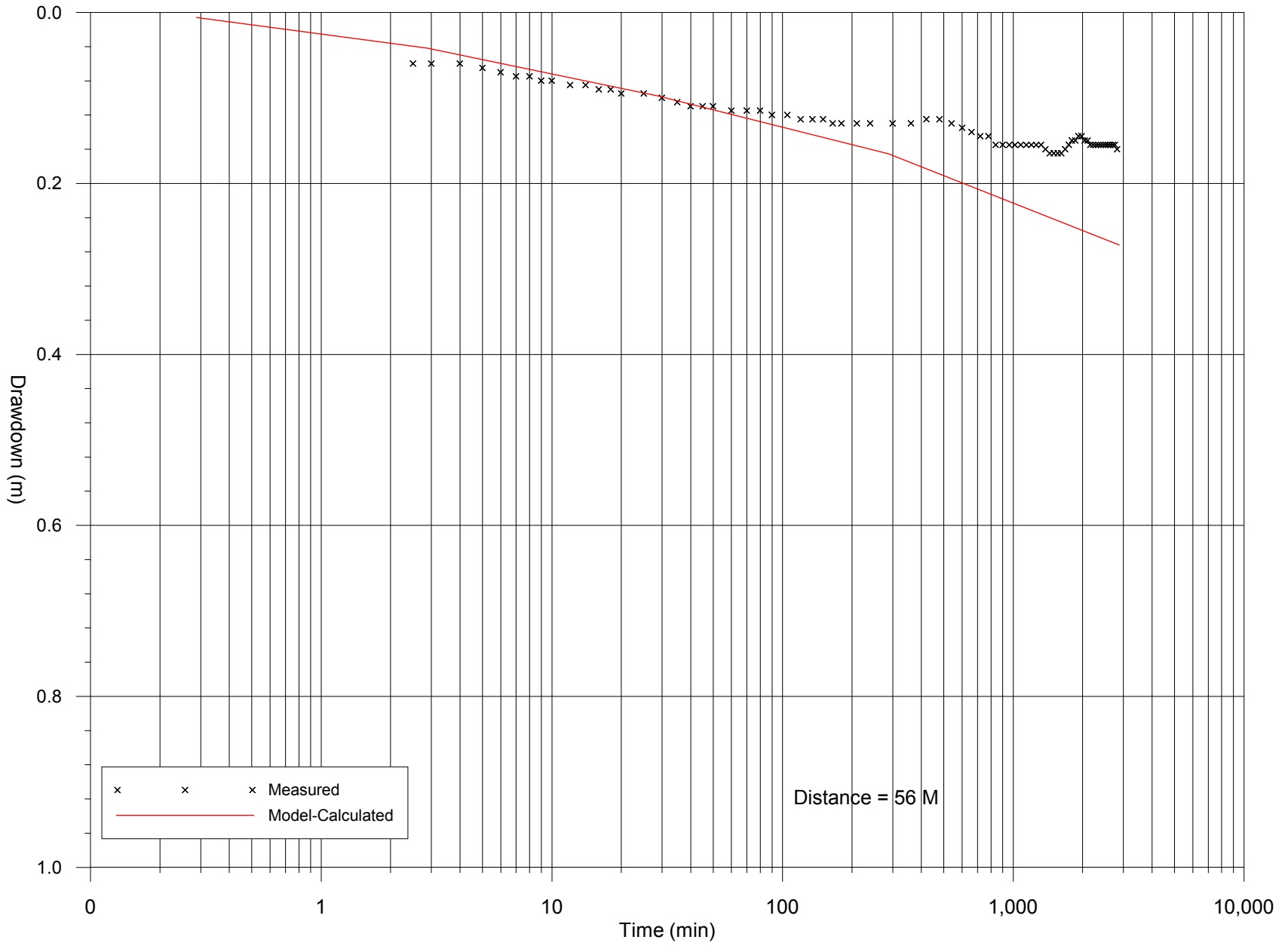
nbw1 ngw37.grf

Client: Vimy Resources
Project: Mulga Rock Hydrogeology
Date: March 2015
Dwg. No: 345-0/15/1-17

BORE NBW1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
DRAWDOWNS IN NGW37



Figure 18



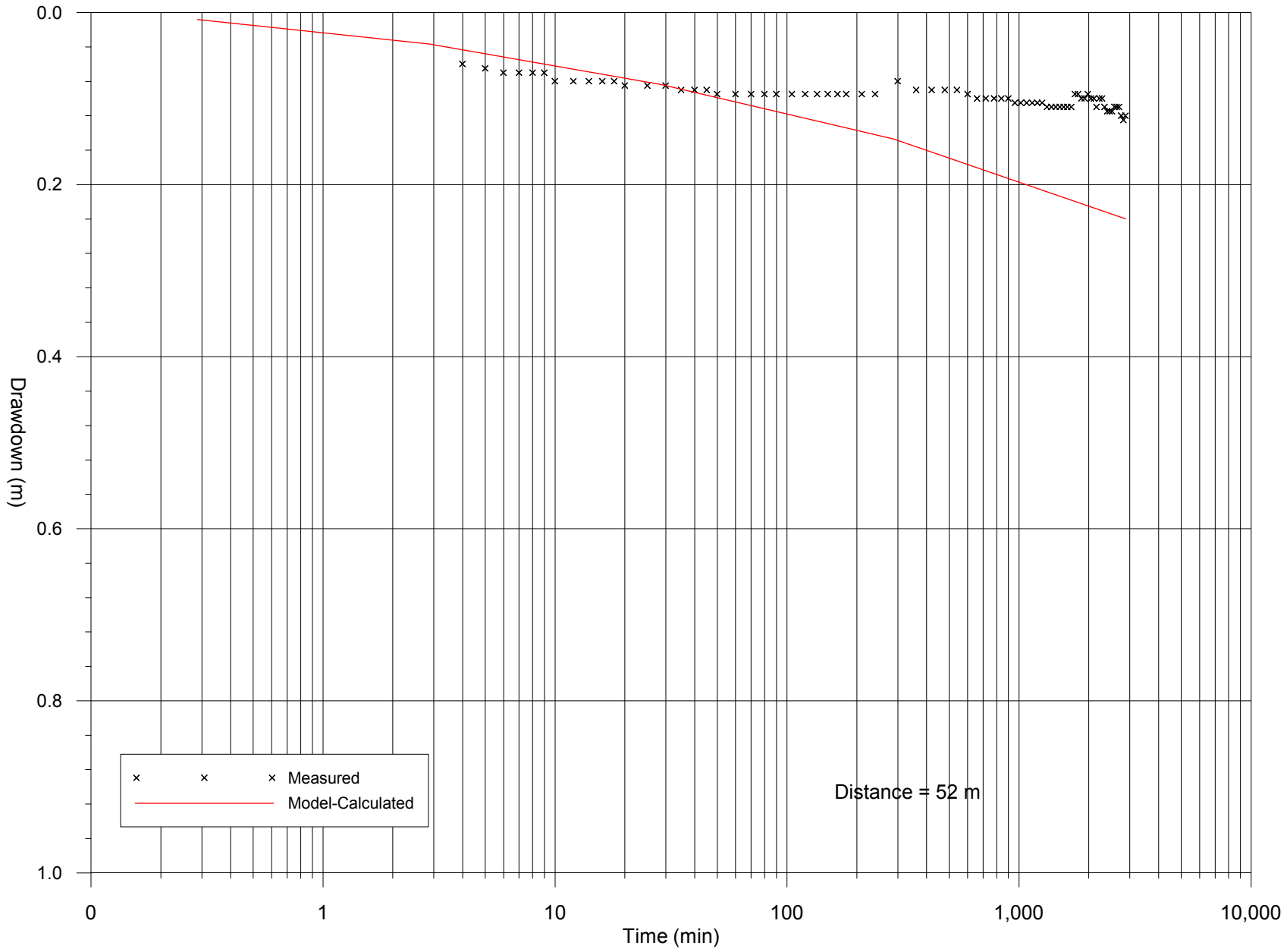
nbw1 ngw54c.grf

Client: Vimy Resources
Project: Mulga Rock Hydrogeology
Date: March 2015
Dwg. No: 345-0/15/1-18

BORE NBW1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
DRAWDOWNS IN NGW54C



Figure 19



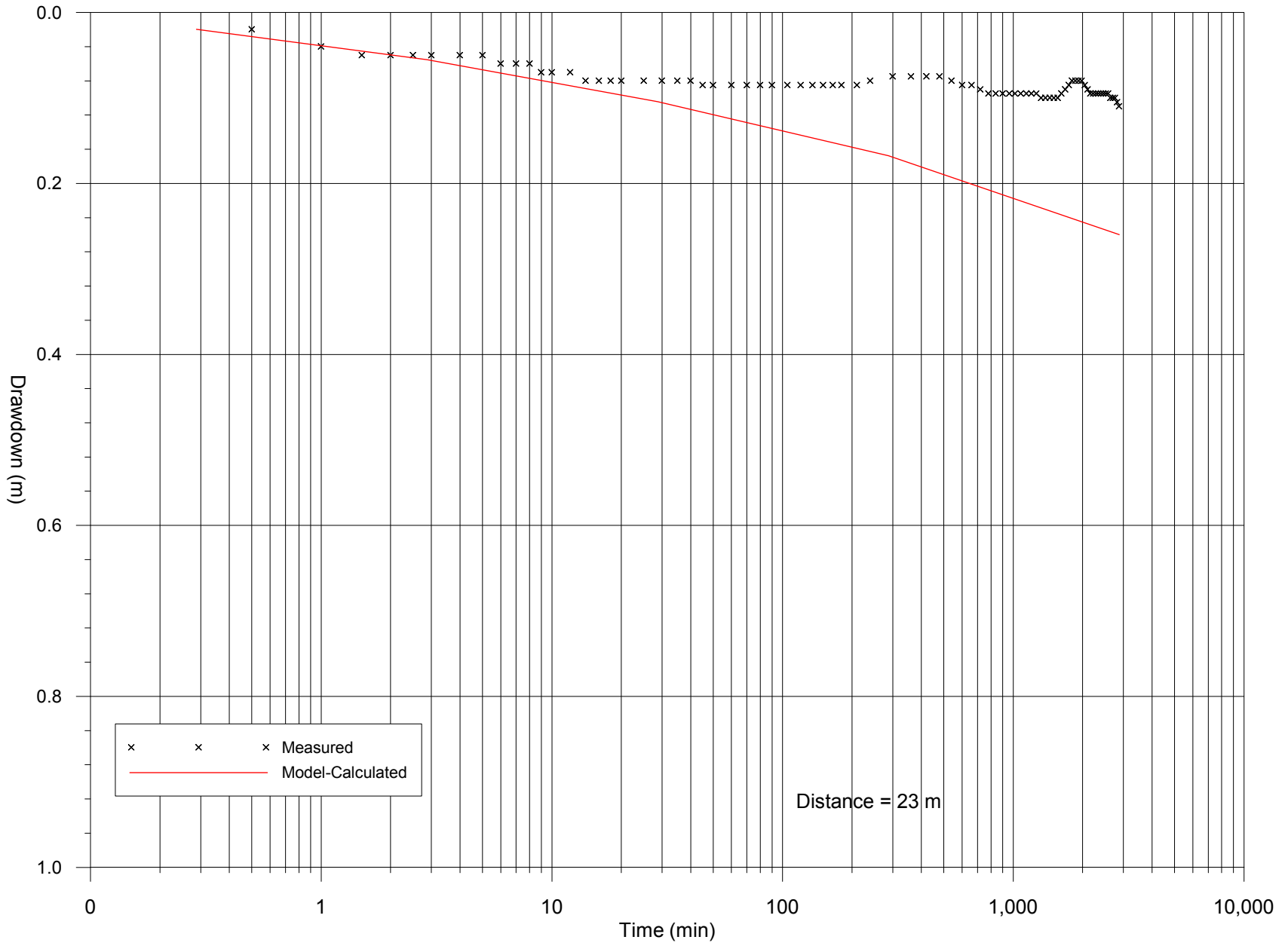
nbw2 ngw30.grf

Client: Vimy Resources
Project: Mulga Rock Hydrogeology
Date: March 2015
Dwg. No: 345-0/15/1-19

BORE NBW2 PUMPING TEST
AT 950 KL/d, 13/3/15
DRAWDOWNS IN NGW30



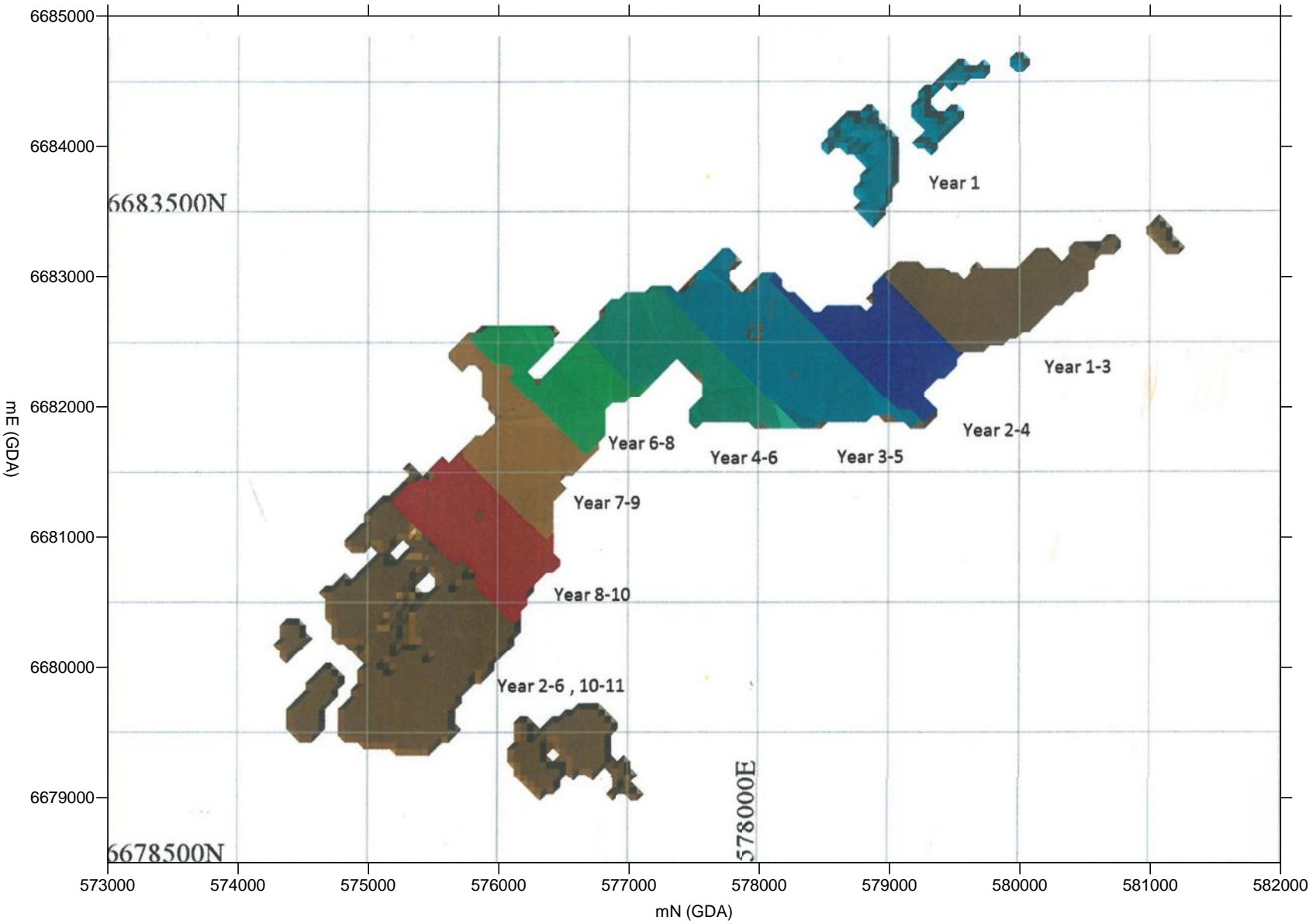
Figure 20



nbw2_ngw55.grf
Client: Vimy Resources
Project: Mulga Rock Hydrogeology
Date: March 2015
Dwg. No: 345-0/15/1-20

BORE NBW2 PUMPING TEST
AT 950 KL/d, 13/3/15
DRAWDOWNS IN NGW55





345-0/Surfer/15-02 Rev2c/Fig21_Mining Areas Y1-Y11.srf

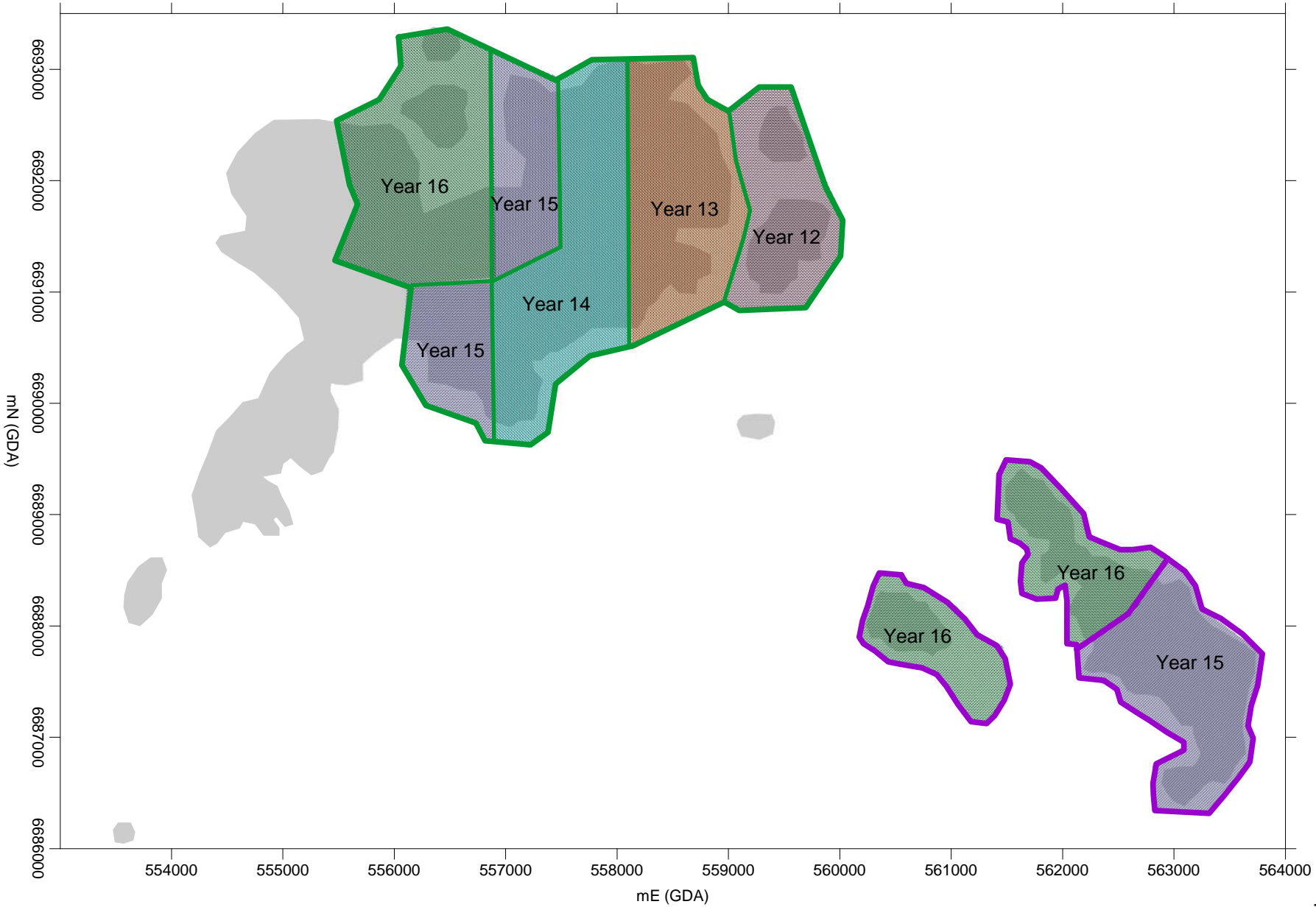
CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 DWG No: 345.0/15/2-21

MINE PLAN, AMBASSADOR AND
 PRINCESS DEPOSITS



Figure 21

Figure 22



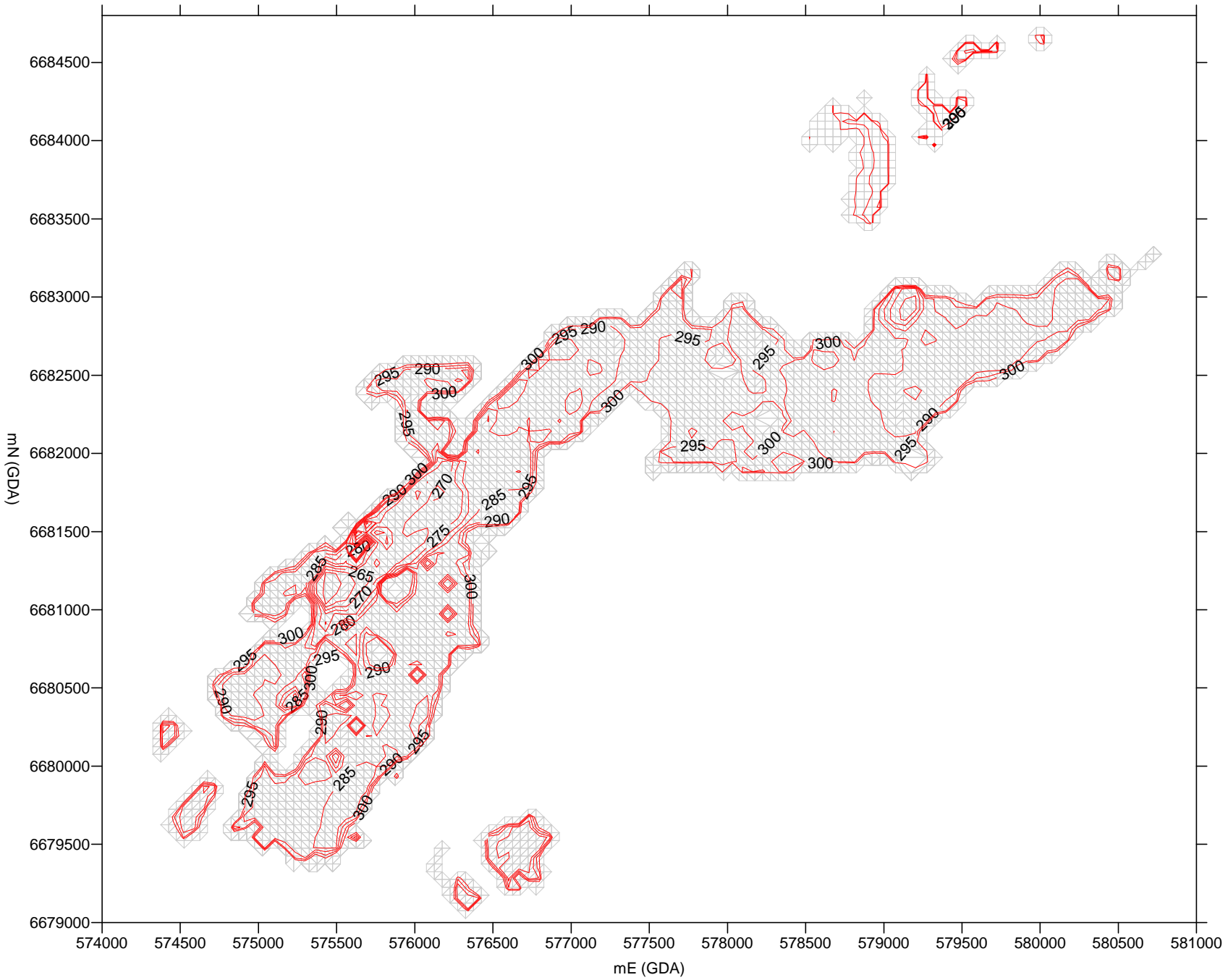
345-0/Surfer/15-02 Rev2c/Fig22: Mining Areas Y12-Y16.srf

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-22

MINE PLAN,
EMPEROR AND SHOGUN DEPOSITS



Rockwater Pty Ltd



345-0/Surfer/15-02 Rev23/fig23: mining base.srf

CLIENT: Vimy Resources

PROJECT: Mulga Rock Hydrogeology

DATE: October 2015

DWG No: 345.0/15/2-23

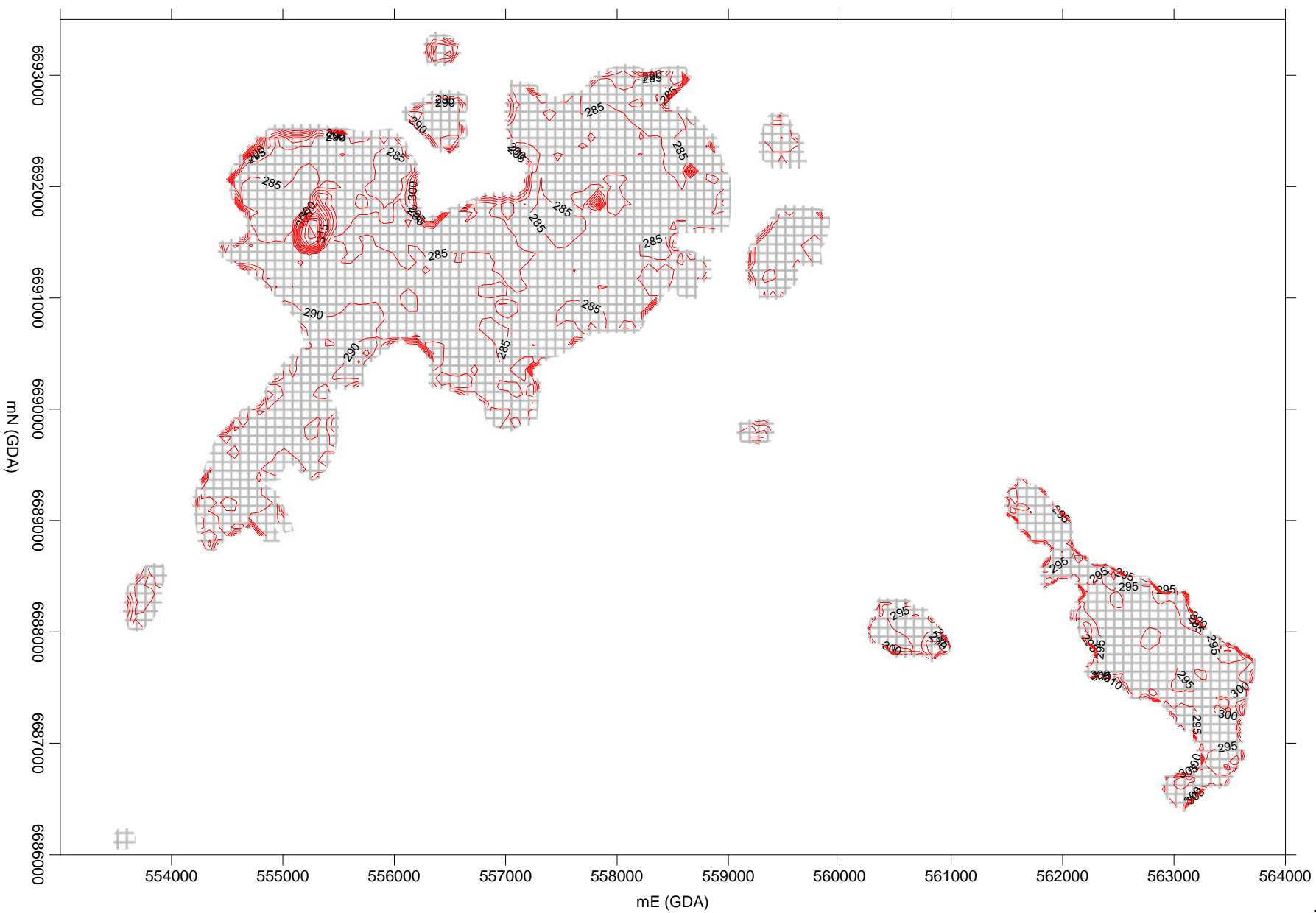
PLANNED BASE OF MINING (m AHD),
 AMBASSADOR AND PRINCESS DEPOSITS



Rockwater Pty Ltd

Figure 23

Figure 24



345-0/Surfer/15-02 Rev2c/Fig24_mining base1.srf

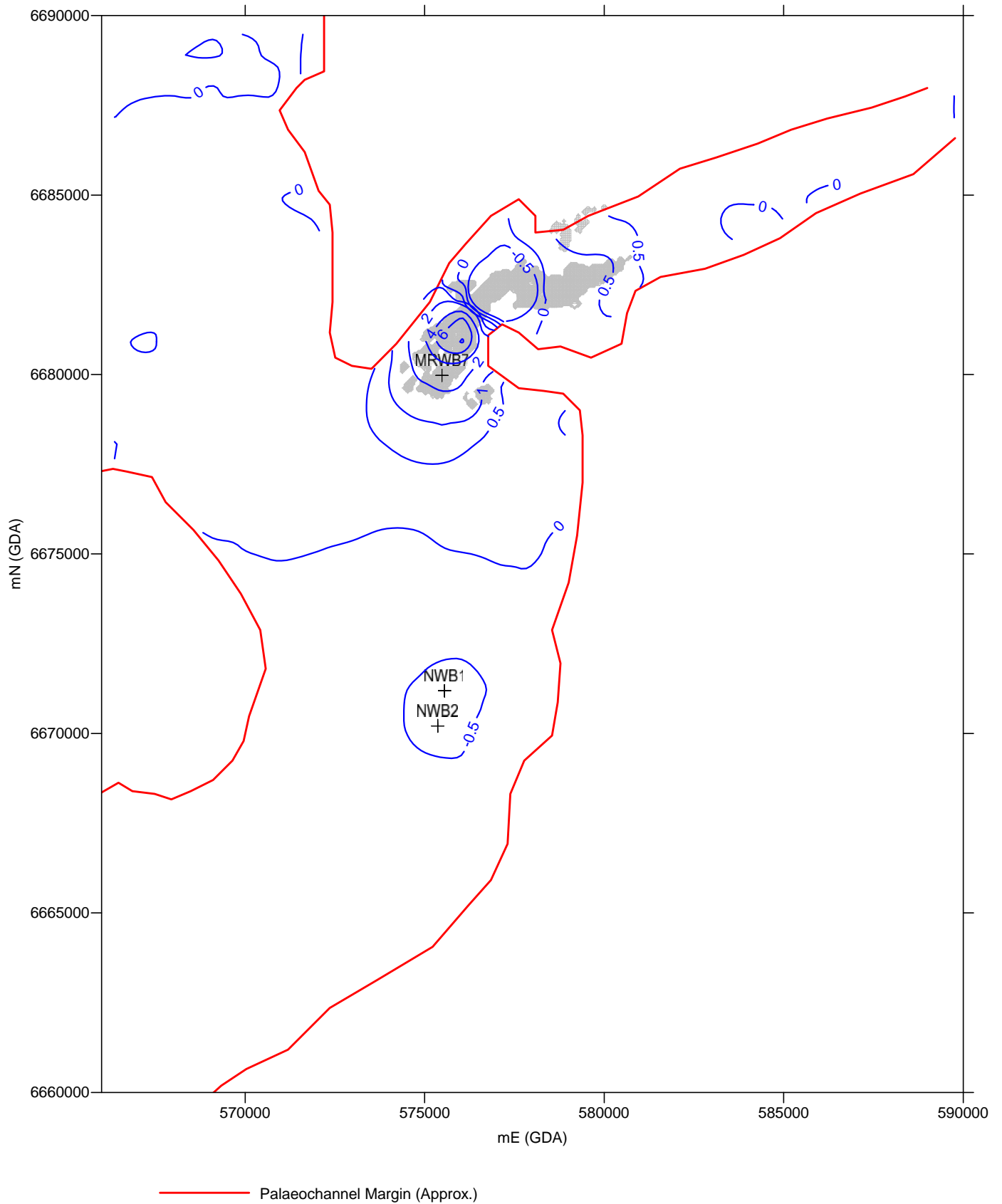
CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-24

PLANNED BASE OF MINING (m AHD),
EMPEROR AND SHOGUN DEPOSITS



Rockwater Pty Ltd

Figure 25

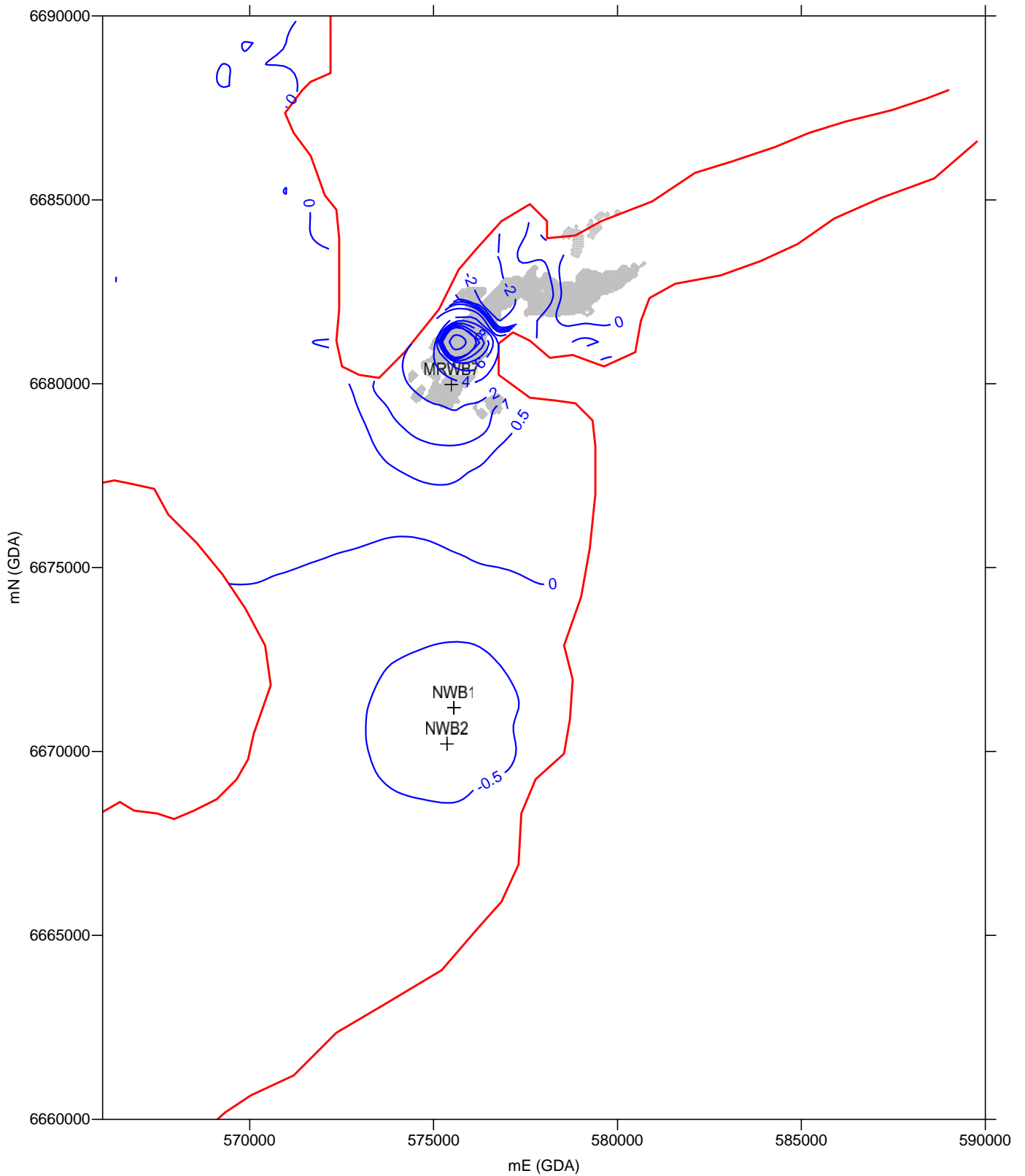


345-0/Surfer/15-02 Rev2c/FIG25. L1Y10DD.srf

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-25

MODEL-CALCULATED DRAWDOWNS (m)
LAYER 1, END OF YEAR 10

Figure 26



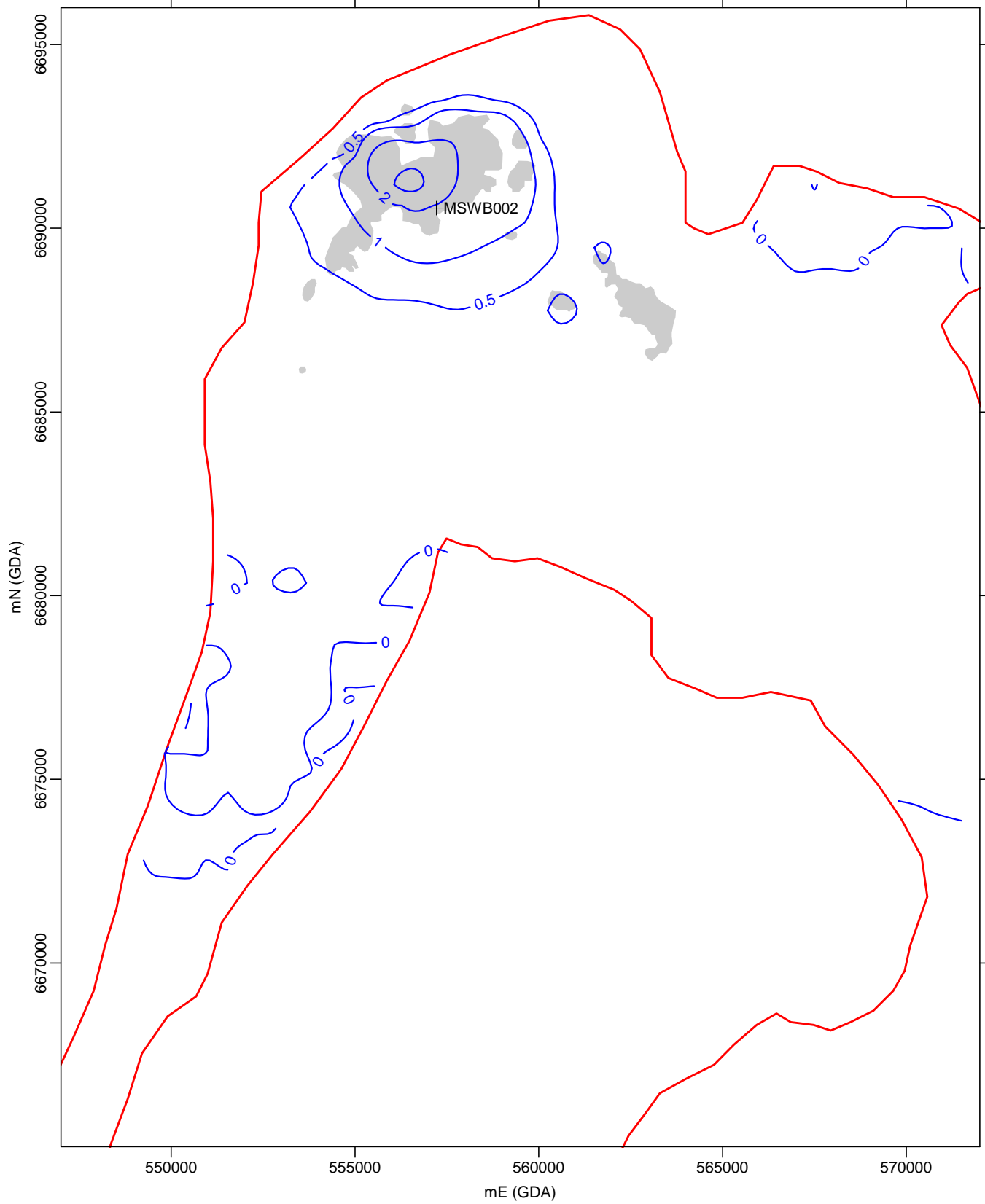
— Palaeochannel Margin (Approx.)

345-0/Surfer/15-02 Rev2c/FIG26. L3Y10DD.srf

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-26

MODEL-CALCULATED DRAWDOWNS (m)
LAYER 3, END OF YEAR 10

Figure 27



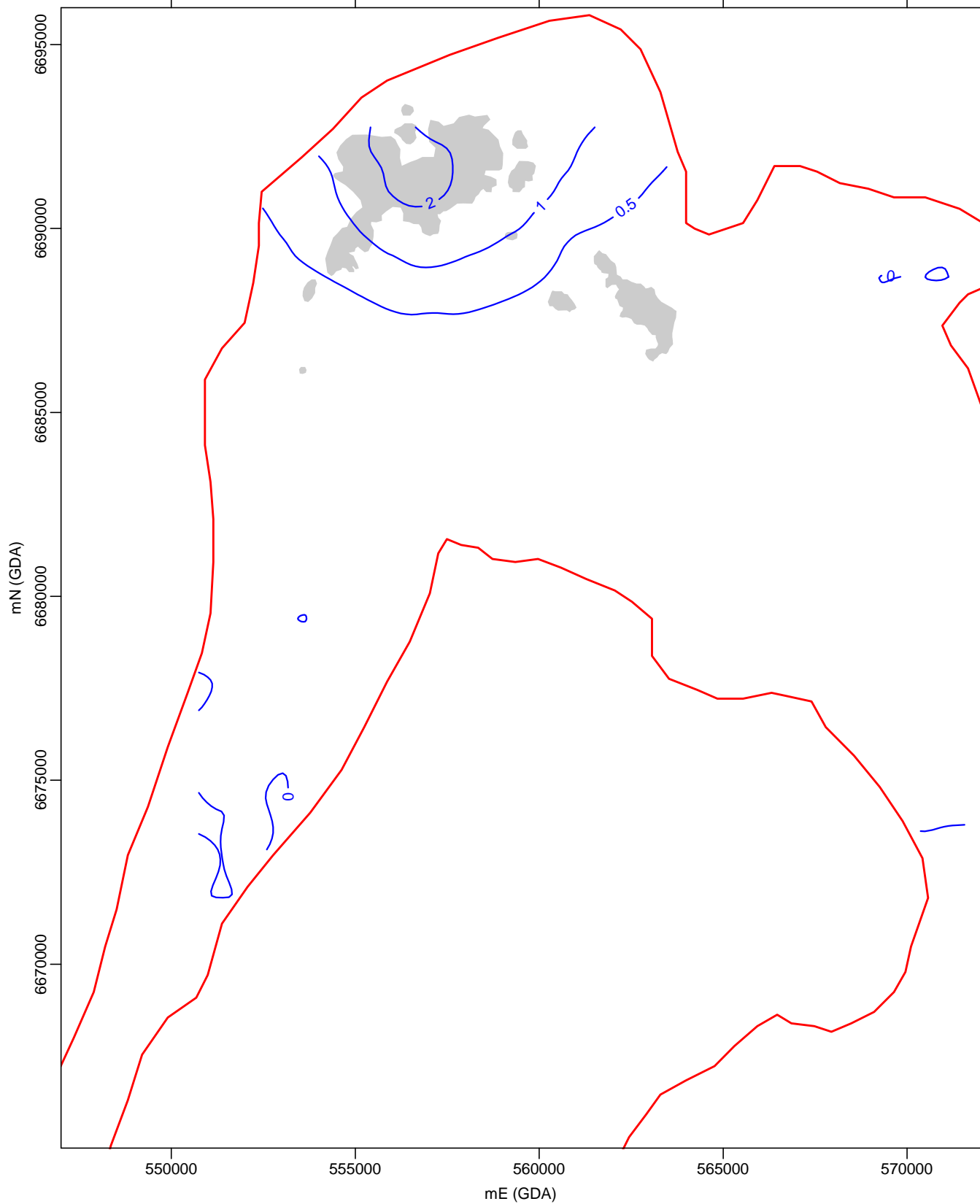
— Palaeochannel Margin (Approx.)

345-0/Surfer/15-02 Rev2c/Fig27. L1Y16DD

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-27

MODEL-CALCULATED DRAWDOWNS (m)
LAYER 1, END OF YEAR 16

Figure 28



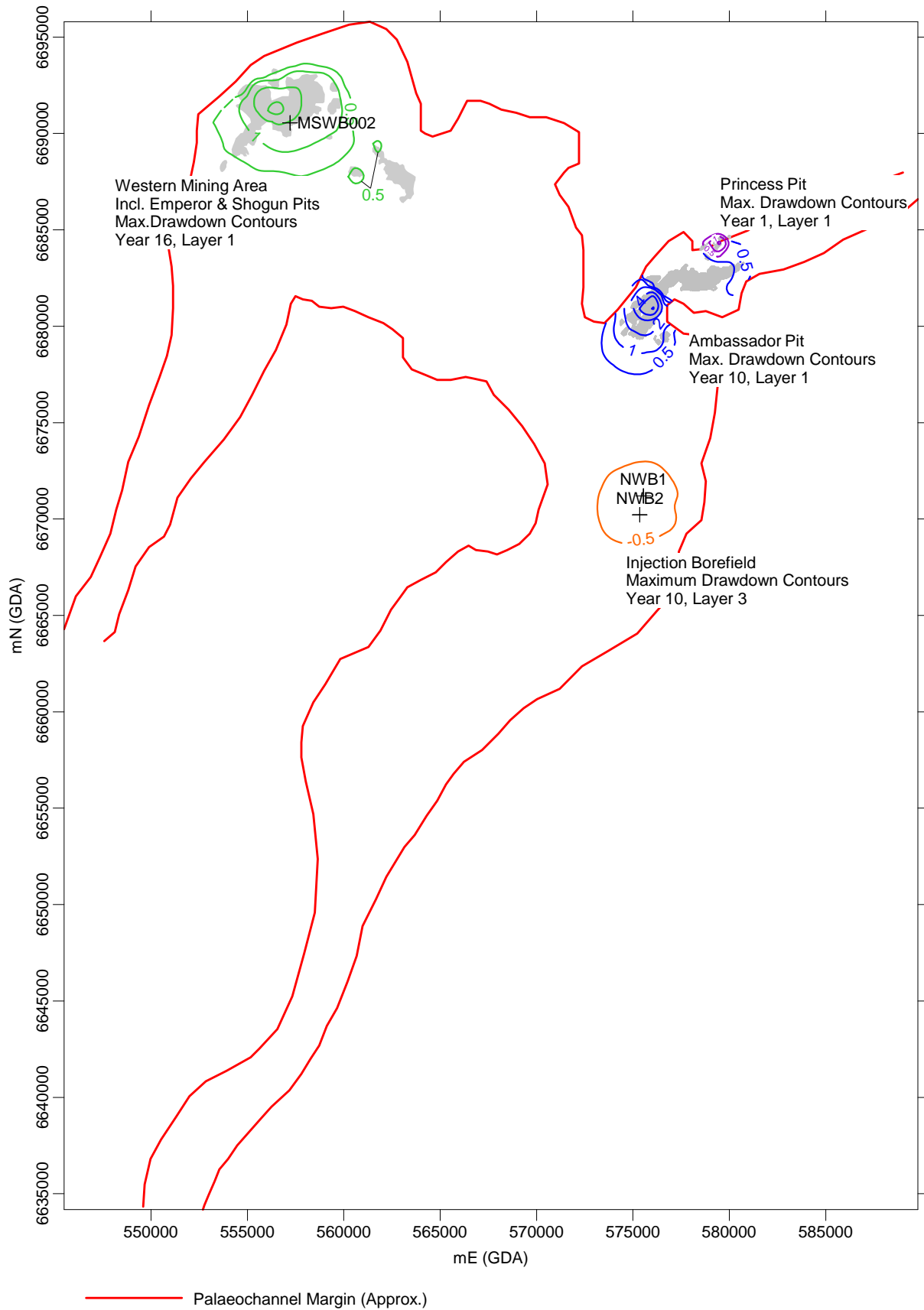
— Palaeochannel Margin (Approx.)

345-0/Surfer/15-02 Rev2c/Fig28. L3Y16DD

CLIENT: Vimy Resources
PROJECT: Mulga Rock Hydrogeology
DATE: October 2015
Dwg No: 345.0/15/2-28

MODEL-CALCULATED DRAWDOWNS (m)
LAYER 3, END OF YEAR 16

Figure 29

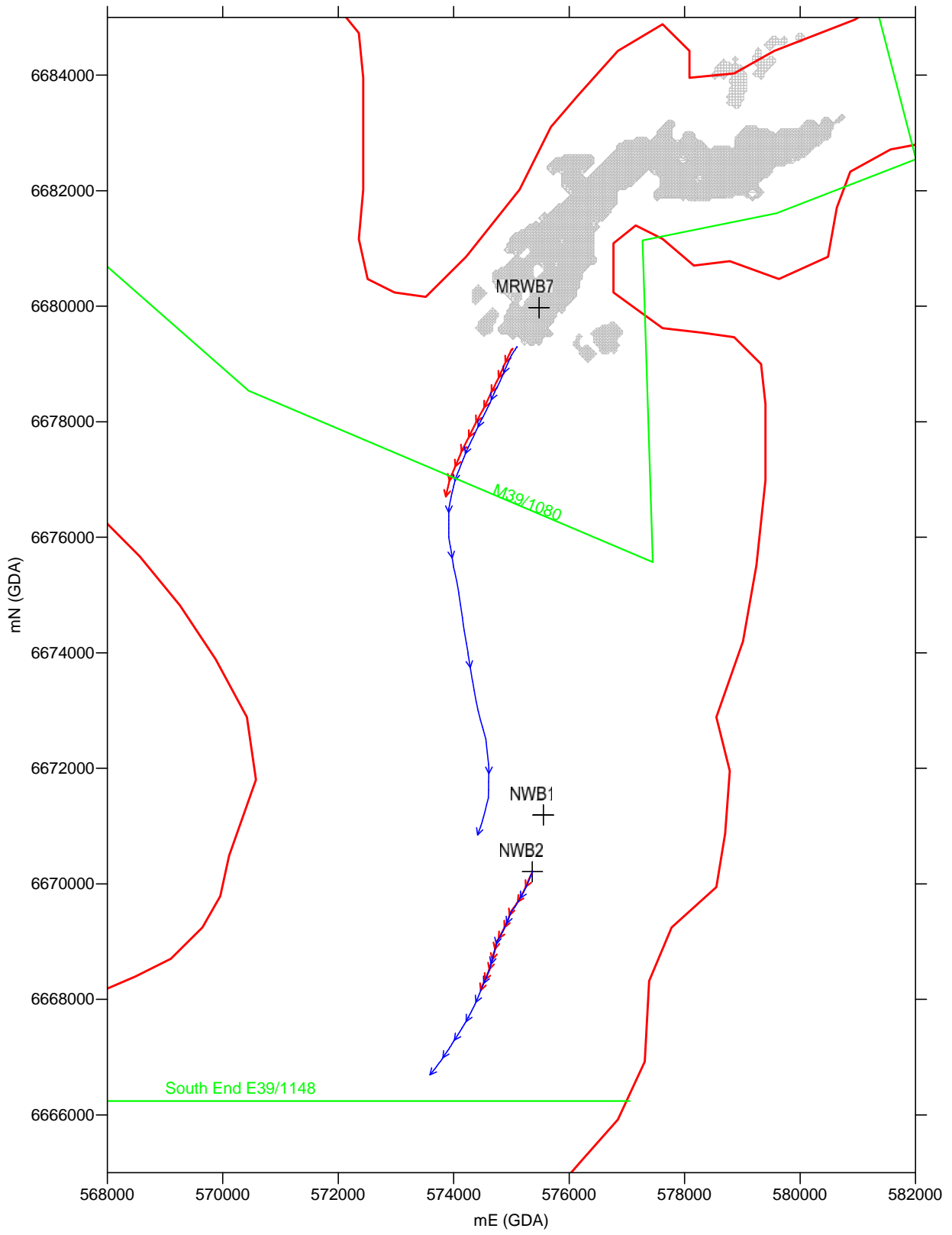


345-0/Surfer/Rpt 15-002 Rev2c/FIG29. Max DD & Mounding.srf

CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 Dwg No: 345.0/15/2-29

MODEL-CALCULATED
 MAXIMUM DRAWDOWNS (m)
 DURING 16 YEAR LoM

Figure 30



- ← Adopted Case
- ← Worst Case

Each Arrow-Head Represents 100 Years Flow
(1,000 Years Total Flow Shown)

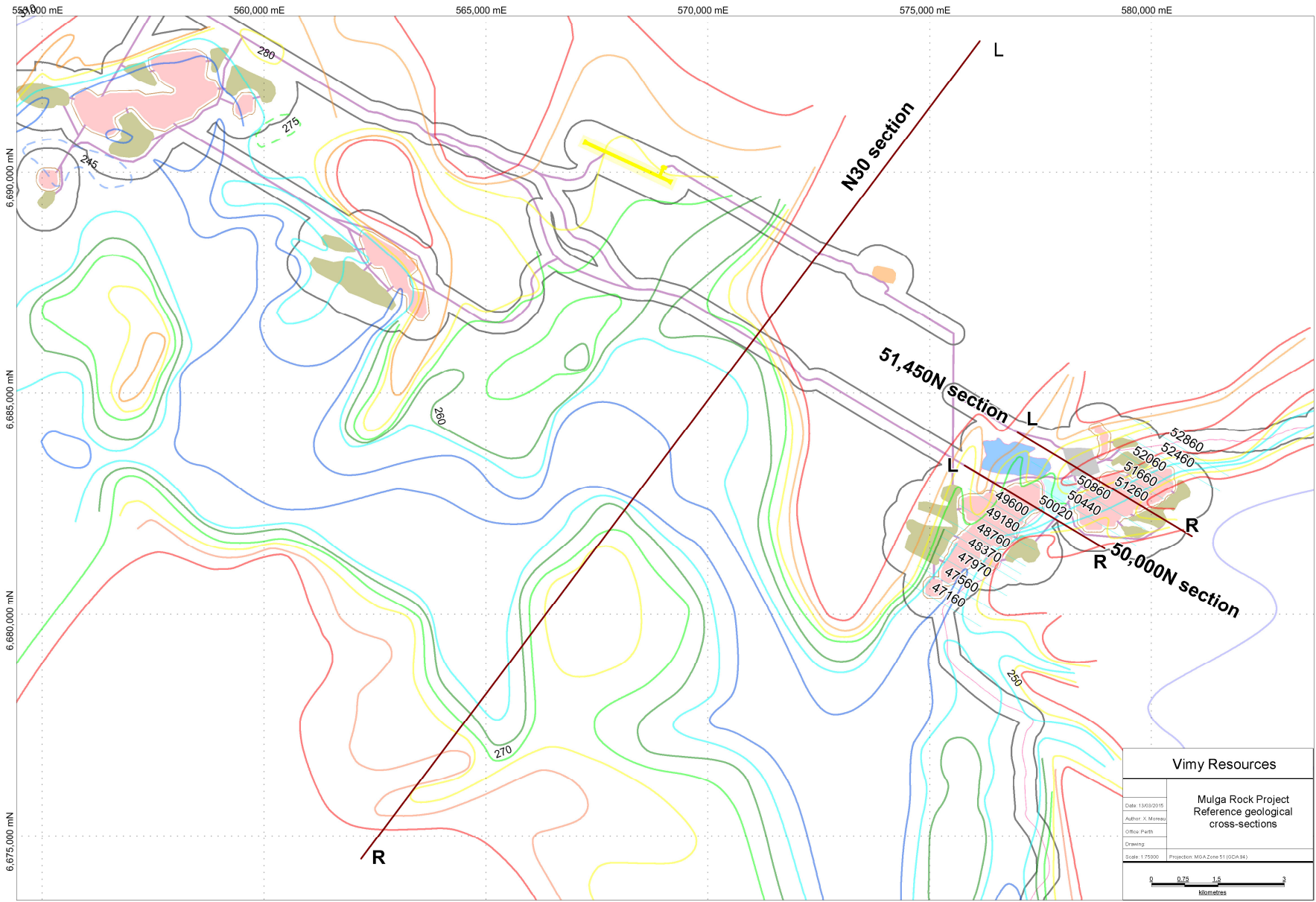
Surfer/15-02 Rev2c/Fig30. Flowpaths2.srf

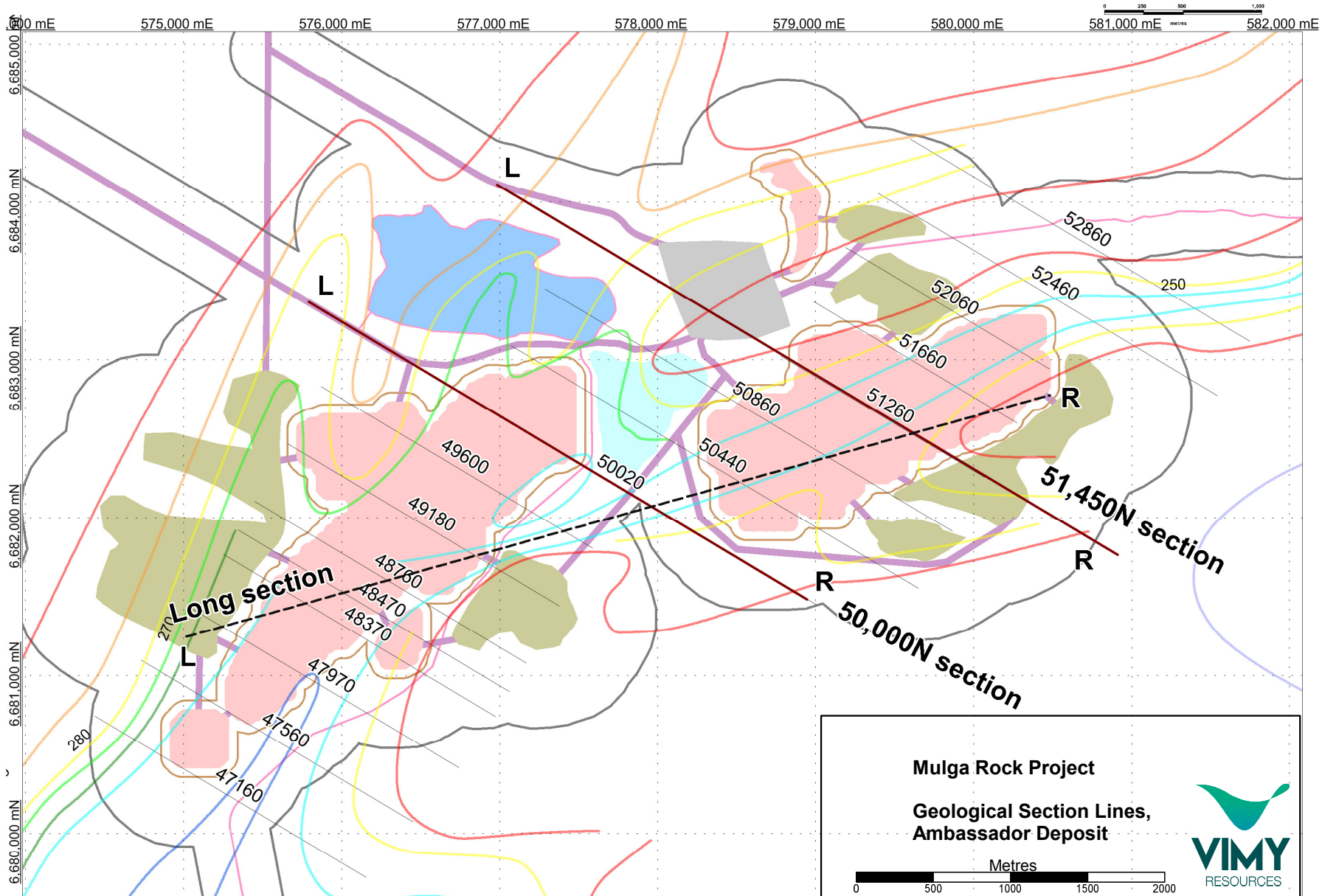
CLIENT: Vimy Resources
 PROJECT: Mulga Rock Hydrogeology
 DATE: October 2015
 Dwg No: 345.0/15/2-30

MODEL-CALCULATED FLOWPATHS
 FOR 1,000 YEARS FROM
 THE END OF MINING (LAYER 3)

APPENDIX I
GEOLOGICAL SECTIONS

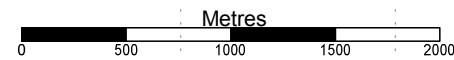




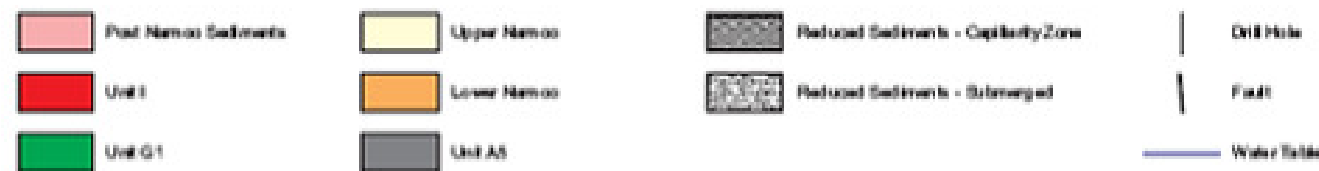
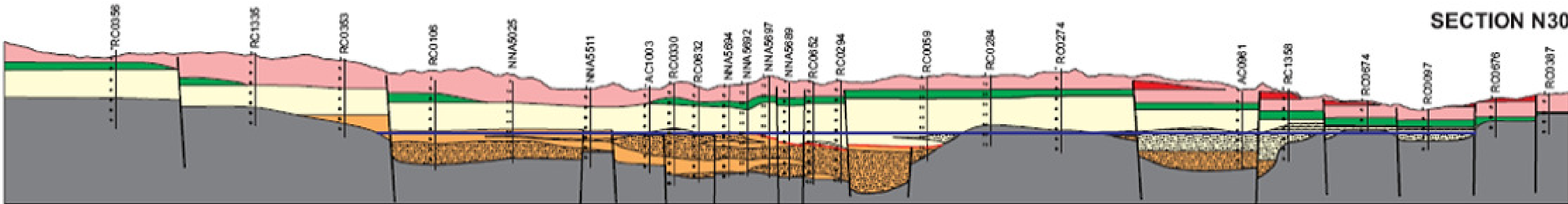


Mulga Rock Project

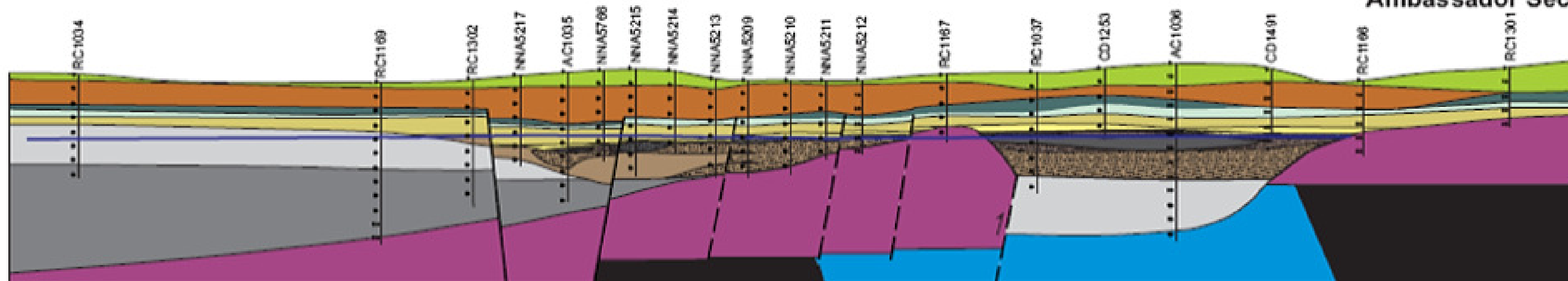
Geological Section Lines,
Ambassador Deposit



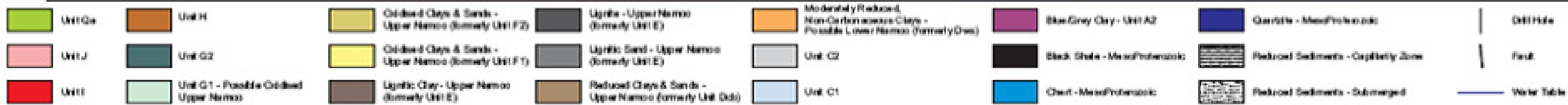
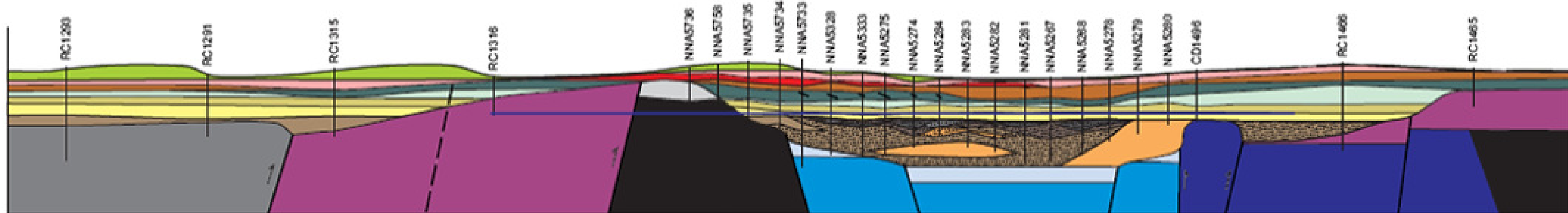
SECTION N30

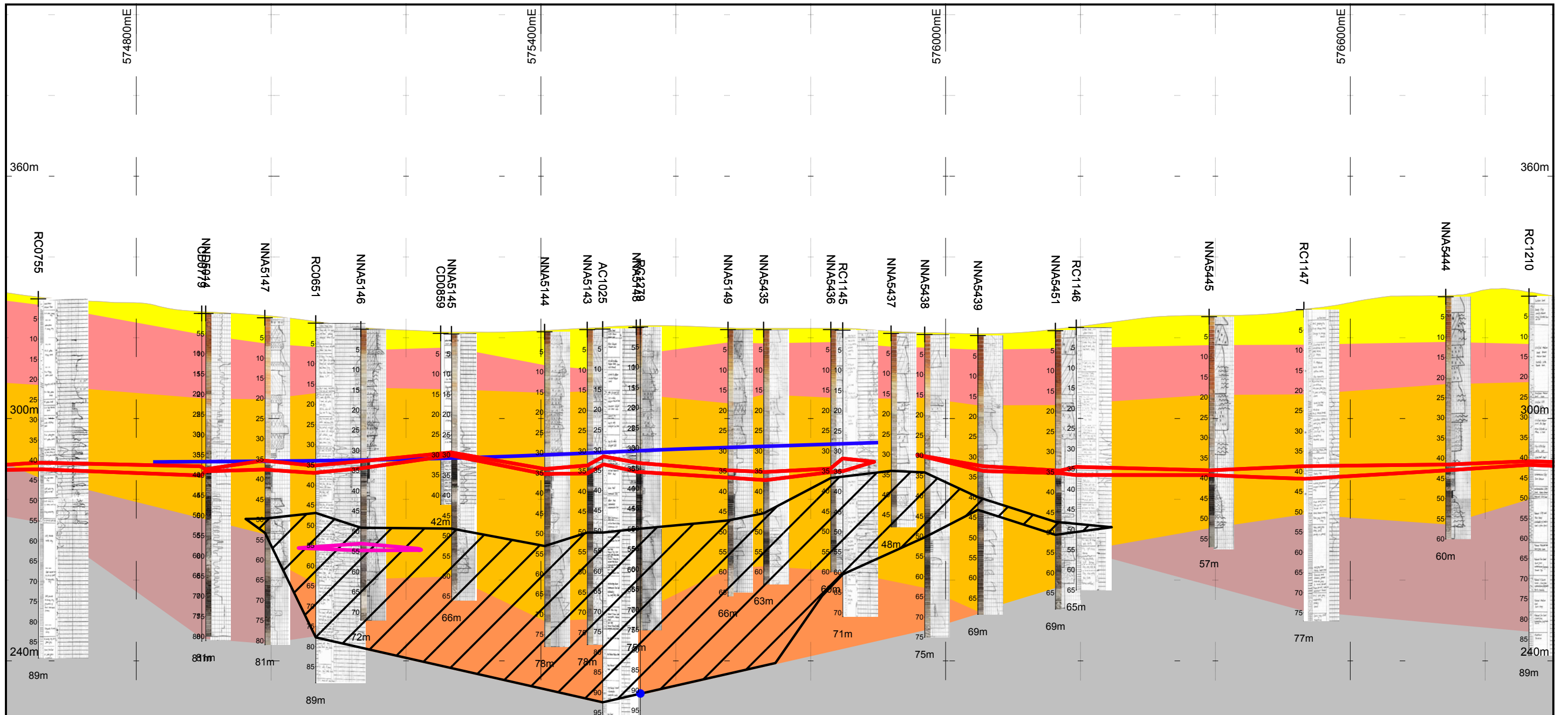


Ambassador Section 50,000N



Ambassador Section 51,450N





- Legend**
- Quaternary Aeolian Sands
 - Miocene Coastal Sand
 - Late Eocene Paleochannel Sediments
 - Mid-Late Eocene Sediments (Incised)
 - Cretaceous Tillites & Carbonaceous Sediments
 - Meso Proterozoic Meta-Sediments
 - Permian Glacio-Lacustrine
 - Uranium Mineralisation - Domain 100
 - Uranium Mineralisation - Domain 200
 - Uranium Mineralisation - Domain 300
 - Uranium Mineralisation - Domain 400
 - Transmissive Sands
 - Measured Water Table
 - Major Fault

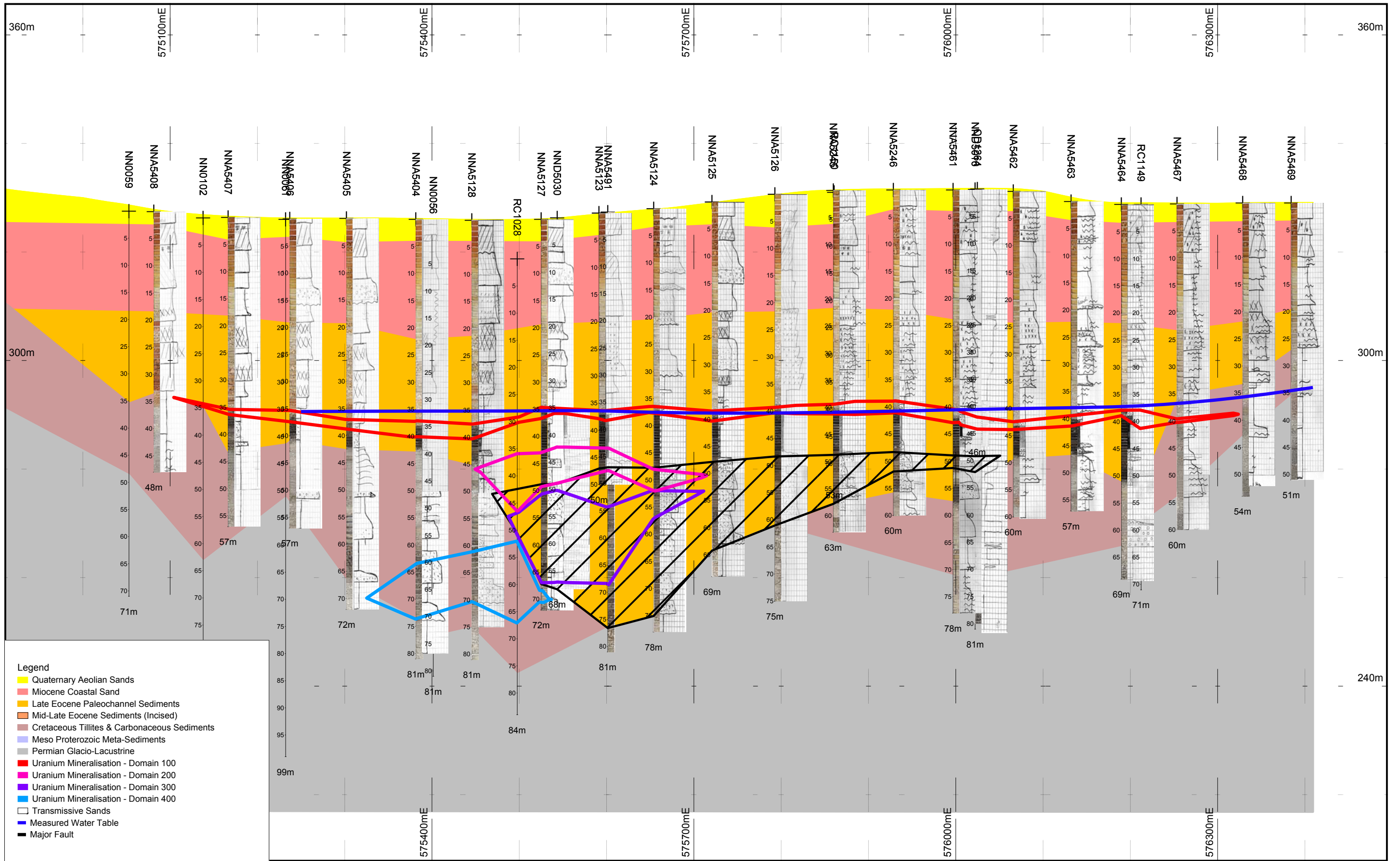


Plot Date 22-Apr-2015 Sheet 1 of 1
 X Scale = 1 : 7047.34 Y Scale = 1 : 1009.47
 Plot File: 47060N_Hydrology

100 0 100m

Ambassador West Local Northing - 47060N

180m

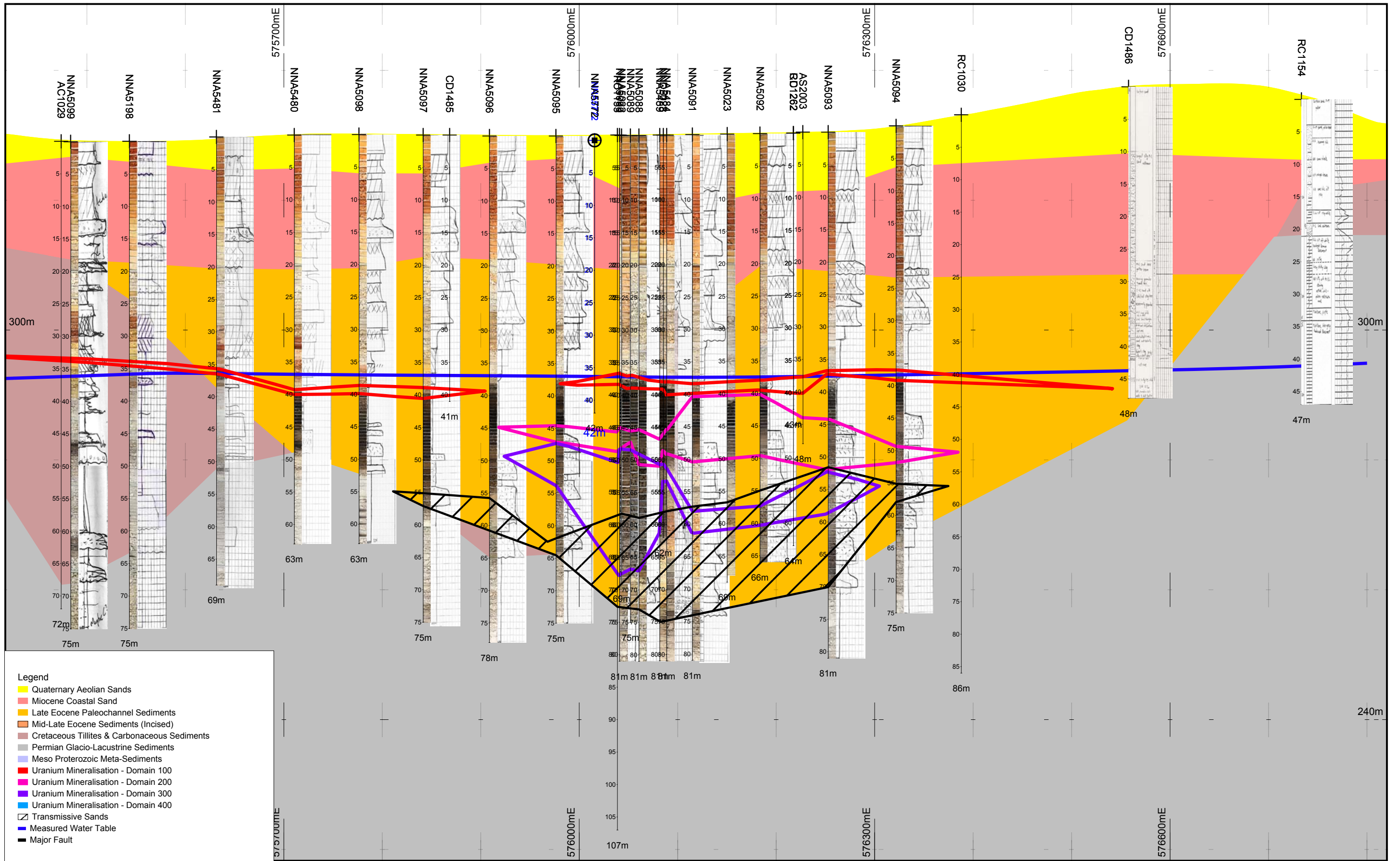


- Legend**
- Quaternary Aeolian Sands
 - Miocene Coastal Sand
 - Late Eocene Paleochannel Sediments
 - Mid-Late Eocene Sediments (Incised)
 - Cretaceous Tillites & Carbonaceous Sediments
 - Meso Proterozoic Meta-Sediments
 - Permian Glacio-Lacustrine
 - Uranium Mineralisation - Domain 100
 - Uranium Mineralisation - Domain 200
 - Uranium Mineralisation - Domain 300
 - Uranium Mineralisation - Domain 400
 - Transmissive Sands
 - Measured Water Table
 - Major Fault



X Scale = 1 : 4856.47 Y Scale = 1 : 671.29	Plot Date 22-Apr-2015	Sheet 1 of 1
Plot File: 47970N_Hydrology		
<div style="display: flex; justify-content: space-between; width: 100%;"> 100 0 100m </div>		

Ambassador West Local Northing - 47970N

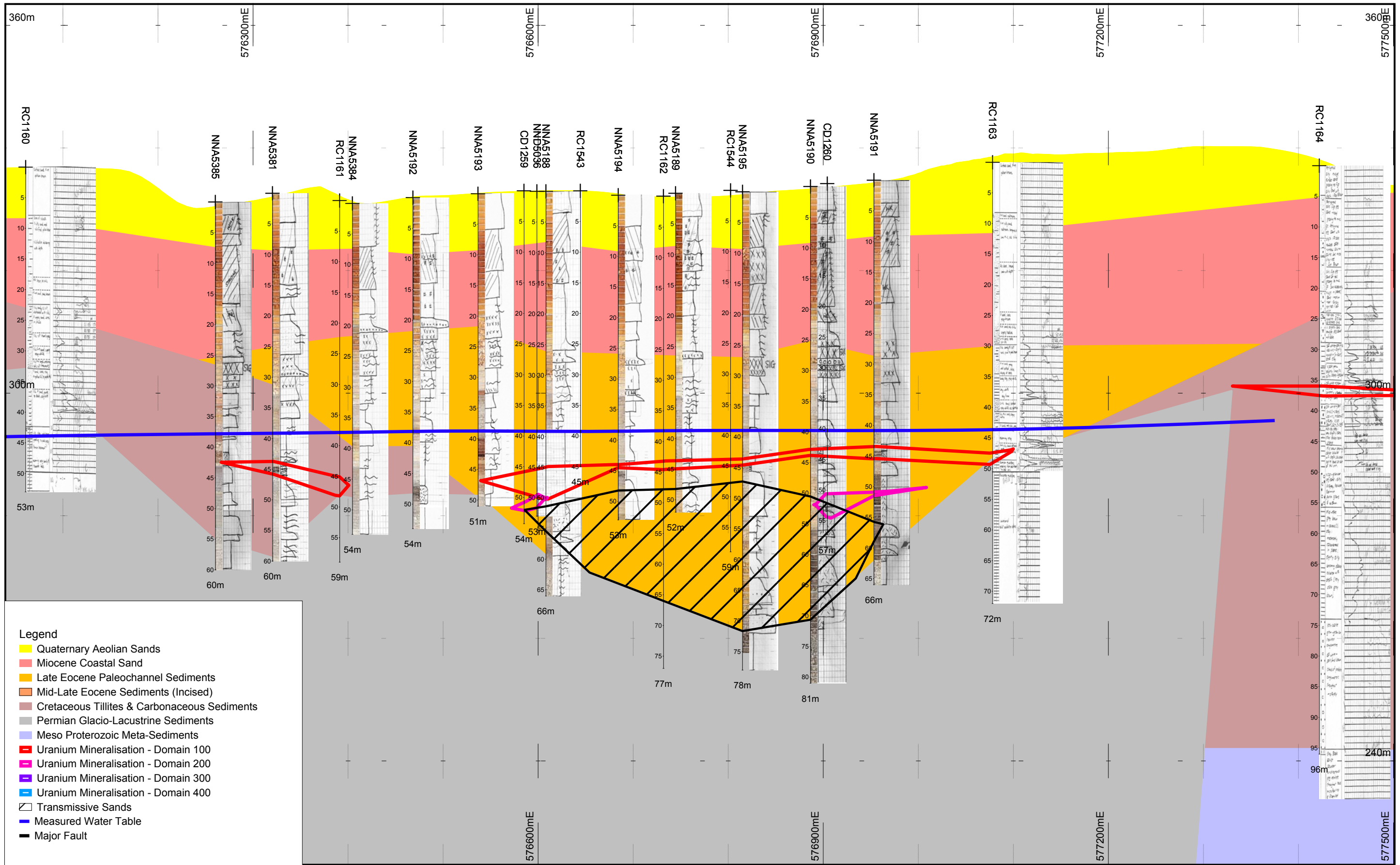


- Legend**
- Quaternary Aeolian Sands
 - Miocene Coastal Sand
 - Late Eocene Paleochannel Sediments
 - Mid-Late Eocene Sediments (Incised)
 - Cretaceous Tillites & Carbonaceous Sediments
 - Permian Glacio-Lacustrine Sediments
 - Meso Proterozoic Meta-Sediments
 - Uranium Mineralisation - Domain 100
 - Uranium Mineralisation - Domain 200
 - Uranium Mineralisation - Domain 300
 - Uranium Mineralisation - Domain 400
 - Transmissive Sands
 - Measured Water Table
 - Major Fault



Plot Date: 22-Apr-2015
 Sheet: 1 of 1
 Plot File: 48760N_Hydrology
 X Scale = 1 : 4305.41
 Y Scale = 1 : 561.08
 100 0 100m

Ambassador West Local Northing - 48760N

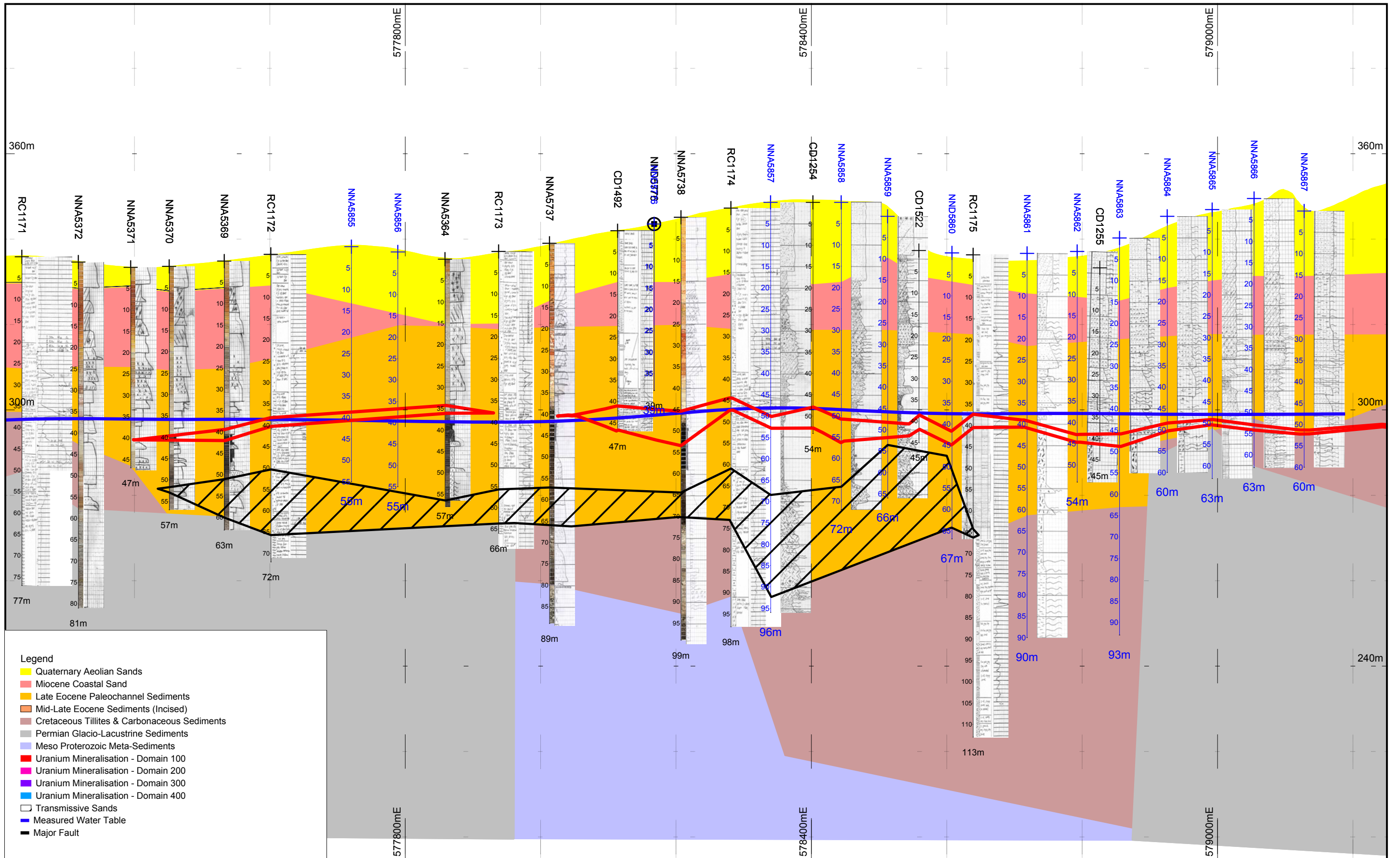


- Legend**
- Quaternary Aeolian Sands
 - Miocene Coastal Sand
 - Late Eocene Paleochannel Sediments
 - Mid-Late Eocene Sediments (Incised)
 - Cretaceous Tillites & Carbonaceous Sediments
 - Permian Glacio-Lacustrine Sediments
 - Meso Proterozoic Meta-Sediments
 - Uranium Mineralisation - Domain 100
 - Uranium Mineralisation - Domain 200
 - Uranium Mineralisation - Domain 300
 - Uranium Mineralisation - Domain 400
 - Transmissive Sands
 - Measured Water Table
 - Major Fault



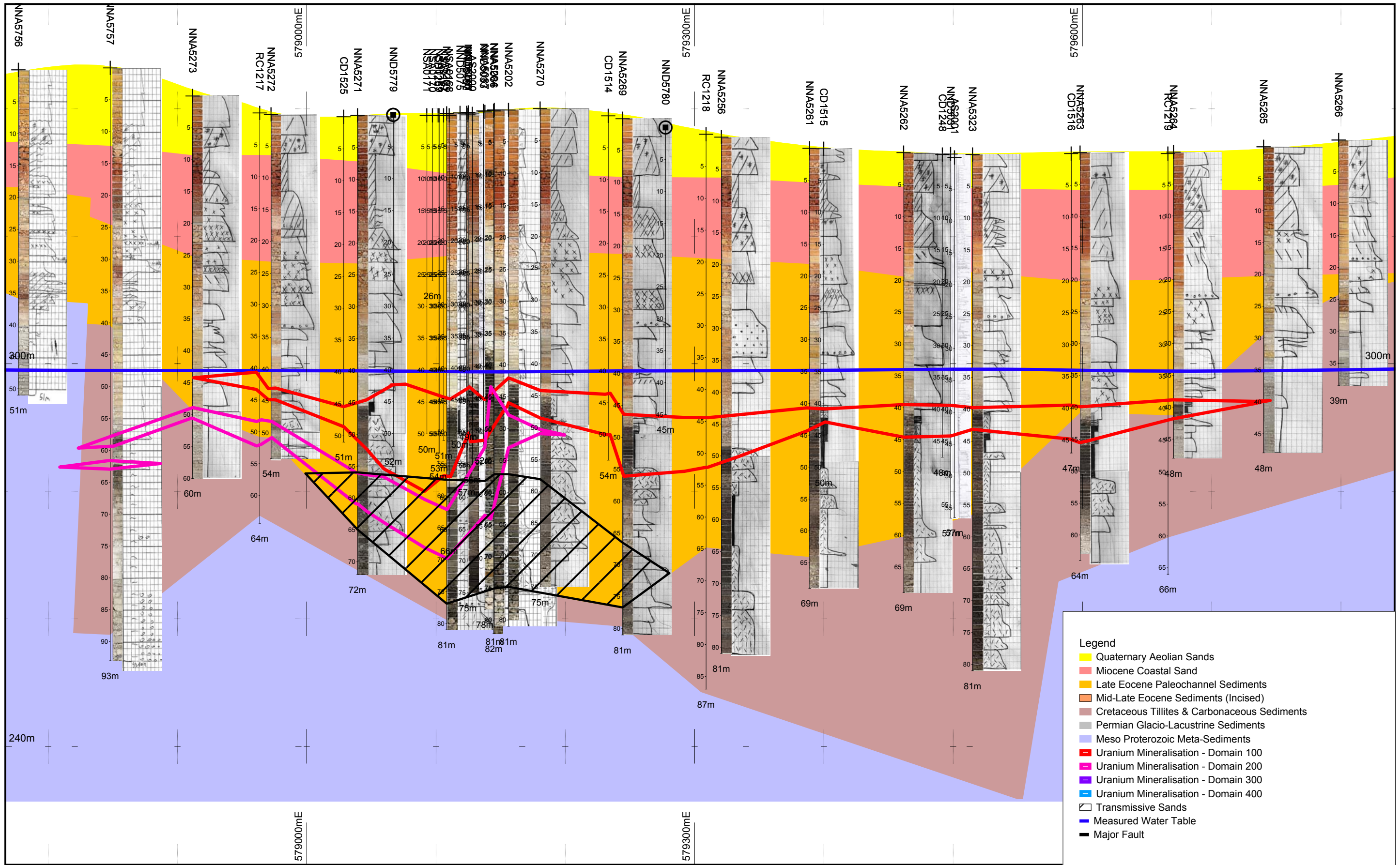
X Scale = 1 : 4485.38 Y Scale = 1 : 597.08	Plot Date 22-Apr-2015	Sheet 1 of 1
Plot File: 49600N_Hydrology		
<div style="display: flex; justify-content: space-between; width: 100%;"> 100 0 100m </div>		

Ambassador West Local Northing - 49600N



X Scale = 1 : 6262.94
 Y Scale = 1 : 852.59
 Plot Date 22-Apr-2015
 Sheet 1 of 1
 Plot File: 50440N_Hydrology
 100 0 100m

Ambassador West to East Local Northing - 50440N



- Legend**
- Quaternary Aeolian Sands
 - Miocene Coastal Sand
 - Late Eocene Paleochannel Sediments
 - Mid-Late Eocene Sediments (Incised)
 - Cretaceous Tillites & Carbonaceous Sediments
 - Permian Glacio-Lacustrine Sediments
 - Meso Proterozoic Meta-Sediments
 - Uranium Mineralisation - Domain 100
 - Uranium Mineralisation - Domain 200
 - Uranium Mineralisation - Domain 300
 - Uranium Mineralisation - Domain 400
 - Transmissive Sands
 - Measured Water Table
 - Major Fault



X Scale = 1 : 3270.37
 Y Scale = 1 : 574.07

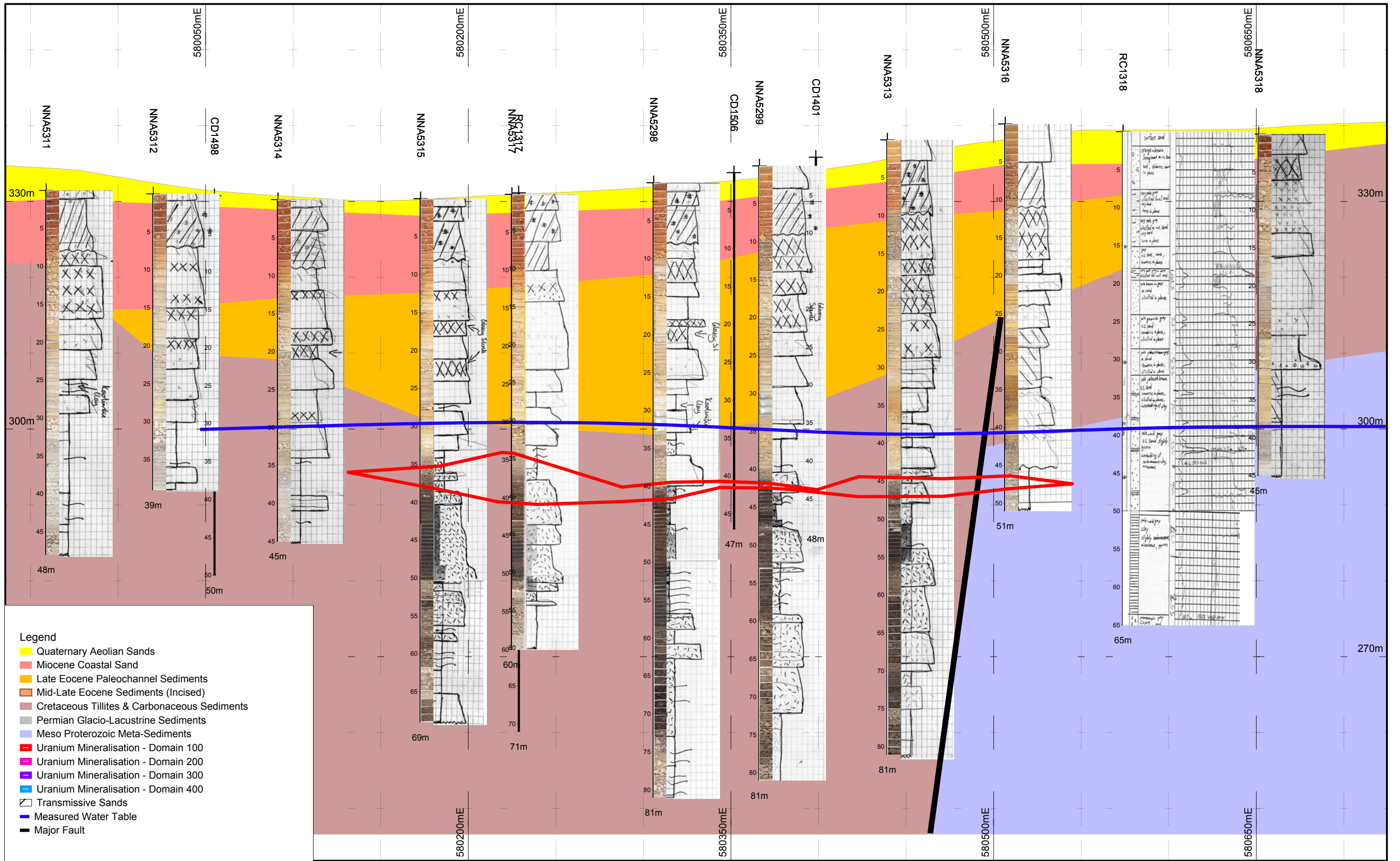
Plot Date
22-Apr-2015

Sheet
1 of 1

Plot File: 51250N_Hydrology

50 0 50m

Ambassador East Local Northing - 51250N



Plot Date
21-Apr-2015

Sheet
1 of 1

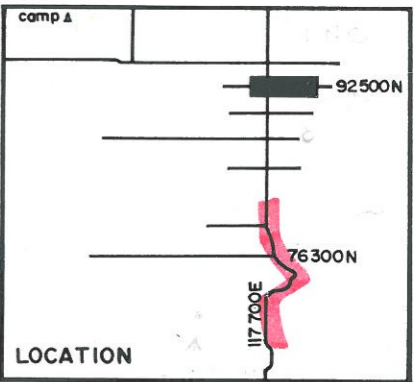
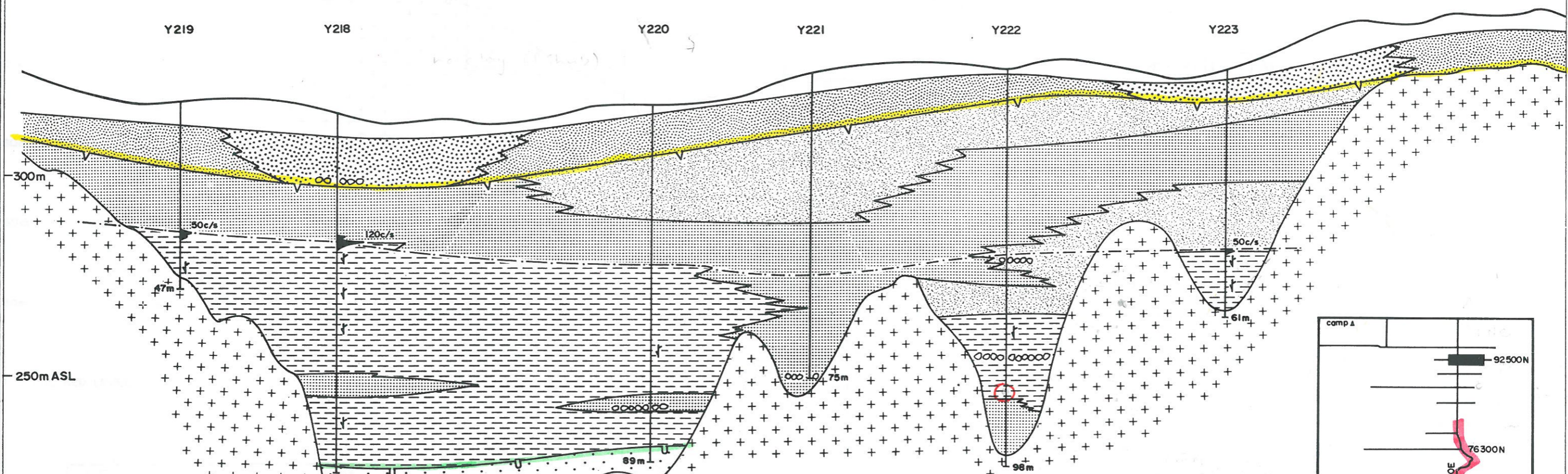
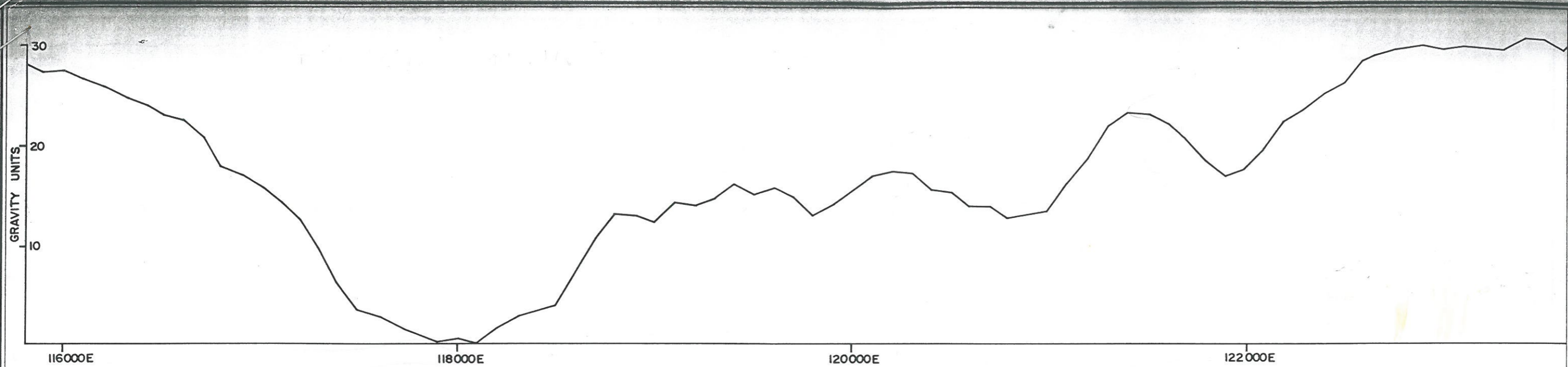
Plot File: 52060N_Hydrology2

X Scale = 1 : 2400.93
Y Scale = 1 : 480.19

50 0 50m

Ambassador East

Local Northing - 52060N



EAST ARM ~ 6655700 m N
 Horiz. Scale 1:20000 Vert. Scale 1:1000

URANERZ AUSTRALIA PTY. LTD.
EAST YILGARN
LINE 92,500N
GRAVITY and
GEOLOGICAL CROSS SECTION

DATE DRAWN Jul 86 FIGURE No. 21
 PLAN No. 320E102 REPORT No. 320-11

- Facies contact
- Redox boundary
- Neogene/Eocene unconformity
- Lignitic material / pebbles
- Downhole gamma log, max cps, through rods

- Quat. Aeolian sand, hardpan
- Quartz clays, salt lake deposits
- Neogene M-F silty sand & indurated clayey silt bands
- M-C gritty silty sands
- Thinly interbedded silts & sands-minor clays
- Eocene Silts & clays often lignitic
- Fluvial sands
- Perm. Blue grey clays-silty
- Archaean Granitic basement

Upper Victoria
Wentz

APPENDIX II
RESULTS OF CHEMICAL ANALYSES



APPENDIX II-a
Emperor and Shogun Raw Water Chemistry Data

Area	Hole ID	Date Sampled	GDA East	GDA North	Ca	Mg	Na	K	Cl	HCO3	SO4	NO3	RL	Sample DEPTH	Sample RL	T.F.R.	TDS	Cond	pH	ORP	Hard	Alkalinity	OH	Fe	Al	F	Si	Br	I	U	Th	Au	As_Sol	Ba_Sol	Cd_Sol	Cr_Sol	Cu_Sol	Co_Sol	Pb_Sol	Mn_Sol	Ni_Sol	Sb_Sol	Sr	Zn	V_Sol	W																		
					mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	mg/L	m AHD	m	m AHD	mg/L	mg/L	µS/cm		mV	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	ug/l	ug/l	ug/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l																			
EMP + SHO	NNA5731	Feb-12	563142	6686527									323.2	69	254.2		39.472	72.707	3.74																																													
EMP + SHO	NNA5731	Feb-12	563142	6686527									323.2	69	254.2		40.372	74.607	3.63																																													
EMP + SHO	NNA5722	Feb-12	563289	6687498									319.7	48	271.7		41.852	74.589	3.39																																													
EMP + SHO	RC0472		563318	6687355									317.7	73	244.7	84.930	84.930																																															
EMP + SHO	RC0472	5/07/1982	563318	6687355	595	2.500	26.000	460	41.610	<.6	10.500	2.2	317.7				127.200	4.40					20		0.4																																							
EMP + SHO	RC0472	7/01/1982	563318	6687355	605	3.040	27.400	470	45.440	<.6	11.500	2.2	317.7				136.500	4.00					2.1		0.7	5																																						
EMP + SHO	RC0472	25/11/1983	563318	6687355	578	2.600	26.600	539	44.870	<.6	9.416	2.4	317.7				140.400	3.80					36																																									
EMP + SHO	RC0472	23/10/1984	563318	6687355	850	850	26.050	560	44.400	<.5	9.110	11	317.7				99.000	4.10					21.4																																									
EMP + SHO	RC0472	Late 1990-Mid 1991	563318	6687355	582	2.871	25.594	506	43.200	12	9.000		317.7				81.839	5.28	167				30	2		4.4	46.4	0.52	<.2		0.009		0.026		0.077	0.013	0.011	0.004	1.45	0.07	<.0005	10.1	0.035	<.0002	<.0015																			
EMP + SHO	NNA5725	Feb-12	563348	6687218									316.7	69	247.7		71.572	129.107	3.18																																													
EMP + SHO	RC0162	18/11/1984	563414	6687607	790	790	18.200	410	31.500	<.5	6.150	18	319.2				75.000	3.80					18.5																																									
EMP + SHO	RC0162	Late 1990-Mid 1991	563414	6687607	697	1.640	15.653	338	27.900	15	5.410		319.2				51.725	5.47	152				55	0.1		14.7	22.5	0.3	<.2		<.0001		0.032		0.002	0.007	<.0005	0.022	1.64	0.01	<.0005	9.7	0.18	<.0002	<.0015																			
EMP + SHO	RC0162	28/02/2013	563414	6687607	690	840	9.200	280	19.000	<.5	3.900		319.2				37.500	49.000	3.80	151																																												
EMP + SHO	WB5-10S	30/11/1984	563414	6687597	850	850	16.700	370	28.800	<.5	6.380	24	319.1										22.8																																									
EMP + SHO	WB5-50S	30/11/1984	563414	6687557	640	640	8.550	220	15.300	<.5	2.850	50	319.2										24.3																																									
EMP + SHO	NNA5727	Feb-12	563439	6687019									320.5	43	277.5		45.172	82.807	3.56																																													
EMP + SHO	NNA5727	Feb-12	563439	6687019									320.5	75	245.5		66.072	119.807	3.28																																													
EMP + SHO	NNA5720	Feb-12	563503	6687552									318.5	51	267.5		45.932	81.729	3.43																																													
EMP + SHO	RC1343	1985	564471	6708311									407.3	75	332.3		48.330		7.00																																													
EMP + SHO	AC0987	25/11/1983	564600	6689549	294	410	4.375	120	7.313	<.6	1.826	1.3	342.0	68.5	273.5			25.400	4.20				1.8																																									
EMP + SHO	RC1134	27/3/1984	566215	6689977	543	378	4.350	93	7.526	1	1.903	6.6	323.2	56.5	266.7			23.600	3.30				160																																									
EMP + SHO	RC1131	27/3/1984	566569	6687057	438	358	4.150	123	7.029	1	1.570	2.7	328.2	59.5	268.7			24.900	3.80				11																																									
EMP + SHO	NNA5685	Feb-12	567629	6684321									337.5	64	273.5		58.372	106.107	3.56																																													
EMP + SHO	NNA5686	Feb-12	567916	6684162									339.9	69	270.9		58.372	105.807	2.84																																													
EMP + SHO	NNA5686	Feb-12	567916	6684162									339.9	99	240.9		71.972	129.807	3.42																																													
EMP + SHO	NNA5682	Feb-12	567959	6684595									334.5	84	250.5		64.760	117.089	3.27																																													
EMP + SHO	NNA5682	Feb-12	567959	6684595									334.5	108	226.5		76.160	136.989	3.29																																													
EMP + SHO	NNA5696	Feb-12	568118	6685554									325.9	66	259.9		69.380	124.776	3.51																																													
EMP + SHO	NNA5696	Feb-12	568118	6685554									325.9	78	247.9		74.480	133.191	3.21																																													
EMP + SHO	NNA5690	Feb-12	568179	6684995									334.0	82	252.0		73.072	131.707	4.35																																													
EMP + SHO	NNA5687	Feb-12	568194	6683993									339.1	69	270.1		71.372	128.707	3.53																																													
EMP + SHO	NNA5683	Feb-12	568236	6684431									334.7	69	265.7		76.572	137.907	3.3																																													

APPENDIX II-bi

Ambassador and Princess Raw Water Chemistry Data Rare Earths

Hole ID	Date Sampled	GDA East	GDA North	La	Ce	Pr	Nd	Sm	Eu	Gd	Tb	Dy	Ho	Er	Tm	Yb	Lu	REE (Total)	δ18O	δ2H
				mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	mg/l	(SMOW)	(SMOW)
RC1213	Late 1990-Mid 1991	575684	6681498	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	-3.18	-26.4
RC1148	Late 1990-Mid 1991	576004	6680326	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd
RC1152	Late 1990-Mid 1991	576022	6681299	0.0022	0.0038	0.0006	0.0029	0.0008	0.0002	0.0008	0.0001	0.0005	0.0003	0.0005	0.0001	0.0005	0.0001	0.0134	nd	nd
CD1366	Late 1990-Mid 1991	577430	6682621	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	-2.08	-14
RC1177	Late 1990-Mid 1991	578272	6682855	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	-3.47	-32.6
RC1216	Late 1990-Mid 1991	578630	6683116	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	nd	-3.59	-32.2
CD1409	Late 1990-Mid 1991	578711	6682585	0.0011	0.0009	0.0002	0.0008	0.0008	0.0003	0.0007	0.0001	0.0004	0.0001	0.0004	0.0001	0.0006	0.0001	0.0066	-3.5	-24

APPENDIX III
CONSTRUCTION DETAILS AND PUMPING TEST PLOTS FOR
PRODUCTION BORES NWB1 AND NWB2





Information to be provided on completion of a non-artesian well

Information to be provided to the Department of Water under the *Water Agencies (Powers) Act 1984* and Section 26E of the *Rights in Water and Irrigation Act 1914* and Regulation 39 of the *Rights in Water and Irrigation Regulations 2000*

Please note:

- All information is to be written clearly and in block letters.
- If insufficient room please use a separate piece of paper.
- It is the responsibility of the person carrying out the works to fill out this form.

Part 1: Details of any licence granted for the work under the *Rights in Water And Irrigation Act 1914* section 26D

Licence number

Individual Company

Licensee's full name

Part 2: Details of person carrying out the works

Company

Driller

Driller licence number (non-mandatory) Driller classification (non-mandatory)

Postal address

Telephone Facsimile

Email

Part 3: Location of well

A 26D licence will list the premises on which well construction is to occur.

If the physical address of the well is different from the property address listed on the licence, contact the Department of Water prior to the commencement of construction.

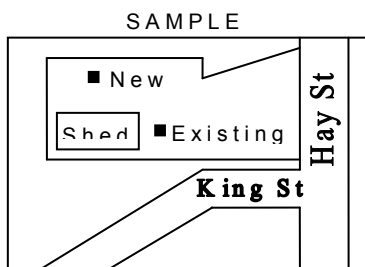
Property address of well or other tenure details

Well coordinates GPS reading Estimate

Zone Easting/latitude Northing/longitude

Datum (e.g. GDA94/WGS84) GPS reliability

Location plan – in the box below please sketch a plan showing position of well in relation to building, boundaries, road, nearest cross road and any additional information to assist in locating the well.



In the box to the right, please sketch a plan showing:
- location of all wetlands / watercourses / wells / soaks (existing and proposed).
- major improvements (house, large sheds etc).
- shaded sections to indicate areas under development.



Part 4: Construction details (All measurements are to be taken from ground level)

Please complete well construction diagram in box provided below. If insufficient room please attach on separate piece of paper.

Production casing detail					
Material	Nominal bore	Diameter O.D (mm)	Wall thickness (mm)	Depth	
				From (m)	To (m)

Screens/slots				
Screens/slot (type)	Diameter O.D (mm)	Aperture (mm)	Top of screen (m)	Bottom of screen (m)

Gravel pack details		
Gravel size (mm) 1.6-3.2	From (m)	To (m)

Annular fill		
Material type	From (m)	To (m)

Cementing detail		
<input type="checkbox"/> Pressure cement grouted <input type="checkbox"/> Tremmie		
Casing diameter (mm O.D)	Depth	
	From (m)	To (m)

Total depth drilled (from ground level)

Geophysical log required as condition of licence? Yes No

Geophysical log taken? (attach log and contractor details) Yes No

From (m)	To (m)	Strata description (If insufficient room attach on separate page)

Part 5: Particulars of well

Drilling start date refers to the date drilling begins. Do not include set up date.

Drilling completion date includes well development and testing.

Well name / number

Drilling start Drilling completion

Drilling method used

Rotary air Cable tool Auger Rotary mud

Sludge Other (specify) _____

Final status of well

Ready to operate Decommissioned

Other (specify) _____

Purpose (use) of well

Production Investigation Monitoring

Other (specify) _____

Part 6: Well development

Date (dd/mm/yy) Duration of development hours

Method Airlift Pump Jetting Surging

Development pump rate (e.g. L/s, m³/day)

Part 7: Pump testing (If applicable)

Date start (dd/mm/yy) Date end (dd/mm/yy) Duration of test hours

Step test Constant rate Other

Constant rate - pump rate (e.g. m³/day)

Pump type (e.g. submersible)

Water rest level prior to test (m)

Measurements taken from top of casing (TOC) ground level (GL)

other (specify) _____

Elevation of measurement reference point if known (metres AHD)

GPS Estimate

other (specify) _____

Final drawdown m Recommended supply (e.g. m³/day)

Final drawdown is the distance between the static water level measured prior to the test and the water level measured at the end of the pumping test.

Comments.....

Part 8: Field samples

Specify unit measurements.

Collection method (e.g. pump test, airlift)

Conductivity (e.g. mS/m)

Water temperature at test

Temperature compensated Temperature uncompensated

pH

Comments.....

Part 9: Lab samples

Lab samples taken (Please attach) Yes No

TDS (e.g. mg/l)

Please submit samples separately to form if not received before the 1 month submission deadline.

Part 10: Water levels

SWL (Static water level) m Water cut at m

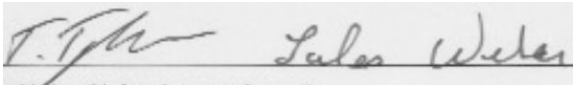
Measurements taken from top of casing (TOC) ground level (GL)
 other (specify) _____

Date of reading (dd/mm/yy)

Comments.....

Part 11: Declaration and signature

- Capacity of person making declaration:
- An individual who carried out the work
 - An officer who is a director or secretary of a corporation that carried out the work.
 - Other (describe).....



I, _____ (name of person making declaration) declare that the information provided on this form is true and correct.

Important information

- All information must be completed on the form unless otherwise indicated as optional for example; provision of the drillers licence number and classification fields are not mandatory and can be filled in at the drillers discretion. Provision of non-mandatory details would greatly assist the department in completion of its data set.
- Failure to complete all mandatory details and to submit the form to the department is an offence under the *Rights in Water and Irrigation Act 1914*.
- Under section 26E and regulation 39 within 1 month of completion of the construction of or deepening of the well, the person carrying out the work for a 26D licence must submit this form.
- Non-artesian wells in proclaimed areas require a licence unless exempted under the *Rights in Water and Irrigation Exemption (S26C) Order 2007*.

Where and how to submit this form

This form can be submitted by fax, post or in person to the appropriate Department of Water regional office. For assistance in completing this form contact your regional office.

<p>Kimberley Region</p> <p>Kununurra Regional Office 27 Victoria Hwy Kununurra WA 6743 Tel: 08 9166 4100 Fax: 08 9168 3174 PO Box 625 Kununurra WA 6743</p>	<p>Kwinana Peel Region</p> <p>Mandurah Regional Office 107 Breakwater Parade Mandurah WA 6210 Tel: 08 9550 4222 Fax: 08 9581 4560 PO Box 332 Mandurah WA 6210</p>	<p>South Coast Region</p> <p>Albany Regional Office 5 Bevan Street Albany WA 6330 Tel: 08 9842 5760 Fax: 08 9842 1204 PO Box 525 Albany WA 6331</p>	<p>Warren Blackwood District</p> <p>Manjimup Regional Office 52 Bath Street Manjimup WA 6528 Tel: 08 9771 1878 Fax: 08 9771 4335</p>
<p>Midwest Gascoyne Region</p> <p>Geraldton Regional Office 94 Sandford Street Geraldton WA 6531 Tel: 08 9965 7400 Fax: 08 9964 5983 Po Box 81 Geraldton WA 6531</p>	<p>South West Region</p> <p>Bunbury Regional Office 35-39 McCombe Road Bunbury WA 6230 Tel: 08 9726 4111 Fax: 08 9726 4100 PO Box 261 Bunbury WA 6231</p>	<p>Pilbara Region</p> <p>Karratha Regional Office Lot 4608 Cherratta Road Karratha Industrial Estate Karratha WA 6714 Tel: 08 9144 2000 Fax: 08 9144 2610 PO Box 836 Karratha WA 6714</p>	
<p>Carnarvon</p> <p>Carnarvon District Office 211 Robinson Street Carnarvon WA 6701 Tel: 08 9941 6100 Fax: 08 9941 4931 PO Box 81 Carnarvon WA 6701</p>	<p>Busselton</p> <p>Busselton District Office Suite 2, 72 Duchess Street Busselton WA 6280 Tel: 08 9781 0188 Fax: 08 9754 4335 PO Box 269 Busselton WA 6280</p>	<p>Swan Avon Region</p> <p>Victoria Park Regional Office 7 Ellam Street Victoria Park WA 6100 Tel: 08 6250 8000 Fax: 08 6250 8050</p>	

Please retain a copy of this form for your records



Information to be provided on completion of a non-artesian well

Information to be provided to the Department of Water under the *Water Agencies (Powers) Act 1984* and Section 26E of the *Rights in Water and Irrigation Act 1914* and Regulation 39 of the *Rights in Water and Irrigation Regulations 2000*

Please note:

- All information is to be written clearly and in block letters.
- If insufficient room please use a separate piece of paper.
- It is the responsibility of the person carrying out the works to fill out this form.

Part 1: Details of any licence granted for the work under the *Rights in Water And Irrigation Act 1914* section 26D

Licence number

Individual Company

Licensee's full name

Part 2: Details of person carrying out the works

Company

Driller

Driller licence number (non-mandatory) Driller classification (non-mandatory)

Postal address

Telephone Facsimile

Email

Part 3: Location of well

A 26D licence will list the premises on which well construction is to occur.

If the physical address of the well is different from the property address listed on the licence, contact the Department of Water prior to the commencement of construction.

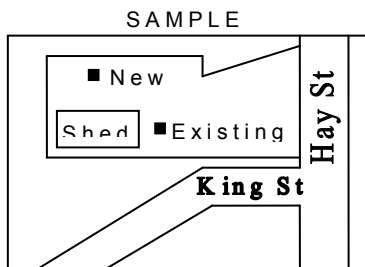
Property address of well or other tenure details

Well coordinates GPS reading Estimate

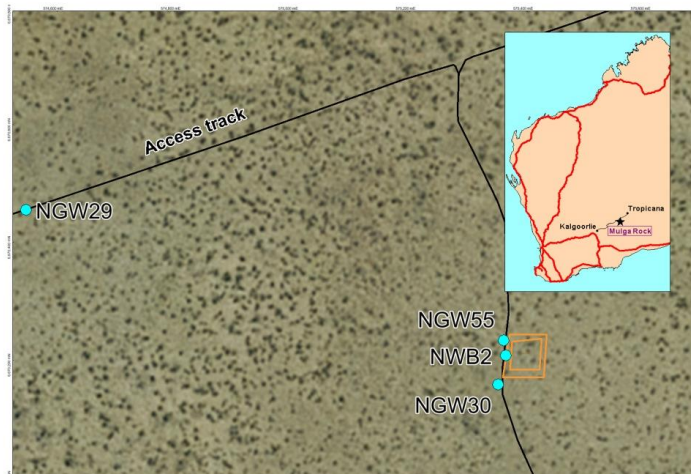
Zone Easting/latitude Northing/longitude

Datum (e.g. GDA94/WGS84) GPS reliability

Location plan – in the box below please sketch a plan showing position of well in relation to building, boundaries, road, nearest cross road and any additional information to assist in locating the well.



In the box to the right, please sketch a plan showing:
- location of all wetlands / watercourses / wells / soaks (existing and proposed).
- major improvements (house, large sheds etc).
- shaded sections to indicate areas under development.



Part 4: Construction details (All measurements are to be taken from ground level)

Please complete well construction diagram in box provided below. If insufficient room please attach on separate piece of paper.

Production casing detail					
Material	Nominal bore	Diameter O.D (mm)	Wall thickness (mm)	Depth	
				From (m)	To (m)

Screens/slots				
Screens/slot (type)	Diameter O.D (mm)	Aperture (mm)	Top of screen (m)	Bottom of screen (m)

Gravel pack details		
Gravel size (mm) 1.6-3.2	From (m)	To (m)

Annular fill		
Material type	From (m)	To (m)

Cementing detail		
<input type="checkbox"/> Pressure cement grouted <input type="checkbox"/> Tremmie		
Casing diameter (mm O.D)	Depth	
	From (m)	To (m)

Total depth drilled (from ground level)

Geophysical log required as condition of licence? Yes No

Geophysical log taken? (attach log and contractor details) Yes No

From (m)	To (m)	Strata description (If insufficient room attach on separate page)

Part 5: Particulars of well

Drilling start date refers to the date drilling begins. Do not include set up date.

Drilling completion date includes well development and testing.

Well name / number	<input type="text"/>		
Drilling start	<input type="text"/>	Drilling completion	<input type="text"/>
Drilling method used	<input type="checkbox"/> Rotary air <input type="checkbox"/> Cable tool <input type="checkbox"/> Auger <input type="checkbox"/> Rotary mud <input type="checkbox"/> Sludge <input type="checkbox"/> Other (specify) _____		
Final status of well	<input type="checkbox"/> Ready to operate <input type="checkbox"/> Decommissioned <input type="checkbox"/> Other (specify) _____		
Purpose (use) of well	<input type="checkbox"/> Production <input type="checkbox"/> Investigation <input type="checkbox"/> Monitoring <input type="checkbox"/> Other (specify) _____		

Part 6: Well development

Date (dd/mm/yy)	<input type="text"/>	Duration of development	<input type="text"/>	hours
Method	<input type="checkbox"/> Airlift <input type="checkbox"/> Pump <input type="checkbox"/> Jetting <input type="checkbox"/> Surging			
			Development pump rate (e.g. L/s, m³/day)	<input type="text"/>

Part 7: Pump testing (If applicable)

Date start (dd/mm/yy)	<input type="text"/>	Date end (dd/mm/yy)	<input type="text"/>	Duration of test	<input type="text"/>	hours
<input type="checkbox"/> Step test <input type="checkbox"/> Constant rate <input type="checkbox"/> Other						
Constant rate - pump rate (e.g. m³/day)	<input type="text"/>	Pump type (e.g. submersible)		<input type="text"/>		
				Water rest level prior to test (m)	<input type="text"/>	
Measurements taken from <input type="checkbox"/> top of casing (TOC) <input type="checkbox"/> ground level (GL)						
<input type="checkbox"/> other (specify) _____						
Elevation of measurement reference point if known (metres AHD)		<input type="checkbox"/> GPS <input type="checkbox"/> Estimate <input type="checkbox"/> other (specify) _____				
Final drawdown	<input type="text"/>	m	Recommended supply (e.g. m³/day)	<input type="text"/>		

Final drawdown is the distance between the static water level measured prior to the test and the water level measured at the end of the pumping test.

Comments.....

Part 8: Field samples

Specify unit measurements.	Collection method (e.g. pump test, airlift)	<input type="text"/>		
	Conductivity (e.g. mS/m)	<input type="text"/>	<input type="checkbox"/> Temperature compensated <input type="checkbox"/> Temperature uncompensated	pH <input type="text"/>
	Water temperature at test	<input type="text"/>		

Comments.....

Part 9: Lab samples

Lab samples taken (Please attach)	<input type="checkbox"/> Yes <input type="checkbox"/> No	TDS (e.g. mg/l)	<input type="text"/>	Please submit samples separately to form if not received before the 1 month submission deadline.
--	---	------------------------	----------------------	---

Part 10: Water levels

SWL (Static water level) m Water cut at m

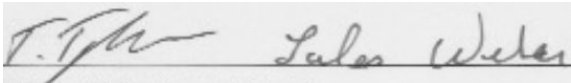
Measurements taken from top of casing (TOC) ground level (GL)
 other (specify) _____

Date of reading (dd/mm/yy)

Comments.....

Part 11: Declaration and signature

- Capacity of person making declaration:
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 - Other (describe).....



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- Under section 26E and regulation 39 within 1 month of completion of the construction of or deepening of the well, the person carrying out the work for a 26D licence must submit this form.
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Kununurra Regional Office
 27 Victoria Hwy
 Kununurra WA 6743
 Tel: 08 9166 4100
 Fax: 08 9168 3174
 PO Box 625
 Kununurra WA 6743

Midwest Gascoyne Region

Geraldton Regional Office
 94 Sandford Street
 Geraldton WA 6531
 Tel: 08 9965 7400
 Fax: 08 9964 5983
 Po Box 81
 Geraldton WA 6531

Carnarvon

Carnarvon District Office
 211 Robinson Street
 Carnarvon WA 6701
 Tel: 08 9941 6100
 Fax: 08 9941 4931
 PO Box 81
 Carnarvon WA 6701

Kwinana Peel Region

Mandurah Regional Office
 107 Breakwater Parade
 Mandurah WA 6210
 Tel: 08 9550 4222
 Fax: 08 9581 4560
 PO Box 332
 Mandurah WA 6210

South West Region

Bunbury Regional Office
 35-39 McCombe Road
 Bunbury WA 6230
 Tel: 08 9726 4111
 Fax: 08 9726 4100
 PO Box 261
 Bunbury WA 6231

Busselton

Busselton District Office
 Suite 2, 72 Duchess Street
 Busselton WA 6280
 Tel: 08 9781 0188
 Fax: 08 9754 4335
 PO Box 269
 Busselton WA 6280

South Coast Region

Albany Regional Office
 5 Bevan Street
 Albany WA 6330
 Tel: 08 9842 5760
 Fax: 08 9842 1204
 PO Box 525
 Albany WA 6331

Pilbara Region

Karratha Regional Office
 Lot 4608 Cherratta Road
 Karratha Industrial Estate
 Karratha WA 6714
 Tel: 08 9144 2000
 Fax: 08 9144 2610
 PO Box 836
 Karratha WA 6714

Swan Avon Region

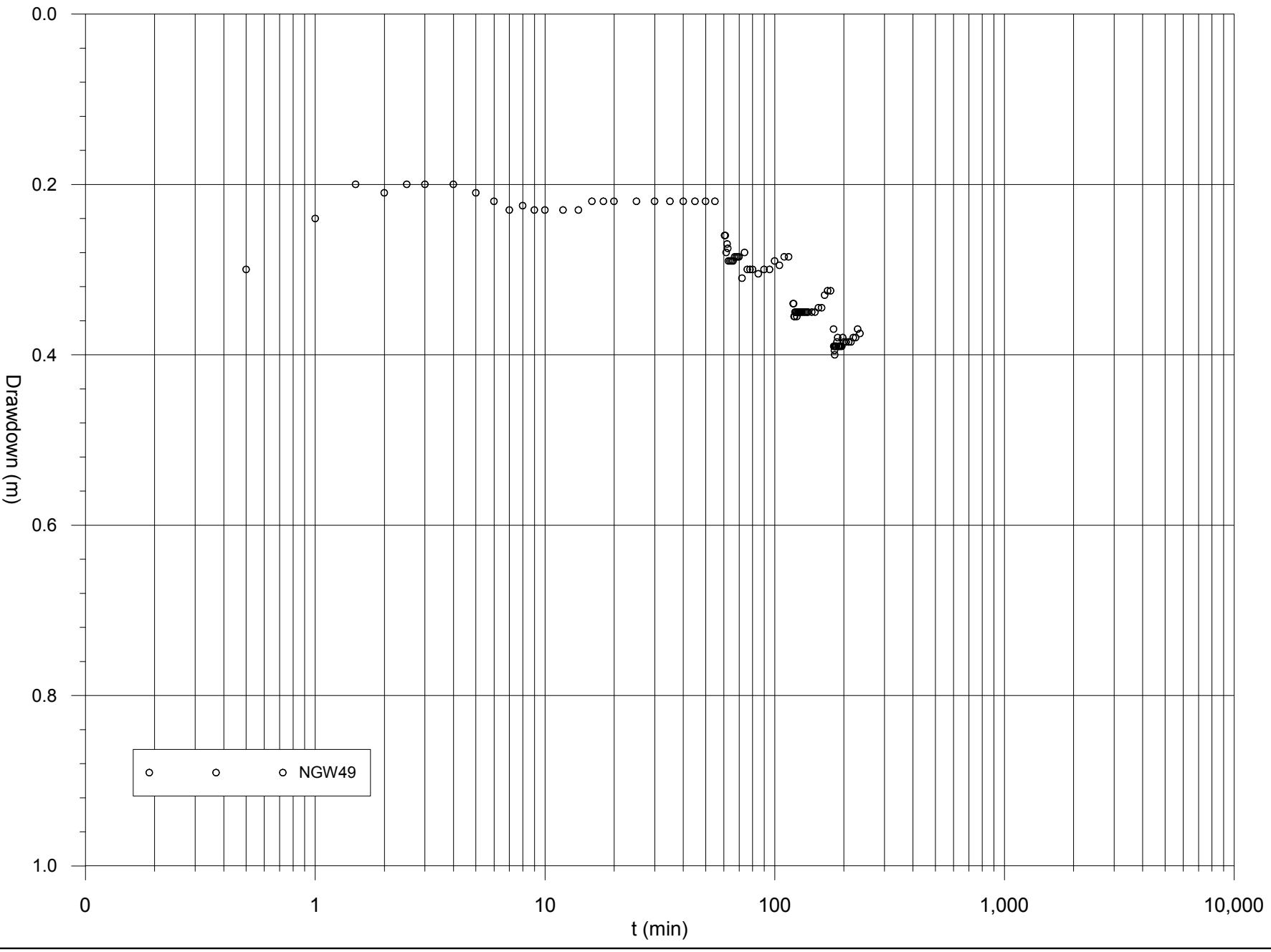
Victoria Park Regional Office
 7 Ellam Street
 Victoria Park WA 6100
 Tel: 08 6250 8000
 Fax: 08 6250 8050

Warren Blackwood District

Manjimup Regional Office
 52 Bath Street
 Manjimup WA 6528
 Tel: 08 9771 1878
 Fax: 08 9771 4335

Please retain a copy of this form for your records

Figure AIII-0

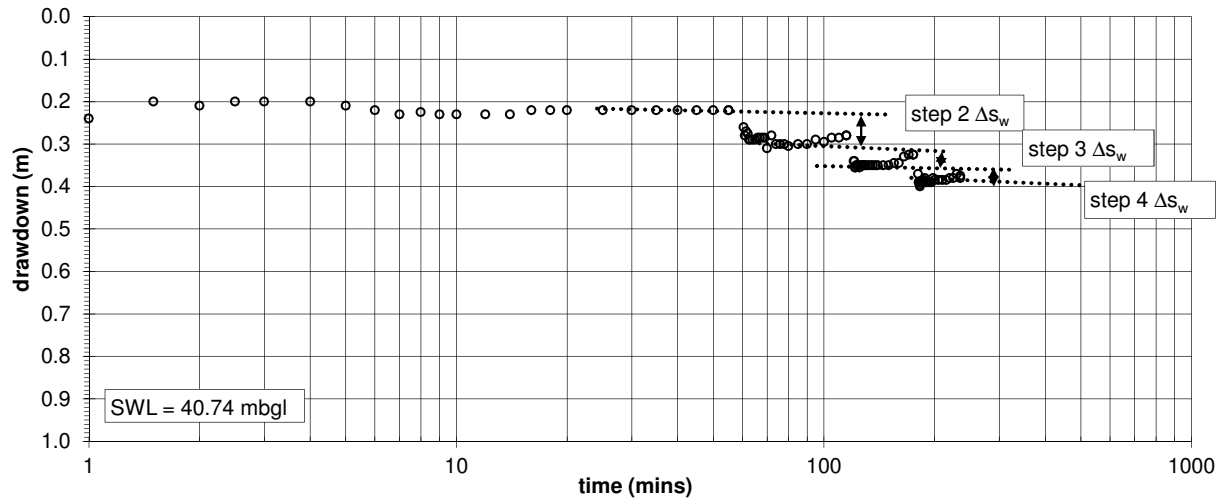


NWB1 step test.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/1-AIII-0

NWB1 PRODUCTION BORE
STEP-RATE PUMPING TEST
at 432 KL/d, 618 KL/d, 789 KL/d, 918 KL/d

Figure AIII-0A



$s=BQ+CQ^2$, where:

BQ is drawdown due to laminar flow

CQ^2 is drawdown due to turbulent flow

$s/Q=B+CQ$, so in plot of s/Q v. Q , B is the intercept

& C is the slope

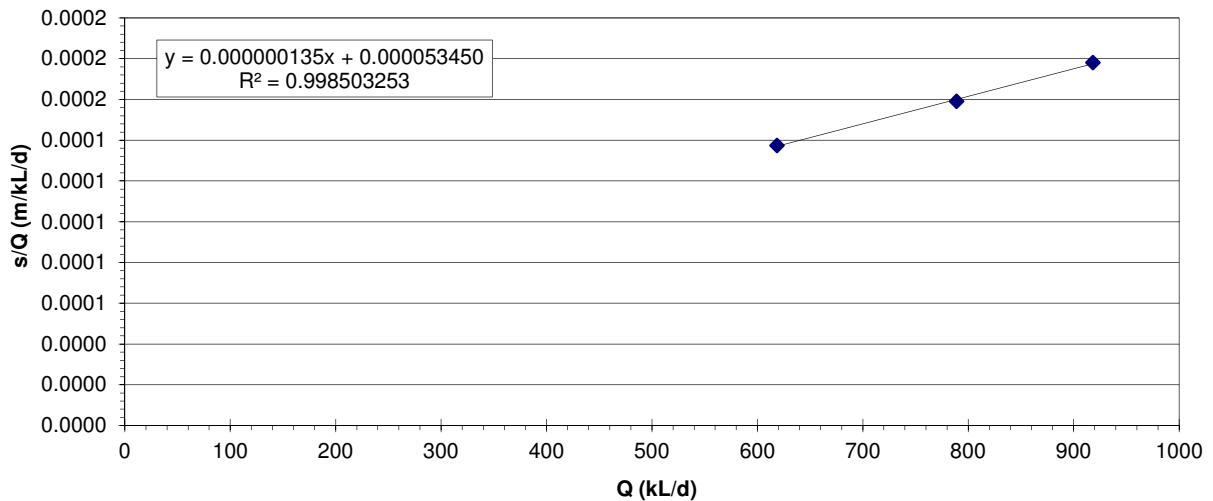
B = 5.3E-05 intercept

C = 1.4E-07 slope

Step	Q		stabilised drawdown (s)		s/Q m/kL/d
	L/s	kL/d	Δs_w (m)	total (m)	
1					
2	7.16	618.62	0.085	0.085	0.00014
3	9.13	788.83	0.041	0.126	0.00016
4	10.63	918.43	0.038	0.164	0.00018

predicted drawdown using B & C @ $Q=14$ L/s, = 0.26 m

actual drawdown from CRT @ $t=1320$ mins & $Q=14$ L/s, = 0.49 m



Drawdown due to turbulent flow in aquifer and bore (Lt)

$Lt=(CQ^2/(BQ+CQ^2))100$

Lt = 52.2 % at $Q=5$ L/s

Lt = 61.0 % at $Q=7$ L/s

Lt = 66.6 % at $Q=9$ L/s

Lt = 69.9 % at $Q=11$ L/s

345.0\Data\Pumping Tests\step test - NWB3 Analysis.xls

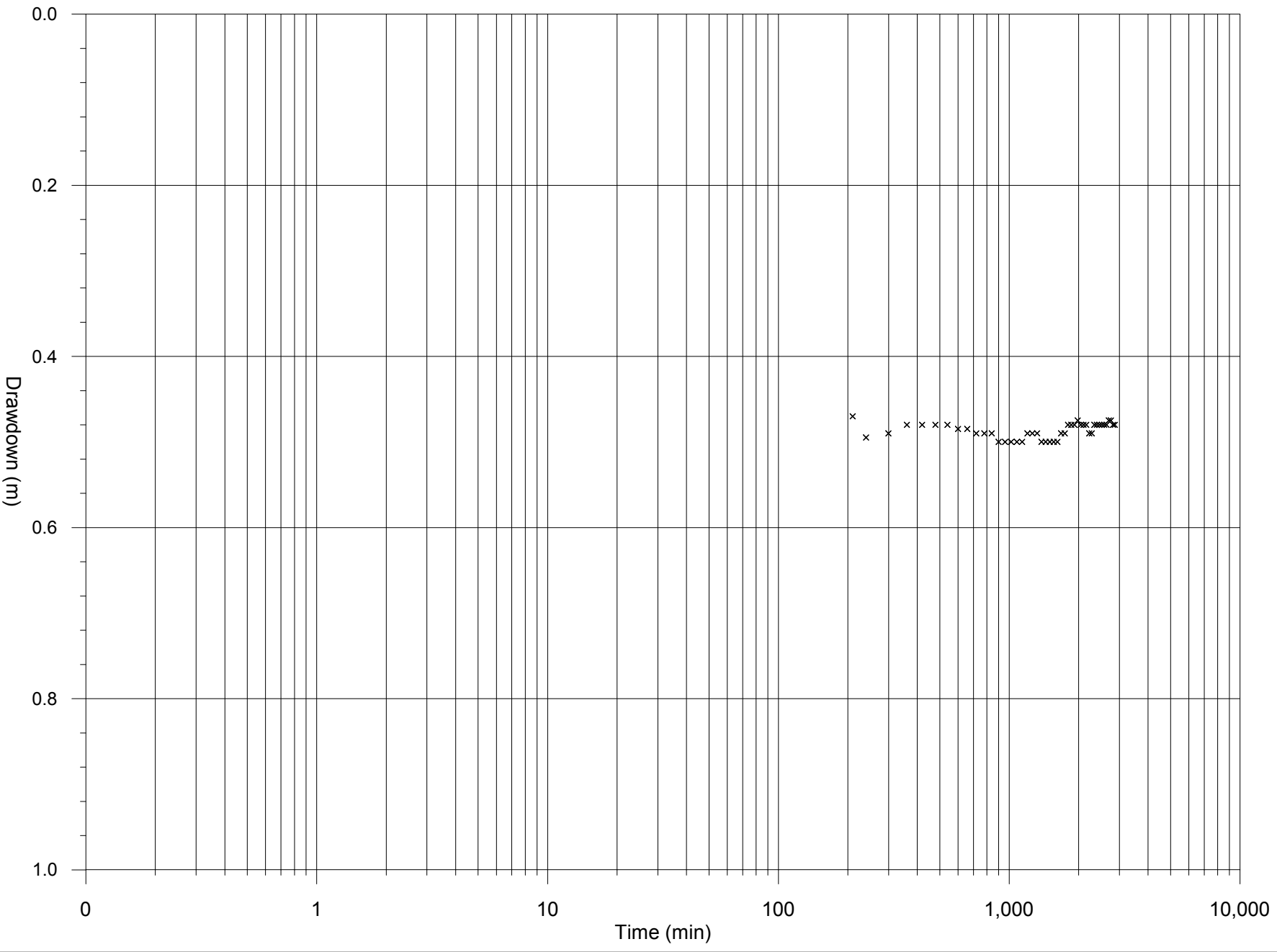
Client: Vimy Resources
 Project: 345-0
 Date: March 2015
 Dwg No. 345-0/15/1-AIII-0A

Bore NWB1 Step-rate Test Data with Analysis
 of Turbulent Flow



Rockwater Pty Ltd

Figure AIII-1

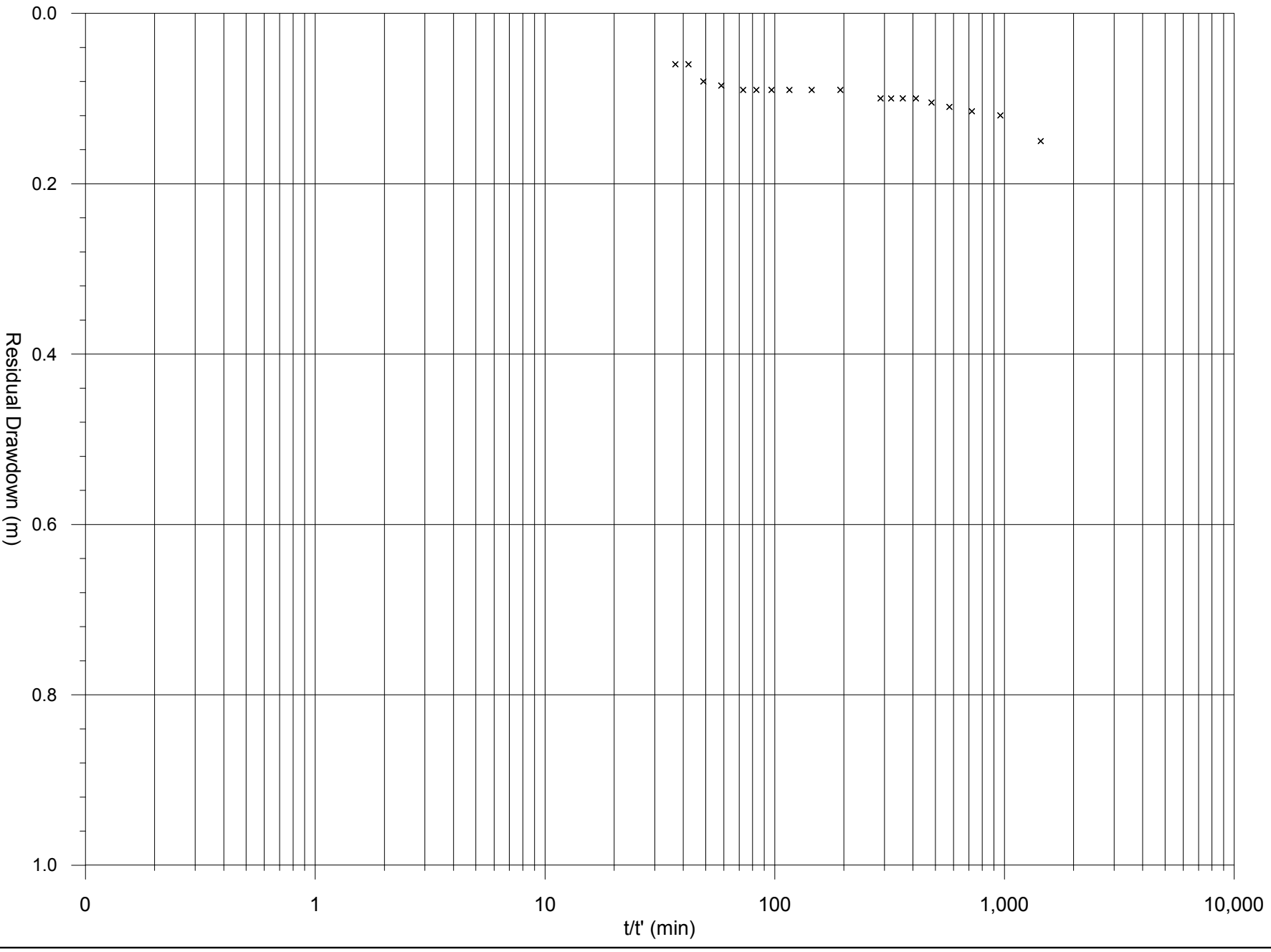


nbw1_prod.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/1-AIII-1

BORE NBW1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
DRAWDOWNS IN NBW1

Figure AIII-2

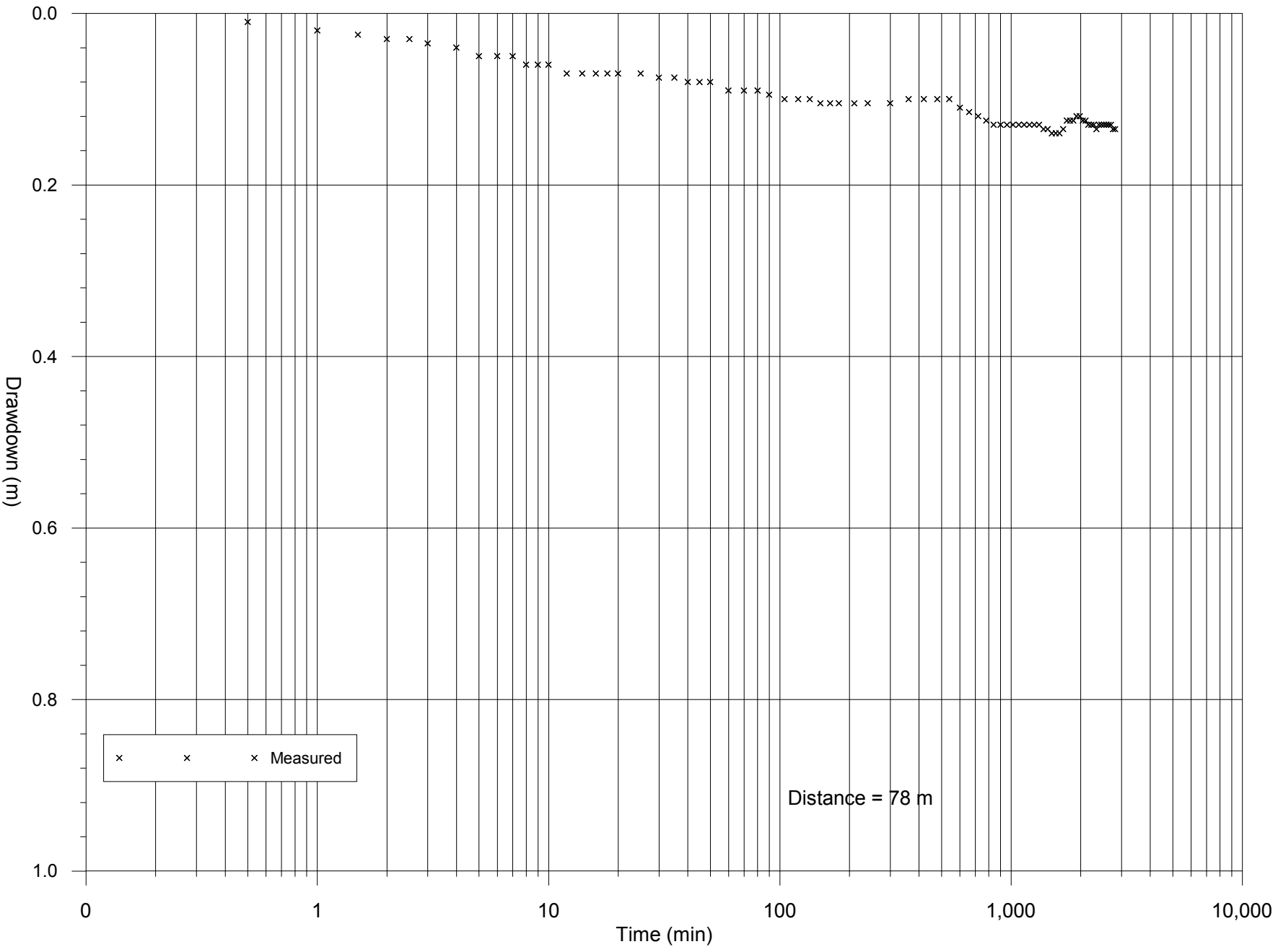


nwb1_recovery.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/1-AIII-2

BORE NWB1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
RECOVERY IN NWB1

Figure AIII-3

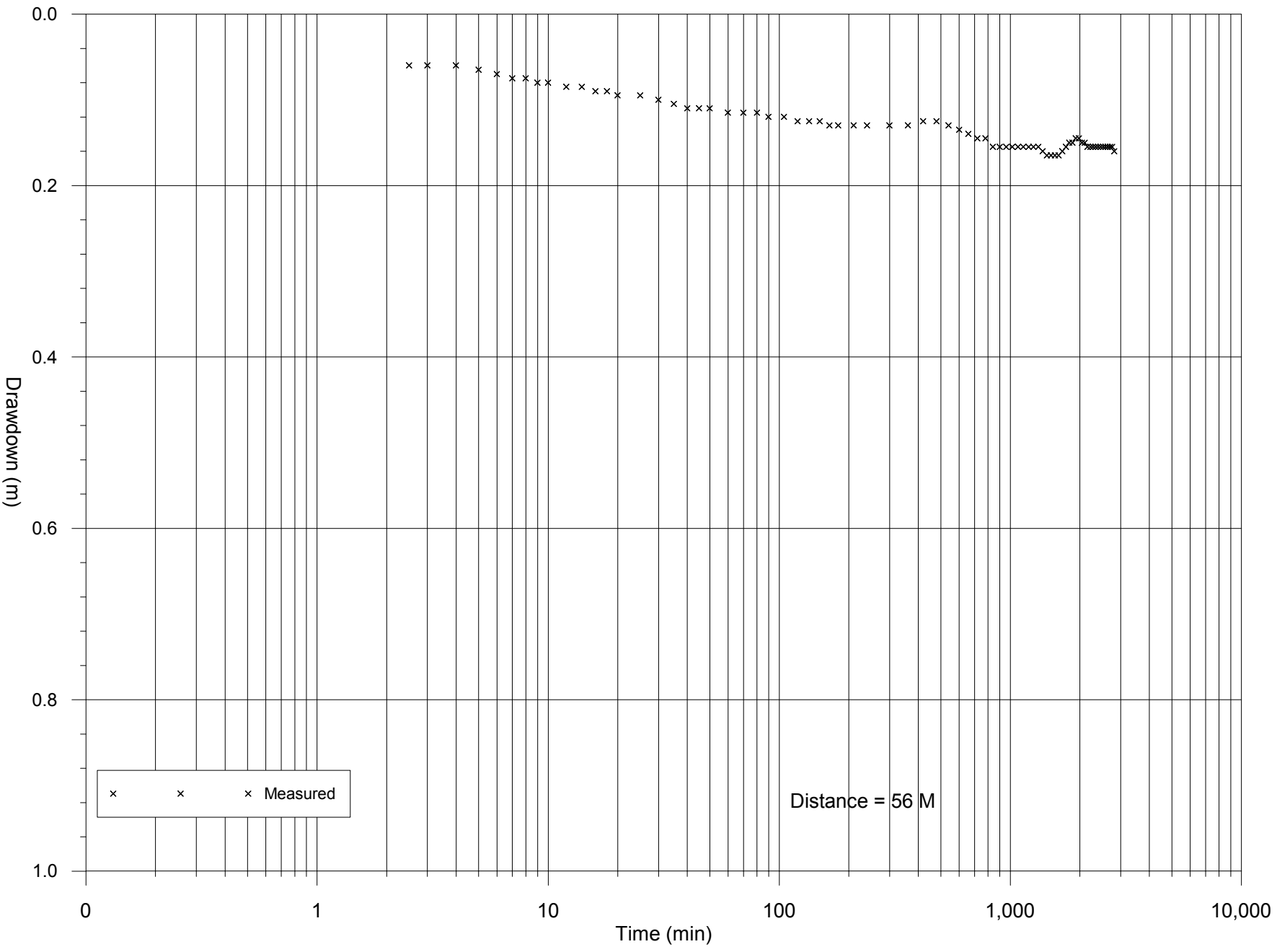


nbw1 ngw37.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-3

BORE NBW1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
DRAWDOWNS IN NGW37

Figure AIII-4

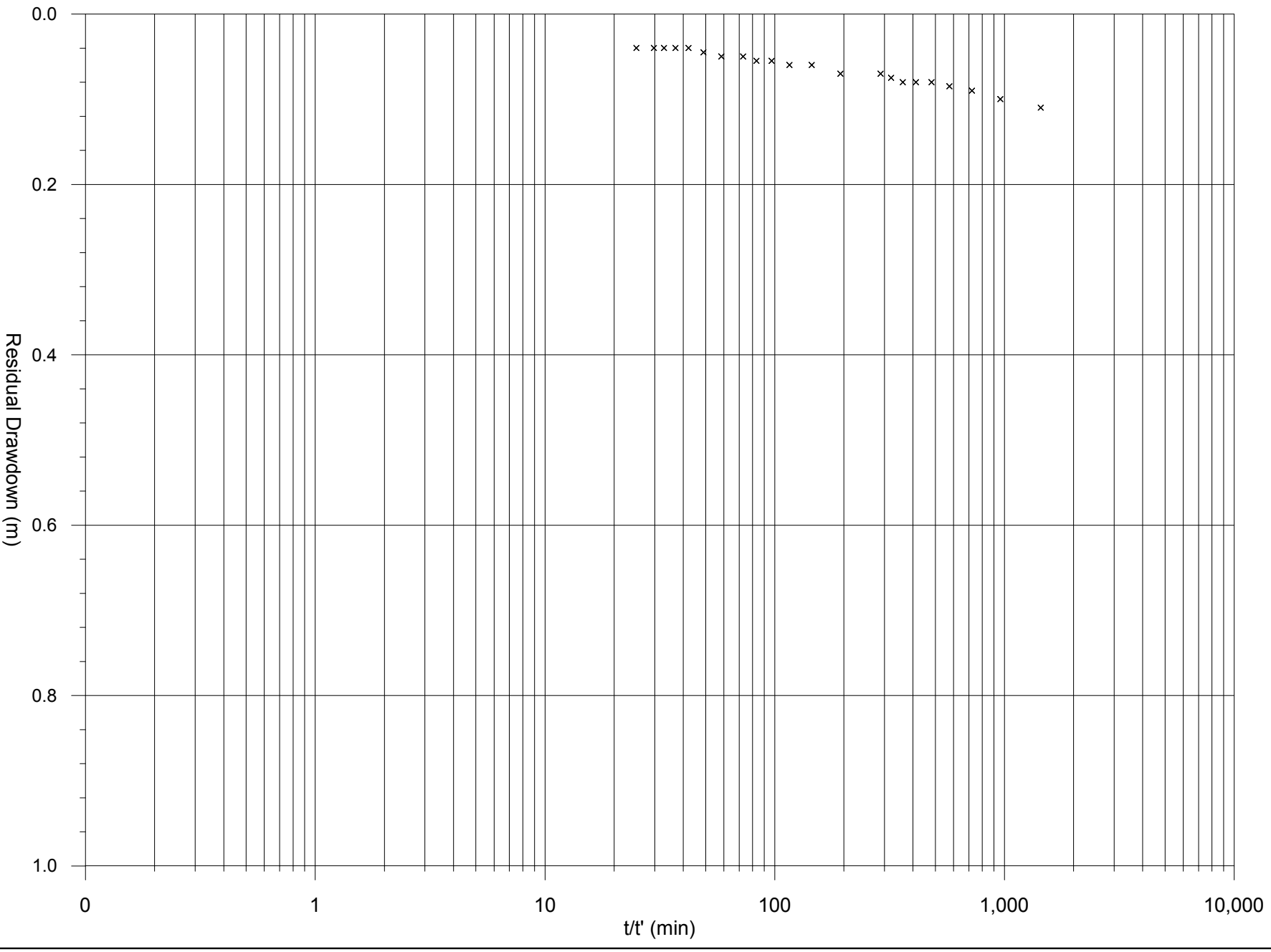


nbw1 ngw54c.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-4

BORE NBW1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
DRAWDOWNS IN NGW54C

Figure AIII-5

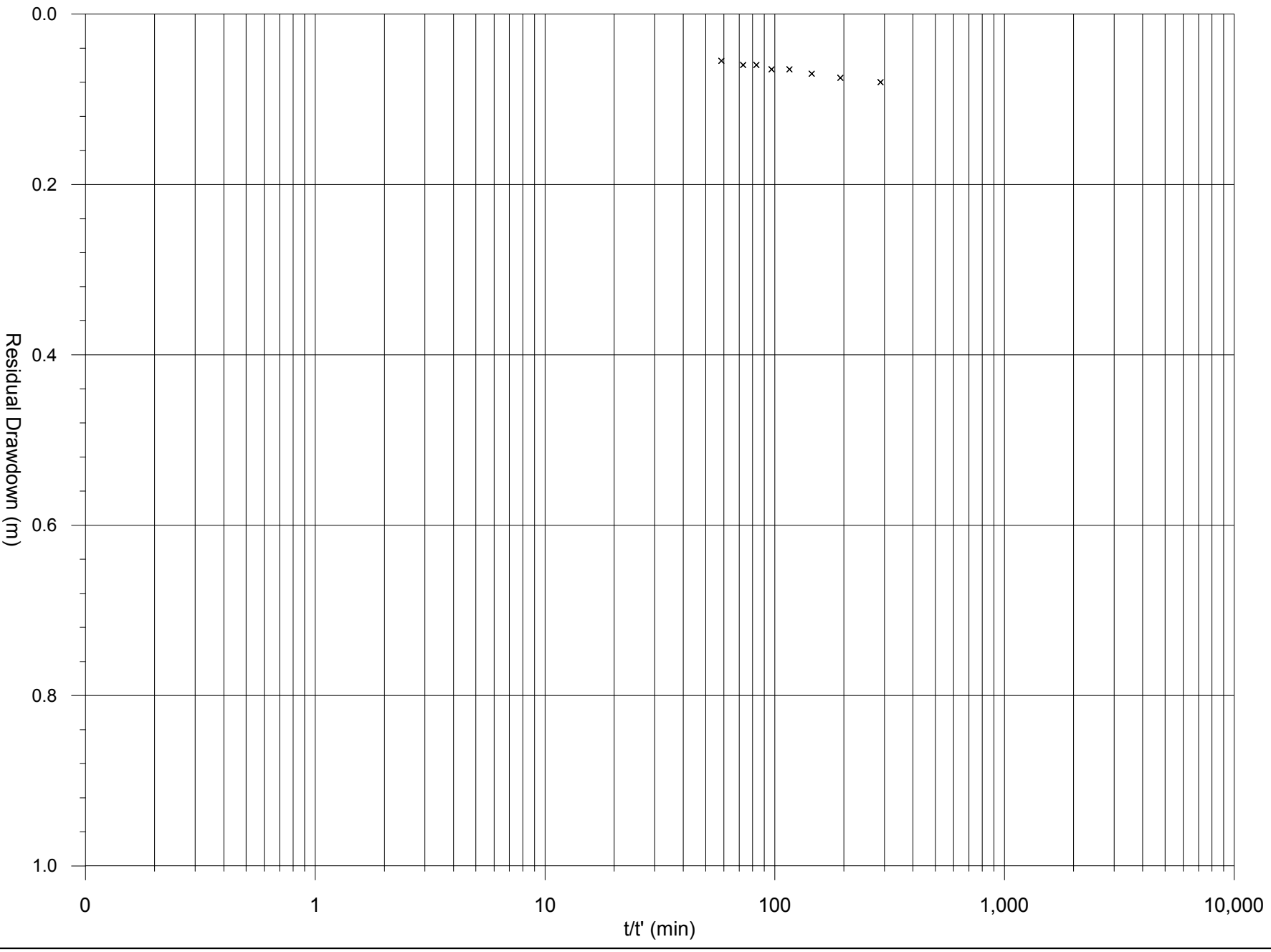


ngw37 recovery.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-5

BORE NWB1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
RECOVERY IN NGW37

Figure AIII-6

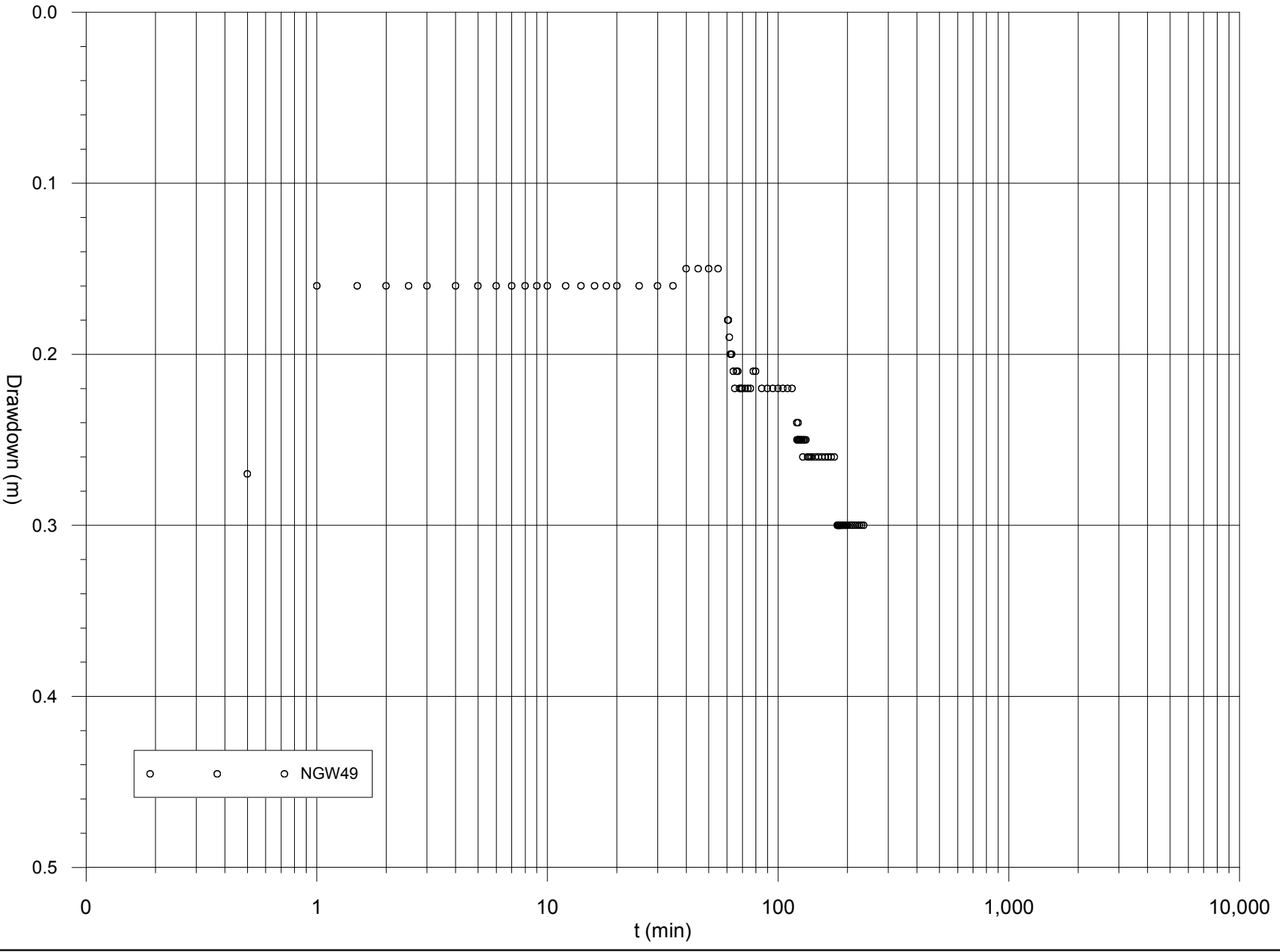


ngw54c_recovery.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-6

BORE NWB1 PUMPING TEST
AT 1,210 KL/d, 16/3/15
RECOVERY IN NGW54C

Figure AIII-7

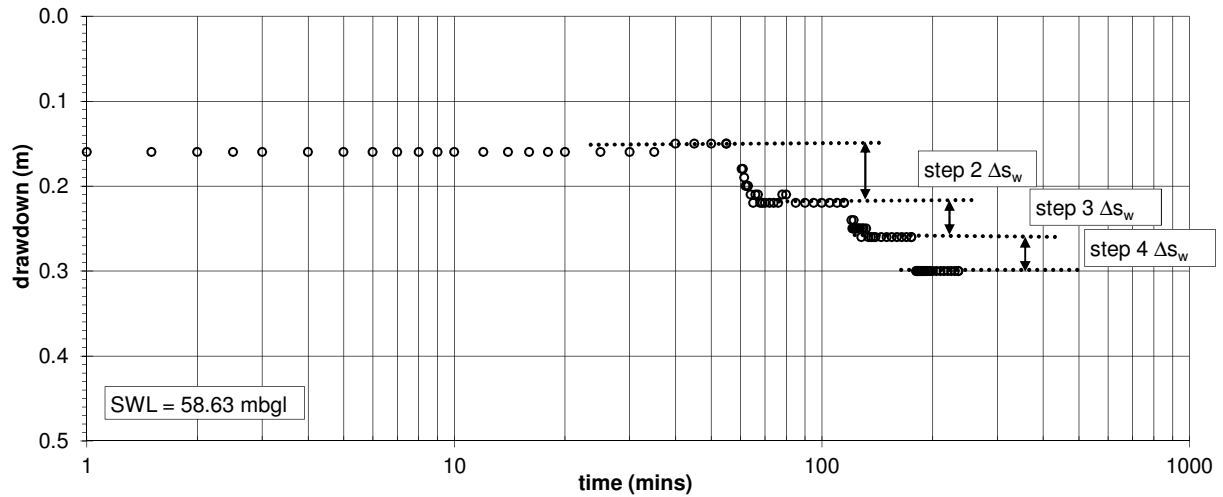


NWB2 step test.grf
Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-7

NWB2 PRODUCTION BORE
STEP-RATE PUMPING TEST
at 415 KL/d, 600 KL/d, 767 KL/d, 943 KL/d



Figure AIII-7A



$s=BQ+CQ^2$, where:

BQ is drawdown due to laminar flow

CQ^2 is drawdown due to turbulent flow

$s/Q=B+CQ$, so in plot of s/Q v. Q , B is the intercept

& C is the slope

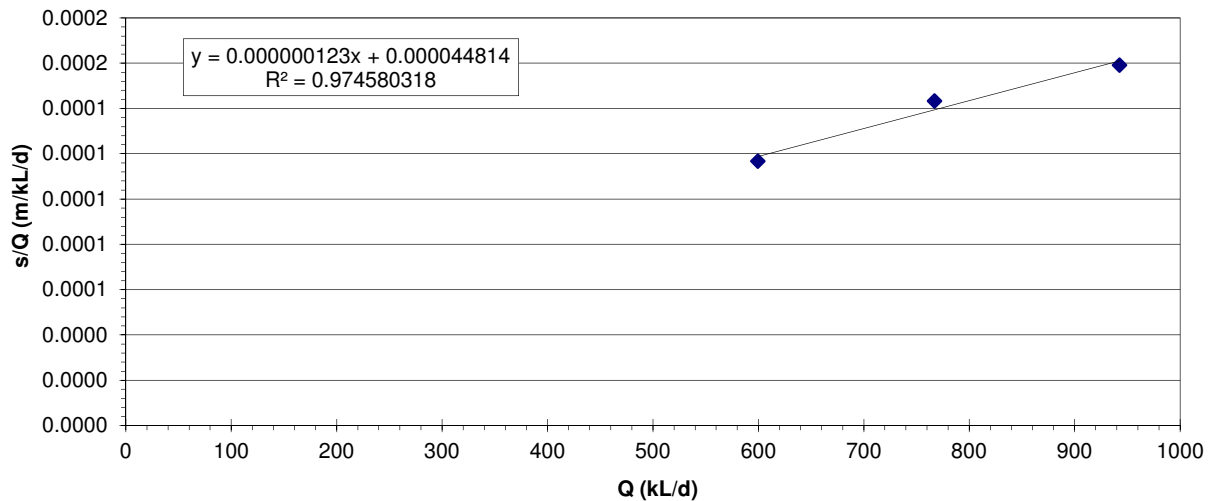
B = 4.5E-05 intercept

C = 1.2E-07 slope

Step	Q		stabilised drawdown (s)		s/Q m/kL/d
	L/s	kL/d	Δs_w (m)	total (m)	
1					
2	6.94	599.62	0.070	0.070	0.00012
3	8.88	767.23	0.040	0.110	0.00014
4	10.91	942.62	0.040	0.150	0.00016

predicted drawdown using B & C @ $Q=11$ L/s, = 0.15 m

actual drawdown from CRT @ $t=2873$ mins & $Q=11$ L/s, = 0.32 m



Drawdown due to turbulent flow in aquifer and bore (Lt)

$Lt=(CQ^2/(BQ+CQ^2))100$

Lt = 49.2 % at $Q=4$ L/s

Lt = 62.3 % at $Q=7$ L/s

Lt = 67.9 % at $Q=9$ L/s

Lt = 72.2 % at $Q=11$ L/s

345.0\Data\Pumping Tests\step test - NWB2 Analysis.xls

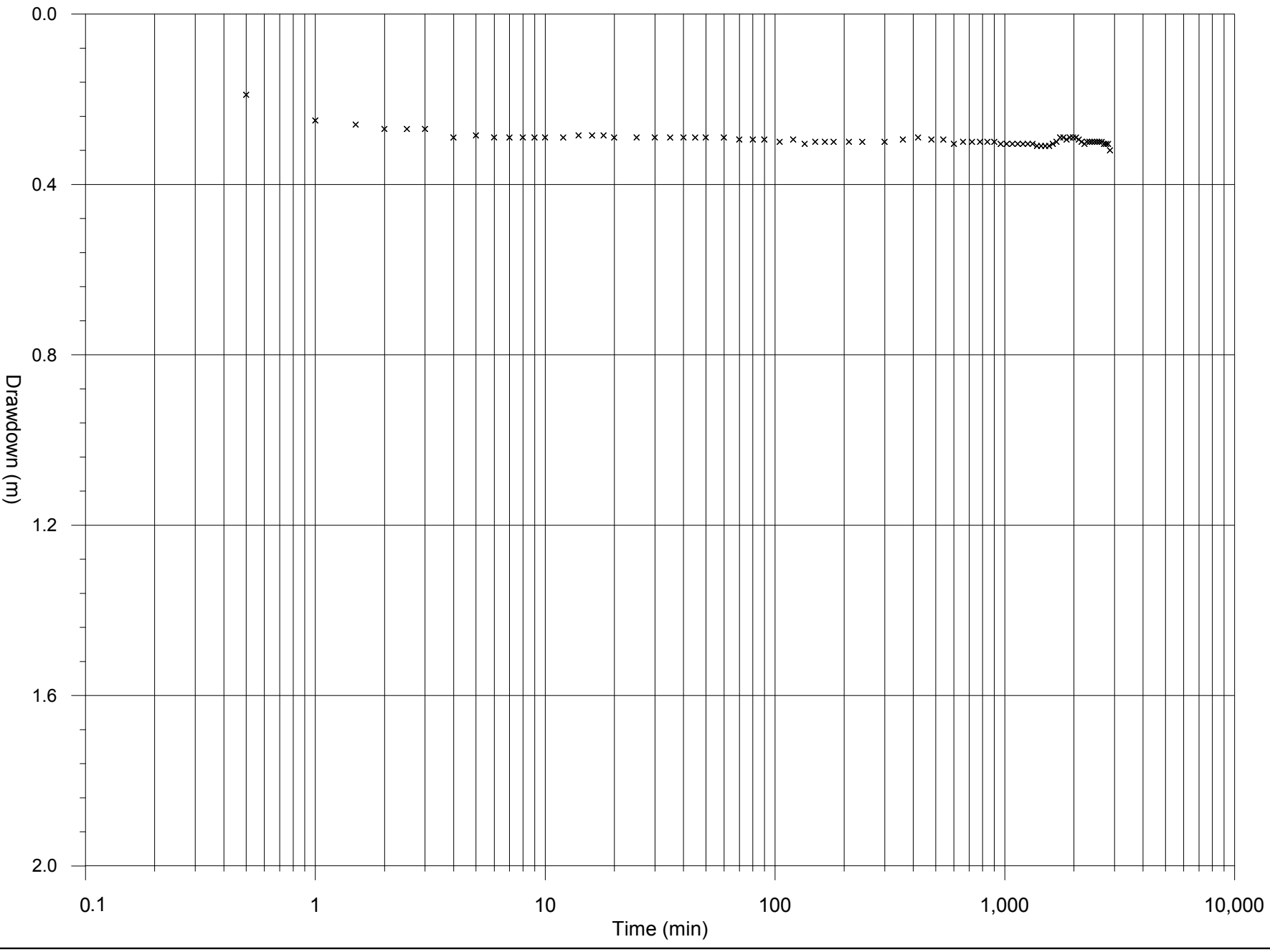
Client: Vimy Resources
 Project: 345-0
 Date: March 2015
 Dwg No. 345-0/15/1-AIII-7A

Bore NWB2 Step-rate Test Data with Analysis
 of Turbulent Flow



Rockwater Pty Ltd

Figure AIII-8

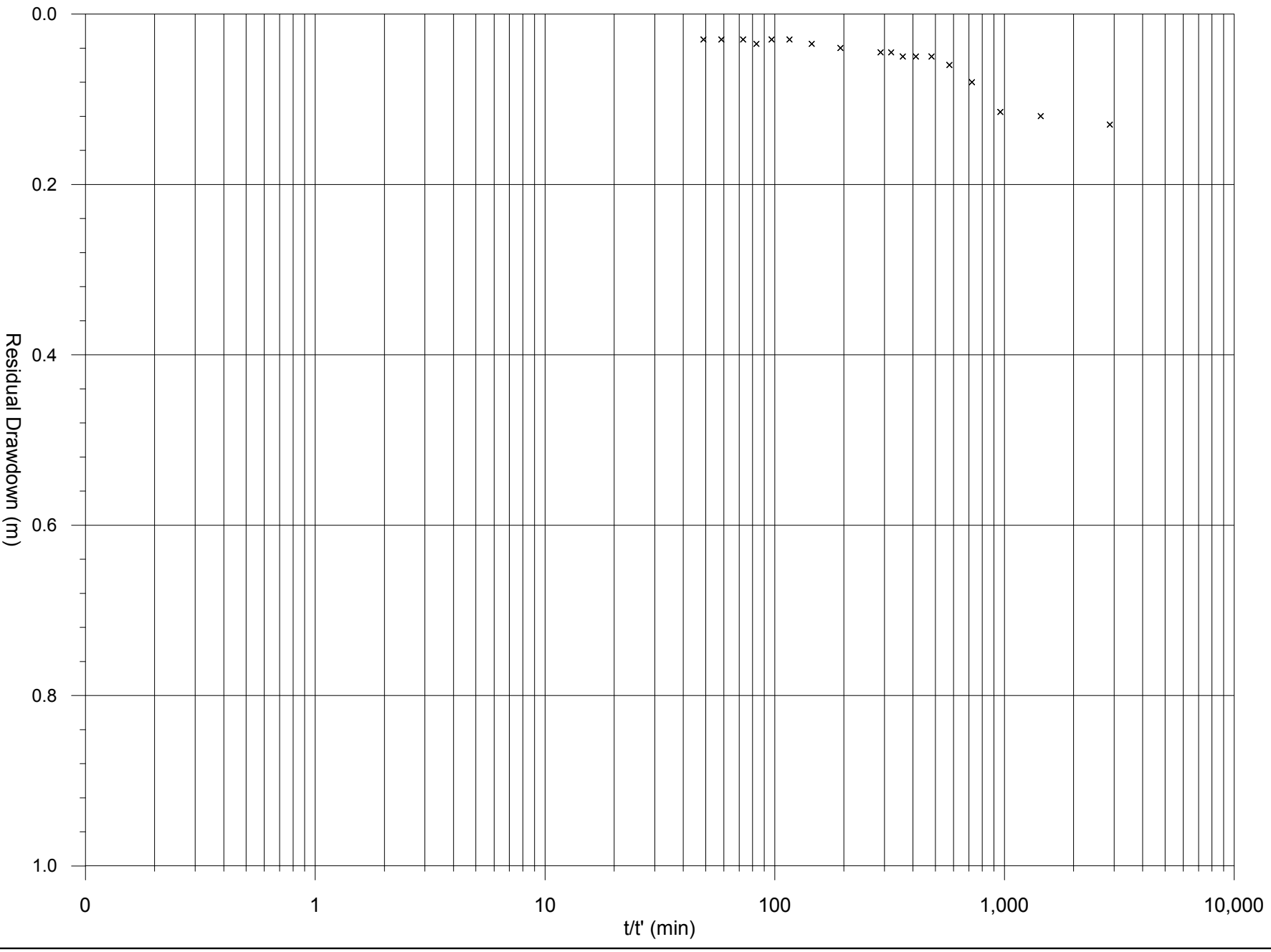


ngw2 prod.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-8

PRODUCTION BORE NGW2
PUMPING RATE 950 KL/d, Start 13/3/15
DRAWDOWN IN PUMPED BORE

Figure AIII-9

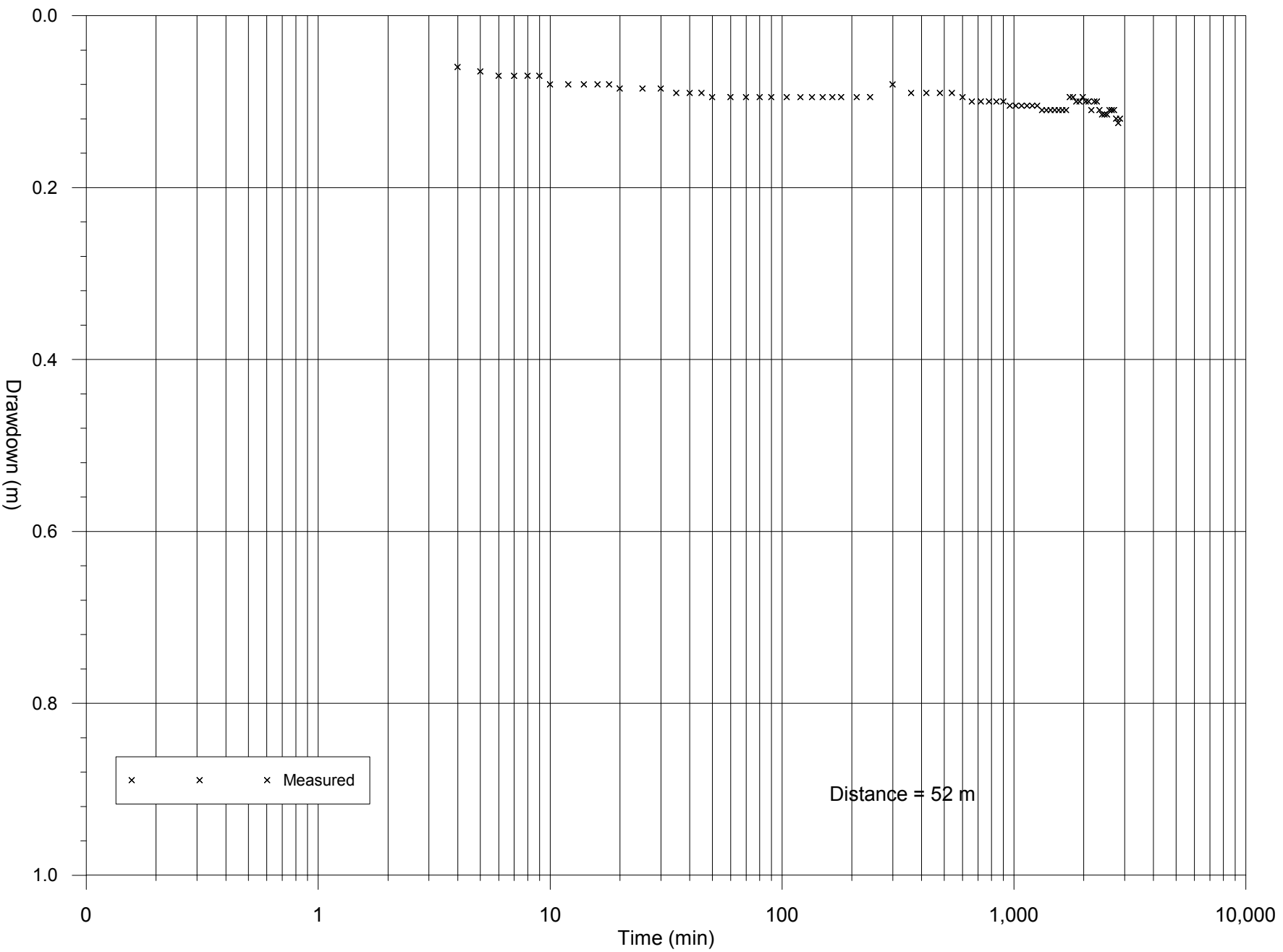


nwb2_recovery.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-9

BORE NWB2 PUMPING TEST
AT 950 KL/d, 7/3/15
RECOVERY IN NWB2

Figure AIII-10

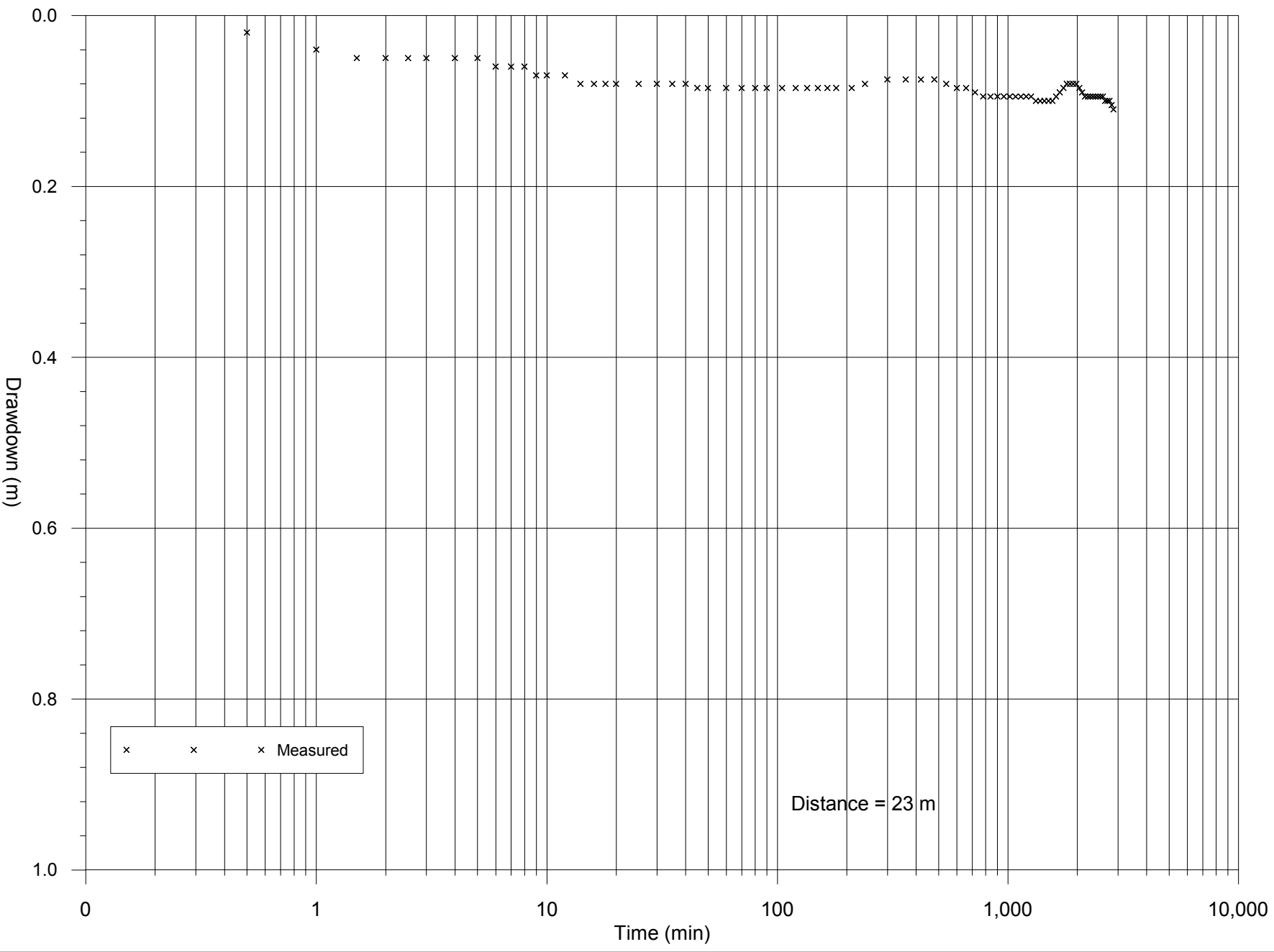


nbw2 ngw30.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-10

BORE NBW2 PUMPING TEST
AT 950 KL/d, 13/3/15
DRAWDOWNS IN NGW30

Figure AIII-11

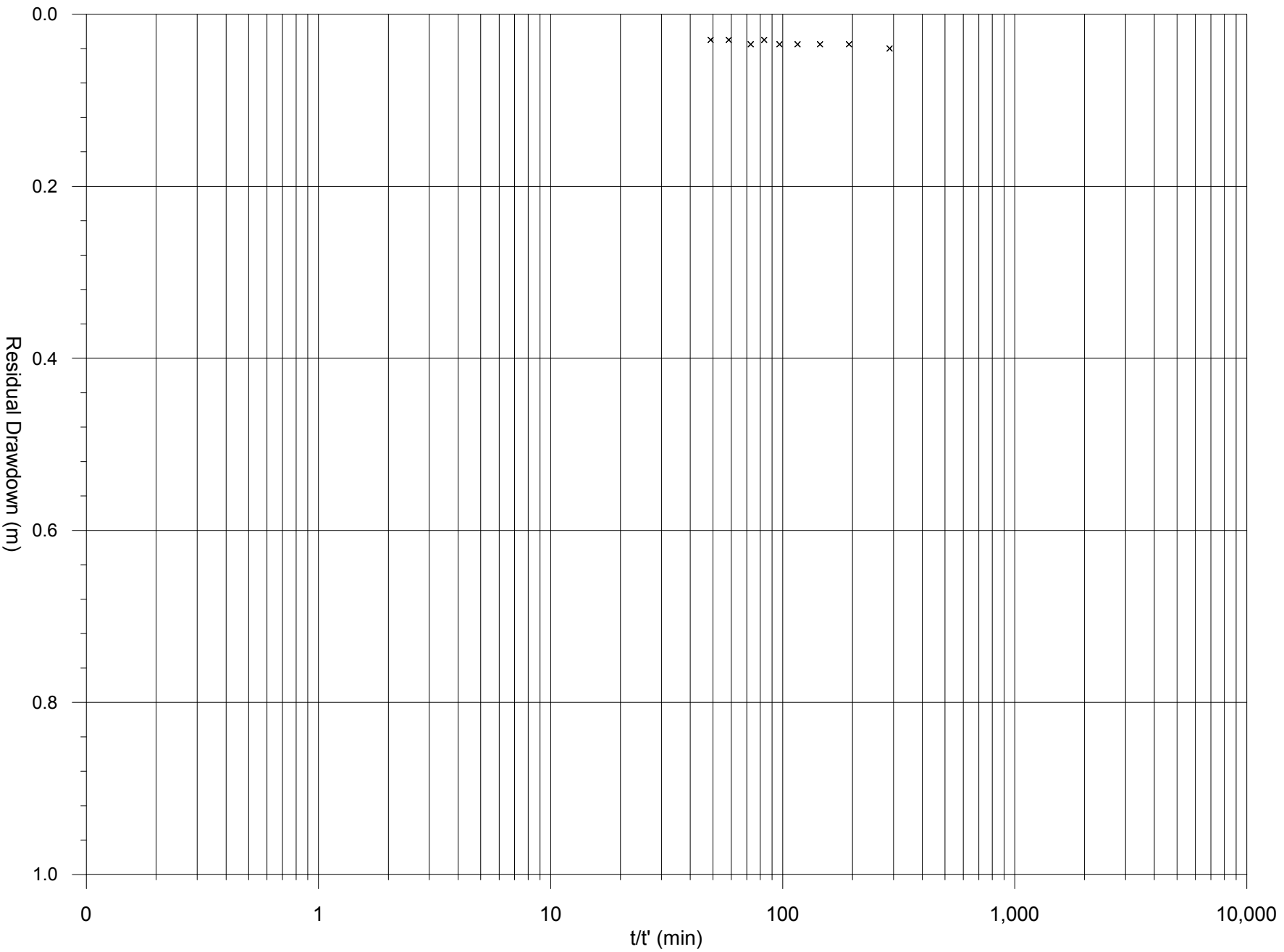


nbw2 ngw55.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-11

BORE NBW2 PUMPING TEST
AT 950 KL/d, 13/3/15
DRAWDOWNS IN NGW55

Figure AIII-12

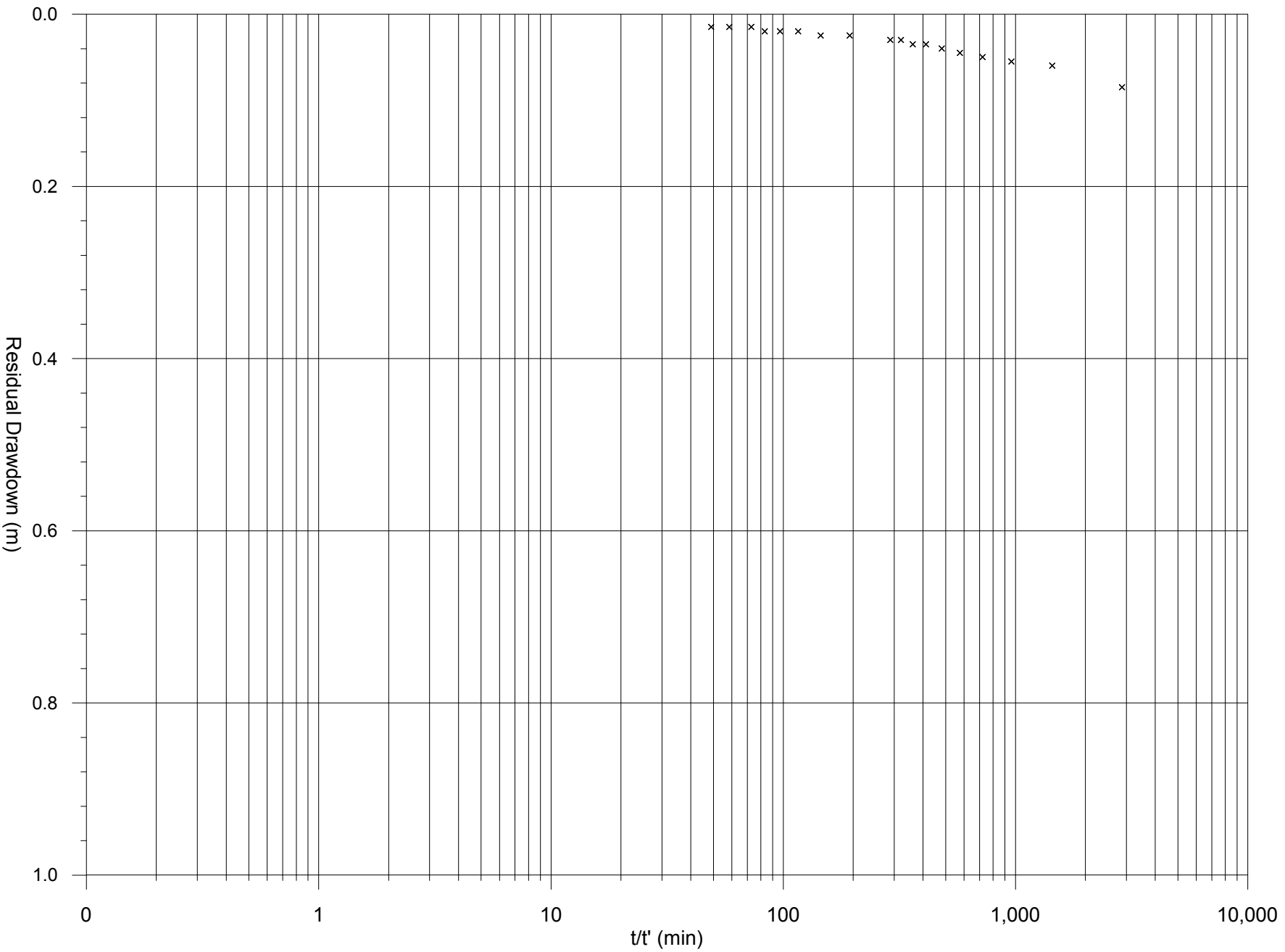


ngw30 recovery.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-12

BORE NWB2 PUMPING TEST
AT 950 KL/d, 7/3/15
RECOVERY IN NGW30

Figure AIII-13



ngw65 recovery.grf

Client: Vimy Resources
Project: Mulga Rock
Date: March 2015
Dwg. No: 345-0/15/2-AIII-13

BORE NWB2 PUMPING TEST
AT 950 KL/d, 7/3/15
RECOVERY IN NGW55