MULGA ROCK URANIUM PROJECT

RESULTS OF HYDROGEOLOGICAL INVESTIGATIONS AND NUMERICAL MODELLING, MULGA ROCK URANIUM PROJECT



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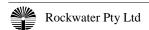
TABLE OF CONTENTS

			PAGE
1	INTI	RODUCTION	1
2	PRE	VIOUS INVESTIGATIONS	1
3	HYD	PROGEOLOGICAL SETTING	2
	3.1	Climate	2
	3.2	Regional Geological Setting	4
	3.3	Local Geology	4
	3.4	Hydrogeology	6
	3.5	Groundwater Chemistry	7
		3.5.1 Ambassador/Princess	8
		3.5.2 Emperor and Shogun Deposits	10
		3.5.3 Reinjection Area	12
4	BOR	E CONSTRUCTION AND PUMPING TESTS	12
	4.1	Drilling and Bore Construction	13
	4.2	Pumping Tests	13
		4.2.1 Bore NWB1	14
		4.2.2 Bore NBW2	16
	4.3	Slug Tests and Low-Flow Pumping Tests	17
5	NUM	MERICAL GROUNDWATER MODELLING	18
	5.1	Conceptual Hydrogeological Model	18
	5.2	Description of Numerical Model	20
	5.3	Model Parameters	20
	5.4	Model Calibration	21
	5.5	Model Simulation and Results	22
	5.6	Sensitivity Analysis	24
	5.7	Discussion of Modelling Results	24
6		ENTIAL ENVIRONMENTAL RECEPTORS	25
	6.1	Queen Victoria Spring	25
	6.2	Palaeochannel Aquifer	25
7		ICLUSIONS	26
REF	FERENC	CES	27

CONTENTS (Continued)

Tables

Table	e 1: Average Monthly Rainfall (mm) Edjudina (BoM Station 012027)	
Tabl	e 2: Comparison of Annual Rainfall, Edjudina and Mulga Rock Airstrip	3
Tabl	e 3: Monthly Rainfall (mm) at the MRUP Climate Stations	3
Tabl	e 4: Comparison between Average Pan Evaporation at Kalgoorlie and the MRUP (20)	14) 3
Tabl	e 5: Results of Major Component Analyses (and Common Metals) 1984	ç
Tabl	e 6: Results of Major Component Analyses (and Other Elements and Metals) 2010	11
Tabl	e 7: Summary of Production Bore Details	13
Tabl	e 8: Results of Pumping and Recovery Tests	14
Tabl	e 9: Results of Pumping and Recovery Tests, NWB1	15
Tabl	e 10: Physico-Chemical Measurements made during NWB1 Test	15
Tabl	e 11: Results of Pumping and Recovery Tests, NWB2	16
Tabl	e 12: Physico-Chemical Measurements made during NWB1 Test	17
Tabl	e 13: Results of Slug and Low-Flow Pumping (Recovery) Tests	19
	e 14: Adopted Aquifer Parameters	20
	e 15: Calculated Dewatering Flows and Injection Rates	23
Tabl	e 16: Results of Sensitivity Analysis	24
Figu	ires	
1	Location of Mulga Rock Uranium Project	
2	MRUP and Nearby Communities	
3	MRUP Mining Centres and Associated Resources	
4	Maximum & Minimum Temperatures, and Monthly Rainfalls, Mulga Rock Weather	er
	Stations	
5	Regional Geological Setting	
6	Reduced Groundwater Levels (m AHD) Measured in all Bores at Various Times	
	(Contours), and in Calibration Bores (Post Values)	
7	Groundwater Levels (m AHD) Measured April 2014, Ambassador Deposit	
8	Hydrogeological Cross-Section Injection Borefield at NWB1 (Line A)	
9	Hydrogeological Cross-Section South of Injection Borefield, Line B	
10	Salinities (mg/L TDS) Measured at Various Times	
11	PH Measured at Various Times	
12	Piper Diagram of Groundwater Samples, Mulga Rock Deposits	
13	Reinjection Area: Salinity versus Sampling Depth	
14	Production Bore Locations	
15	Model Grid	
16	Comparison between Groundwater Levels (m AHD) Measured at Various Times (l	Post
	Values), and Model Calculated Levels (Contours)	
17	Bore NWB1 Pumping Test at 1,210 kL/d, 16/3/15, Drawdowns in NGW37	
18	Bore NWB1 Pumping Test at 1,210 kL/d, 16/3/15, Drawdowns in NGW54C	
	1 0 / /	



CONTENTS (Figures, Continued)

- Bore NWB2 Pumping Test at 950 kL/d, 13/3/15, Drawdowns in NGW30
- Bore NWB2 Pumping Test at 950 kL/d, 13/3/15, Drawdowns in NGW55
- 21 Mine Plan, Ambassador and Princess Deposits
- 22 Mine Plan, Emperor and Shogun Deposits
- 23 Planned Base of Mining (m AHD) Ambassador and Princess Deposits
- 24 Planned Base of Mining (m AHD) Emperor and Shogun Deposits
- 25 Model-Calculated Drawdowns (m) Layer 1, End of Year 10
- Model-Calculated Drawdowns (m) Layer 3, End of Year 10
- 27 Model-Calculated Drawdowns (m) Layer 1, End of Year 16
- 28 Model-Calculated Drawdowns (m) Layer 3, End of Year 16
- 29 Model- Calculated Maximum Drawdowns (m) During 16 Year LoM
- 30 Model-Calculated Flowpaths from the End of Mining (Layer 3)

Appendices

- I Geological Sections
- II Results of Chemical Analyses
- III Construction Details & Pumping Test Plots for Production Bores NWB1 and NWB2

VERSION	AUTHOR	REVIEW	ISSUED
15-002	PHW	JRP	19/05/2015
15-002a	PHW	JRP	29/05/2015
15-002b	PHW	JRP	4/06/2015
15-002c	MJT		23/10/2015
15-002d	MJT		29/10/2015

1 INTRODUCTION

The Mulga Rock Uranium Project (MRUP) lies approximately 240km east-north-east of Kalgoorlie-Boulder in the Shire of Menzies (Figure 1). The area is remote, located on the western flank of the Great Victoria Desert, comprising a series of large, generally parallel sand dunes, with inter-dunal swales and broad flat plains.

Access to the Project area is limited and is only possible using four-wheel-drive vehicles. The nearest residential town to the Project is Laverton which lies approximately 200km to the north-west. Other regional residential communities include Pinjin Station homestead located approximately 100km to the west, Coonana Aboriginal community situated approximately 130km to the south-south-west, Kanandah Station homestead positioned approximately 150km to the south-east and the Tropicana Gold Mine lying approximately 110km to the north-east of the Project (Figure 2).

The MRUP covers approximately 102,000 hectares on granted mining tenure (primarily M39/1080 and M39/1081) within Unallocated Crown Land. It includes two distinct mining centres, Mulga Rock East (MRE) comprising the Princess and Ambassador resources, and Mulga Rock West (MRW) comprising the Emperor and Shogun resources, which are approximately 20km apart (Figure 3). MRE contains over 65% of the total recoverable uranium and is of a higher grade than MRW. Mining will commence at MRE, which will include the location of the processing plant. Up to 4.5 Million tonnes per annum (Mtpa) of ore will be mined using traditional open cut techniques, crushed, beneficiated and then processed at an acid leach and precipitation treatment plant to produce, on average, 1,360 tonnes of uranium oxide concentrate (UOC) per year over the life of the Project. The anticipated Life-of-Mine (LOM) is up to 16 years, based on the currently identified resource.

This report presents the results of geological and hydrogeological investigations in the planned mining area, as well as numerical modelling to determine dewatering pumping rates and the potential impacts of groundwater reinjection, to support an application to the Department of Water (DoW) for licences to take and reinject water. The model can also be used to assess the impacts of tailings disposal.

2 PREVIOUS INVESTIGATIONS

There are many publications describing palaeodrainages and palaeochannel aquifers in Western Australia such as the one that hosts the Mulga Rock deposits. These include Van der Graaff *et al.* (1977); de Broekert and Sandiford (2005); Magee (2009); and English *et al.* (2012).

GRC (1984) reviewed all available data for PNC Exploration Pty Ltd (PNC) which held the Mulga Rock Uranium Project then, and carried out hydrogeological assessments for the mine water supply, dewatering of the Emperor, Shogun and Ambassador deposits, and potential environmental impacts.

Following the above study, a programme of drilling, bore construction and test-pumping was completed, and a reconnaissance was made for a source of low-salinity water (GRC, 1985). Six additional sites were drilled to explore for low-salinity water (GRC, 1986), but with little success.

Douglas et. al. (1993) completed a detailed investigation of the hydrochemistry of groundwater from the Ambassador deposit as well as the chemistry and mineralogy of the lignite.

Rockwater (2010, and 2013) conducted dewatering and water-supply investigations for the MRUP. This report updates and expands the information contained in those reports. Rockwater (2015) prepared a separate report on the planned low-salinity (Kakarook North) borefield.

3 HYDROGEOLOGICAL SETTING

3.1 CLIMATE

The MRUP is located in the Great Victoria Desert and has an arid climate with hot dry summers and cool to mild winters. The nearest long-term climate station is at Edjudina (BoM Station 012027), 145 km to the west of the Ambassador deposit. Average rainfall data for the station (1900 to 2014) are given in Table 1.

Table 1: Average Monthly Rainfall (mm) Edjudina (BoM Station 012027)

Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Total
22.4	28.2	26.1	19.6	22.0	22.1	19.2	16.7	9.7	11.8	14.0	12.8	222.6

Most of the rain falls in irregular thunderstorm events or during the passage of the remnants of cyclones, with some frontal systems in winter. Daily rainfalls have been up to 98 mm (in February). No other climate data are available for the station.

The MRUP has maintained climate stations at the airstrip and at the Emperor and Shogun deposits since March 2009. A suite of climatic measurements has been made including rainfall, maximum and minimum air temperature, and pan evaporation.

Rainfall at the MRUP airstrip from 2010 to November 2014 can be compared with those at Edjudina in Table 2.

Table 2: Comparison of Annual Rainfall, Edjudina and Mulga Rock Airstrip

Year	Tota	l Rainfall (mm)
	Edjudina	Mulga Rock Airstrip
2010	222	173
2011	503	433
2012	337	129
2013	284	170
2014 to Nov.	469	160

The comparison in annual rainfall amounts over the period shown in Table 2 suggests that the climate at the MRUP is substantially drier than at Edjudina. Monthly rainfall data for the three MRUP climate stations are shown in Table 3. These also show a general decrease in rainfall from west (Emperor) to east (Airstrip).

Pan evaporation at the MRUP airstrip station from Dec-13 to Nov-14 was significantly lower than the average for Kalgoorlie (Luke, Burke and O'Brien, 1988), as shown in Table 4.

Table 3: Monthly Rainfall (mm) at the MRUP Climate Stations

Month			Airstrip			1		Emperor					Shogun		
Month	2010	2011	2012	2013	2014	2010	2011	2012	2013	2014	2010	2011	2012	2013	2014
January	9.3	58.7	23.6	15.2	65.7	0	108.2	55.4	20.8	128.8	3	105.8	62.6	15.2	116.6
February	10.3	191.3	13.7	7.5	31.3	12.6	252.4	23	3.8	51.8	15	247.4	21.6	10.2	49.2
March	5.9	9.3	20.7	36.6	3.3	3.6	17	47.4	70	11.8	11.2	18.2	48.8	58.2	12.2
April	31.3	20.3	0.7	8.6	0.9	38.2	28.8	0.2	14.6	21.4	53	33.8	0.2	16.6	12
May	8	11.2	2.6	18.7	17.2	7.3	17.4	2.6	18.2	38.4	9.1	19.8	3	31	31.6
June	7.8	57.2	6.9	4.5	4.6	7.8	85.2	10	5.8	6.6	9.6	82.2	13.2	7.2	7.2
July	8.8	21	2.1	8.1	2.5	13.2	38.4	2.4	14.7	4	12	36.2	3.4	13	4
August	55.1	1.9	0.6	2.1	0.4	86.8	3	1.4	3.4	1.2	79.2	3	0.8	1.8	1.2
September	27.4	2.1	0.6	5.8	5.1	36.4	5.6	1	13.2	7.6	36.2	4	0.8	10	6.8
October	1.5	36.7	3.8	0.9	9	0.6	61.4	9.4	1.2	19.2	1.8	59.2	6.4	2.8	17.4
November	1.9	12.2	35.1	47.9	21.6	2	24.4	48	65.4	30	1	24.2	50.8	57.2	32
December	7.7	12.7	17.5	15	N/A	7.4	28.8	53.8	16.8	N/A	9	22.8	28.4	16	N/A
Annual Total	175	434.6	127.9	170.9	161.6	215.9	670.6	254.6	247.9	320.8	240.1	656.6	240	239.2	290.2

Table 4: Comparison between Average Pan Evaporation at Kalgoorlie and the MRUP (2014)

<u></u>	Jan	Feb	Mar	Apr	May	Jun	Jul	Aug	Sep	Oct	Nov	Dec	Year
MRUP (2014)	306	280	225	211	150	91	81	90	140	206	255	276	2309
Kalgoorlie (Av.)	431	346	306	199	133	93	103	130	181	271	326	424	2943

Maximum and minimum air temperatures at the three MRUP weather stations are shown with monthly rainfalls in Figure 4. The temperatures are very similar at all three stations. In 2014, average maximum air temperatures ranged from 18.6 °C in June to 34.6 °C in January; and average minimum temperatures ranged from 1.1 °C in July to 18.0 °C in January.

3.2 REGIONAL GEOLOGICAL SETTING

Mineral exploration holes drilled by Vimy and its predecessor PNC, as well as other companies including Uranerz and Paladin, have shown that the Mulga Rock palaeodrainage is about 8 to 10km wide. The eastern arm of the palaeochannel is probably continuous over a length of at least 65 km, and is interpreted in plans and sections in Uranerz (1986) to be hydraulically connected to a trunk palaeochannel that follows Ponton Creek to the south and is downstream of the confluence of the Lake Raeside, Lake Rebecca and Roe palaeochannels (Fig. 5).

The palaeodrainage skirts a southerly extension of the Gunbarrel Basin, which contains sediments of Carboniferous to Pleistocene age, and is bounded by crystalline rocks of the Yilgarn Craton of Archaean age to the west and the Albany Fraser Province of Proterozoic age to the east (Fig. 5).

3.3 LOCAL GEOLOGY

The geology of the eastern part of the MRUP, from information provided by Vimy, can be summarised as follows.

Ambassador is a sediment-hosted uranium deposit. This deposit, together with the other MRUP deposits, occurs within the Narnoo Basin, a local name for the host structure. The mineralisation is primarily in geochemically reduced sediments of Eocene age, preserved within a complex set of sedimentary troughs overlying an extensive paleodrainage referred to as the Mulga Rock palaeochannel, which is probably an isolated oxbow channel of the Lake Raeside regional paleodrainage.

The reduced sediments that contain the Ambassador and other deposits are part of a sedimentary package named the Narnoo Basin Sequence. This sequence consists of multiple fining-upwards units including sandstone, claystone (typically carbonaceous) and lignite which were deposited in alluvial and lacustrine environments.

Sedimentation within the Eocene palaeochannel is interpreted as a transgressive sequence. The lowest part of the sequence is dominated by medium to coarse, marginally carbonaceous sands. These sands are mostly devoid of clay and are highly transmissive to groundwater flow. The central portion of the sequence is dominated by fine textured, organic-rich sediments (highly carbonaceous fine sands, lignitic clays and lignite) containing humic macerals of low reflectance (huminite). These fine textured, sediments occur at and near the maximum flooding surface of the transgression. The upper portion of the sediments are dominated by stacked beds of reverse graded (upward coarsening) sands that represent the progradational portion of the transgression.

The main sequence of Late Eocene lacustrine sediments correlates regionally with the third-order transgressive sequences of the Tortachilla cycle (~39 Ma) whilst the youngest Late Eocene sediment correlates with the Tuketja (~36 Ma) transgressive cycle.

Cretaceous sediments are dominant in the north-eastern part of the Ambassador deposit and also occur around the deposit margins. Although superficially similar to the late-Eocene palaeochannel sediments, they do not have the regular transgressive sequence of the later sediments and are characterised by beds of black, mature forms of carbonaceous material such as inertinite and glassy vitrinite. The Cretaceous sediments are probably remnants of a formerly deeply buried sequence that covered much of southern Australia prior to the Late Cretaceous (Albian-Maastrichtian) uplift.

Overlying the Narnoo Basin Sequence is a succession of oxidised sediments which at Ambassador are about 36 to 55 m thick. Pre-Cretaceous and Eocene basement in the Ambassador area consists of a Carboniferous sedimentary succession, as well as Paleoproterozoic metasediments to the east of the Gunbarrel fault. The Carboniferous sediments are assigned to the Paterson Formation and understood to be part of the Gunbarrel Basin.

Mineralisation is believed to have formed via biogenic processes, through the fixation of metals in solution that were mobilised in the course of repeated weathering episodes, resulting in the leaching of the upper part of the Eocene and thick sections of Cretaceous sediments upgradient of the deposits. This weathering is akin to acid-sulphate weathering processes, oxidising sulphides and organic matter and organic carbon resulting in very aggressive groundwater conditions (low pH and elevated temperature), and thereby mobilising metals and metalloids (including silica) from the overburden. The remnant, highly altered material is typically strongly bleached and characterised by a kaolinite fraction of notably high crystallinity (due to dissolution and recrystallisation of the clay).

The uranium mineralisation is assumed to be similar in nature to that studied at Ambassador via multiple recent spectral, mineralogical, deportment and metallurgical studies, showing that the bulk of the uranium is in a hexavalent ionic state and adsorbed onto organic matter, with a negligible fraction contained in refractory minerals.

Similarly, the majority of base metals in the deposits are expected to be bound to organic matter, with a significant fraction in sulphate phases and a lesser fraction in supergene sulphide phases.

3.4 HYDROGEOLOGY

The water table at the Ambassador deposit is 29 m to 49 m deep, and generally lies within fine-grained, carbonaceous sediments of Eocene age; and in the north-east, of Cretaceous age. The mineralised zones are mainly just below the water table, but some extend down into the coarse-grained sediments towards the base of the palaeochannel (see the geological sections in Appendix I).

Reduced groundwater levels within the palaeochannel that have been measured at various times are shown in Fig. 6, with values shown for representative bores that were used to calibrate the groundwater model described in Section 5 below. They show that in most of the Narnoo Basin/paleochannel the water table is very flat, at an elevation of about 288 to 290 m AHD, and that there is very little flow into the basin (or recharge) and out of the basin (discharge). Hydraulic gradients suggest there is minor flow into the basin from the northeastern tributary that includes the Ambassador deposit; and a small component of flow into the basin from the north-west.

Limited data suggest there is flow from north to south in the western arm under a low hydraulic gradient. There is also indicated to be flow to the south in the eastern arm, south of about 6655000 mN – the steeper hydraulic gradient there is attributed to a narrowing of the channel containing coarse-grained sediments and lower transmissivity as indicated by Uranerz Section 92,500 N, which is at about 6655700 mN (GDA) (Appendix I). There, much of the channel is filled with fine-grained sediments.

Water-level measurements taken in April 2014 in the Ambassador area (Fig. 7) show that the water table is very flat in Ambassador East at about 299 m AHD; and with a low hydraulic gradient from 291 m to 293 m AHD in Ambassador West. There is a relatively steep gradient between these two parts of Ambassador due to the presence of a high of Permian sediments separating the Eocene sediments in each area. This is shown by the Long Section N30 in Appendix I.

Seasonal and annual water-level variations are very small, showing there is very little recharge to the aquifer and no extraction or significant flow out of the basin. Groundwater levels were monitored every one to three months in 38 bores in the Ambassador area from 2010 to 2014. Most of the August 2012 measurements were in error, presumably due to a faulty probe. Without those measurements, the range in water-level fluctuations in the bores was from 0.05 m to 0.76 m, and averaged 0.25 m. The higher ranges probably included some measurement errors and the impacts of pumping for sampling, and so the actual range and average would have been lower.

The results of pumping tests of three bores screened in the basal Eocene palaeochannel sediments (Section 4) indicate that these sediments are moderately to highly permeable, with

hydraulic conductivities ranging from 9 to 140 m/d. The low value is typical of these sediments where tested elsewhere in the Eastern Goldfields. The high values at bores NWB1 and 2 in the planned injection area reflect the local gravels screened by the bores. Hydrogeological sections through these bores are presented in Figs 8 and 9. The section lines are shown in Fig. 6.

The fine-grained sediments higher in the palaeochannel, generally associated with the mineralised zones, will have low hydraulic conductivity as shown by the results of slug tests (Section 4.3).

The groundwater is unconfined at the water table, but confined below by the fine-grained sediments above and within the basal sands and gravels.

3.5 GROUNDWATER CHEMISTRY

Douglas *et. al.* (1993) concluded that groundwater at the MRUP differs from that in other Yilgarn palaeochannels, having low oxidation potentials with anomalous isotope effects and low concentrations of a number of trace elements. All of these differences were attributed to the high organic content of sediments at the site. They also noted that groundwater at Ambassador, in a tributary palaeochannel, is geochemically distinct from that in the main palaeochannel, which includes the Emperor and Shogun deposits. The main palaeochannel contains groundwater that is more saline, depleted in K, Ca and Sr, and enriched in Al, Fe and Mn relative to Ambassador. Conversely, Ambassador groundwater is significantly enriched in dissolved HCO₃, PO₄, Ba, U and W; and is depleted in dissolved Si. This is consistent with younger groundwater flowing down the Ambassador channel into the main palaeochannel system.

Douglas *et. al.* (1993) also state that the geochemistry of groundwater in the Ambassador mineralized zone may relate to interactions between groundwater and solid organic matter, and/or the inflow of water from a different source. The latter possibility is supported by the lower salinity at Ambassador.

The chemistry of water samples taken from each of the project areas is discussed below. Salinities are shown in Fig. 10, pH in Fig. 11, and a trilinear (Piper) diagram showing major ion composition is given in Fig. 12. Water from all the MRUP deposits is of similar ionic composition (Fig. 12), although the water from Ambassador tends to have proportionately higher sodium and chloride and lower magnesium and sulphate than water from some of the other deposits.

3.5.1 Ambassador/Princess

Water samples have been analysed at various times for different suites of parameters from 97 drillholes in total at the Ambassador and Princess deposits. The results of all the analyses are given in Appendix II, and the results from some of the separate sampling events for the Ambassador deposit are described below.

1984 to 1991 Samples

Water samples collected from Bores 1 and 7 at the end of pumping tests in 1984 were analysed for major components (GRC, 1985). Water samples airlifted from 13 drillholes in and near the Ambassador deposit in 1990 and 1991 were also analysed for major components as well as a wide range of metals and rare earth elements (Douglas *et. al.* 1993).

The results of the major component analyses and some other common elements are given in Table 5.

The analyses show that the water ranges in salinity from 7,500 to 37,600 mg/L TDS. It is moderately acidic to neutral with pH ranging from 4.3 to 7.0 (generally 5.5 to 6.6); and is of a sodium chloride type with elevated magnesium and sulphate. Metals and other elements that were analysed for (most are not shown in Table 5) were generally at low concentrations. Exceptions were moderate concentrations of iron in several holes (up to 16 mg/L); and high bromine concentrations (up to 23 mg/L). Uranium concentrations were mostly below the limit of detection (0.002 mg/L), with a maximum of 0.038 mg/L.

Oxidation potentials (Eh) range from -167 to 335 mV and are generally greater than 100 mV indicating potentially oxidising conditions. It is likely that the low pH in hole CD1515 resulted from oxidation of sulphides, and increased rates of oxidation will almost certainly occur when the lignite is dewatered.

The areal distribution of the salinity data for all the deposits and sampling programmes is shown in Figure 10. Salinity increases to the south-west in the direction of groundwater flow, mostly from 20,000 to 40,000 mg/L TDS. Salinity also tends to increase with sample depth with moderate correlation, although the main water-bearing zones in each hole have not been identified.

Two holes, CD1366 and CD1409, had much lower salinities than in the other holes. Douglas *et. al.* (1993) consider that this resulted from contamination with rainwater in CD1366; and CD1409 has a high bicarbonate concentration and low sulphate that suggests that the water is young and that there is a high rate of recharge from rainfall/runoff.

Hole/Bore HCO3 TDS Mg Cl **SO4** NO3 Si рΗ Eh Na Κ Ca Fe Mn Br Sr (mg/L) (mg/L)(mg/L)(mg/L)(mg/L) (mg/L) (mg/L) (mg/L)(mg/L)(mg/L)(mg/L)(mg/L)(mg/L)(mg/L)(mV) 37,609 11,100 19,800 Bore 1 6.5 ND 260 800 1,400 89 4,150 10 12.8 ND ND ND ND RC1148 5.98 129 22,678 6,800 248 532 742 11,800 86 2,490 ND 0.4 0.2 23.1 6.9 21 Bore 7 5.8 ND 36,771 11,000 250 770 1,280 19,600 10 3,850 16.2 ND ND ND ND 11 3,769 6,730 1,250 RC1213 5.46 148 12,506 138 246 350 24 ND 0.46 0.22 10.6 3.3 21 RC1152 5.91 143 19,522 5,645 231 450 700 10,400 30 2,060 ND 0.15 0.13 20.7 6.3 22 RC1151 6.36 14,784 4,392 169 319 7,810 104 1,560 0.88 0.24 15 4 15.4 144 467 ND RC1419 6.85 173 14,535 4,185 204 300 522 7,430 283 1,730 ND 6.3 0.05 20.3 3.4 6.3 CD1500 5,276 9,820 0.27 6.01 293 18,459 207 415 651 107 2,020 ND 1.02 16.6 4.1 4 CD1498 6.58 335 32,875 9,646 383 858 1,176 16,600 303 4,040 0 0.06 23.3 11.6 7.6 ND CD1247 7,939 2,950 0.19 0.05 5.1 7.01 213 26,887 308 626 856 14,000 382 ND 20.4 4.6 CD1515 19,000 3,520 4.27 35,984 11,278 1,212 147 250 708 0 ND 0.18 1.34 14.7 7.9 2.8 RC1216 6.45 9 25,376 7,717 515 681 13,400 339 2,630 5.1 0.17 13 249 ND 4.1 1.6 RC1177 6.58 27,343 8,236 14,200 191 3,090 7.8 0.28 15.1 171 754 3.2 263 683 ND 5.9 CD1409 7,519 2,285 4,070 1,231 56 3.3 1.7 6.58 -167 66 174 262 ND 0.22 0.6 2.9 CD1366 2,271 1,140 0.34 0.32 4.9 2.2 4.6 6.46 80 8,461 84 461 290 4,210 ND ND

Samples from 2010 to 2014

Water samples were airlifted from 10 holes in the Ambassador deposit in March 2010 and analysed for major components and a range of other elements and metals (Table 6). Many other holes in the area were sampled in 2012 to 2014 (Appendix II). The results are similar to the 1984 analyses, with salinity ranging from 700 to 80,000 mg/L TDS; pH 3.0 to 8.0; and Fe <0.2 to 56 mg/L. Salinities within the Princess and Ambassador deposits generally range from 20,000 to 30,000 mg/L TDS. Most of the higher salinities, around 60,000 mg/L TDS, are for drillholes about 5 km west of Ambassador but are included with the Ambassador data here.

Minor elements and metals other than iron that were analysed for were generally at low concentrations or below the limits of detection, including uranium. There were some elevated metal concentrations in holes that had low pH. Bromine concentrations ranged from 3 to 23 mg/L; and strontium 2 to 12 mg/L.

Water samples taken from the Princess deposit have been measured in the field in 2012 and 2013 for salinity and pH. The water is acidic, with pH generally ranging from 5.0 to 6.5. Lower pHs of around 3 have been measured in one hole, NNA5623. Salinities are lower than most at Ambassador, ranging from 8,700 to 21,400 mg/L TDS, as the deposit is up-gradient of Ambassador.

3.5.2 Emperor and Shogun Deposits

Water samples have been collected and analysed from 161 drillholes in these deposits, mostly in 1984 and 2012.

Groundwater salinity at Emperor and Shogun ranged from 13,000 to 139,700 mg/L TDS (GRC, 1984) with the highest salinities in the south, and the lowest salinities towards the margins of the palaeochannel to the north or west (Fig. 10) suggesting possible recharge in these areas of less-saline water. The salinity increases with depth, and is generally more saline than at the Ambassador deposit.

The water from the bores at Emperor and Shogun is more acidic than at Ambassador, with pH of 3.8 to 5.0. It is of sodium chloride type with moderately high magnesium and sulphate concentrations.

The Piper trilinear diagram indicates that the portions of the major ions are similar to seawater (Fig. 12). Of the water samples collected from drillholes in 2012 to 2014 (Appendix II) many had low pH in the range 3 to 4 (minimum 2.9 and maximum 6.2), and salinity ranging from 6,100 to 95,500 mg/L TDS. Most salinities are greater than 50,000 mg/L TDS.

Table 6: Results of Major Component Analyses (and Other Elements and Metals) 2010

Hole/Bore	Units	NNA5027	NNA5198	NNA5393	NNA5127	NNA5140	NNA5086	NNA5103	NNA5199	NNA5155	NNA5107
Hole/Sample Depth		82	64	73	65	51	75	66	55	51	69
Date Analysed		26/03/2010	26/03/2010	26/03/2010	26/03/2010	26/03/2010	26/03/2010	26/03/2010	26/03/2010	26/03/2010	26/03/2010
рН	pH Units	4.1	3.5	4.2	5.5	6.4	6.8	4.3	4.2	6.7	4.8
Conductivity @25°C	μS/cm	17780	23060	31200	31400	27420	47800	41700	45000	28390	44700
TDS (Calculated)	mg/L	10668	13836	18720	18840	16452	28680	25020	27000	17034	26820
Soluble Iron, Fe	mg/L	0.844	50.813	6.526	0.203	<0.2	<0.2	0.76	5.885	<0.2	<0.2
Sodium, Na	mg/L	3038	4116	5748	5710	4898	8651	7602	8197	5087	8130
Potassium, K	mg/L	101	128	185	187	171	349	257	316	180	292
Calcium, Ca	mg/L	197	274	416	463	357	604	580	614	362	620
Magnesium, Mg	mg/L	301	336	548	531	422	900	772	833	488	834
Chloride, Cl	mg/L	5311	7558	11235	10922	8689	17219	13693	16462	9677	15717
Carbonate, CO₃	mg/L	<1	<1	<1	<1	<1	<1	<1	<1	<1	<1
Bicarbonate, HCO ₃	mg/L	<5	<5	<5	49	9	32	<5	<5	31	<5
Sulphate, SO₄	mg/L	1355	1633	2237	2227	1751	3317	2875	3273	1827	3553
Nitrate, NO₃	mg/L	0.35	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2	<0.2
Cation/Anion balance	%	-2.5	-5	-6.3	-5.2	-2.1	-6.3	-1.9	-6.9	-4.6	-5.8
Sum of lons (calc.)	mg/L	10303	14045	20368	20089	16297	31071	25778	29695	17652	29147
Soluble Arsenic, As	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Boron, B	mg/L	1.252	1.011	1.611	1.409	1.208	2.712	1.722	2.126	1.352	1.688
Soluble Barium, Ba	mg/L	0.038	0.052	0.035	0.055	0.07	0.051	0.066	0.094	0.053	0.067
Soluble Beryllium, Be	mg/L	<0.005	0.02	0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Cadmium, Cd	mg/L	<0.0005	0.001	0.003	0.024	0.0009	0.007	0.013	<0.001	<0.0005	0.319
Soluble Chromium, Cr	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	0.013	<0.01	<0.005	<0.01
Soluble Copper, Cu	mg/L	0.032	0.021	0.018	0.013	0.024	0.018	0.628	0.016	0.005	1.904
Soluble Cobalt, Co	mg/L	0.075	0.719	1.052	0.625	0.148	0.199	3.958	0.653	0.026	2.292
Soluble Lead, Pb	mg/L	0.015	0.041	<0.005	<0.005	0.006	<0.01	0.345	<0.01	<0.005	3.077
Soluble Molybdenum, Mo	mg/L	<0.005	<0.005	<0.005	0.012	0.035	<0.01	<0.01	<0.01	0.008	<0.01
Soluble Manganese, Mn	mg/L	3.208	1.367	1.021	1.246	0.532	1.964	1.608	1.299	0.562	2.345
Soluble Nickel, Ni	mg/L	0.055	1.153	1.888	0.627	0.181	0.377	3.83	1.719	0.023	2.905
Antimony, Sb	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Tin, Sn	mg/L	<0.005	<0.005	<0.005	<0.005	<0.005	<0.01	<0.01	<0.01	<0.005	<0.01
Soluble Selenium, Se	mg/L	<0.005	0.007	<0.005	0.009	<0.005	<0.01	0.104	<0.01	<0.005	<0.01
Soluble Zinc, Zn	mg/L	0.08	6.647	3.252	0.266	0.162	0.918	5.256	7.779	0.074	12.888
Soluble Uranium	mg/L	<0.005	<0.005	0.028	0.032	<0.005	<0.01	0.019	<0.01	< 0.005	0.068
Vanadium	mg/L	<0.005	<0.005	<0.005	<0.005	0.009	<0.01	<0.01	<0.01	< 0.005	<0.01
Soluble Mercury, Hg	mg/L	<0.0001	< 0.0001	<0.0001	<0.0001	<0.0001	<0.0001	< 0.0001	<0.0001	<0.0001	<0.0001

Iron concentrations range from <0.05 mg/L to 55 mg/L in recent samples (below the limit of reporting in 2014) and up to 190 mg/L in the 1984 samples. Prior to 2014, bromine (four analyses) ranged from 23 to 71 mg/L; and strontium 7.7 and 8.8 mg/L (two samples). In 2014 these elements were below the limit of reporting in all seven samples analysed. Other elements and metals that were analysed were at low levels or below levels of detection. Uranium was above the level of detection in five samples, with one high value (0.35 mg/L) from the Shogun costean in 1983. One sample from drillhole MSW002 had an anomalously high zinc concentration (26 mg/L) in May 2012, but was low (0.76 mg/L) in the October 2012 sample.

3.5.3 Reinjection Area

Water samples were analysed from 17 bores in the Reinjection Area in 2014 and 2015 – with two to four samples analysed from 12 of the bores. The results are included in Appendix II.

The water is moderately acidic, with pH ranging from 4.0 to 6.9, and is generally between 4.5 and 5.0. It is of a sodium chloride type, with relatively high magnesium and sulphate concentrations. Salinity ranges from 20,000 to 73,000 mg/L TDS and averages 51,500 mg/L TDS; generally significantly higher than for groundwater in the Ambassador/Princess area.

There is a good correlation between sample depth and salinity (Fig. 13). Seepage from in-pit tailings will infiltrate to shallow groundwater of similar salinity to that at the Ambassador deposit. The zone where any seepage would reach the water table includes reactive carbon-rich layers that will tend to fix any metals in the leachate.

Where analysed, metals and trace elements in groundwater in the injection area were at low levels or below the limits of reporting. There were some elevated boron concentrations of 4.2 to 7.2 mg/L in seven of the bores.

4 BORE CONSTRUCTION AND PUMPING TESTS

Many mineral exploration holes and holes drilled to delineate the deposits have been cased with 50 mm uPVC casing and are used for groundwater-level and water quality monitoring. In addition, a number of production bores have been drilled in the project area for potable and process water supply, dewatering testing, and for road construction. These are described below and production bore locations are shown in Figure 14.

4.1 DRILLING AND BORE CONSTRUCTION

GRC (1985) supervised the construction and testing of seven bores (MRWB1–7) in the project area for PNC in 1984; four of these were low-yielding, including MRWB5 which was used to determine the vertical permeability of sediments beneath the mineralised zone at Shogun. Details of that bore and the higher-yielding bores are given in Table 7.

Bore MRWB6 near the Emperor deposit has collapsed, and was replaced by two bores MSWB02 and 03 constructed to provide water for road construction (MWES, 2011) for the Tropicana Gold Project.

Bores NWB1 and NWB2 were constructed as test-injection bores, south of the Ambassador deposit in the palaeochannel sediments. Construction details and logs for these bores are given in Appendix III.

Table 7: Summary of Production Bore Details

Bore	mE (M0	mN GA)	RLGL mAHD	Date Drillled	TD (mbgl)	Casing	Screened Interval (m)	Aquifer Depth	SWL (mbtc)	TDS (mg/L)
MRWB4	557595	6691810		1984	71	130 mm uPVC	63-67.5	45.5-71	31.9	69,500
MRWB5	563440	6687600		1984	67	195 mm uPVC	44.2-46.2	44-62	30.2	59,100
MRWB6	557176	6690643	316	1984	74.5	195mm uPVC	58.5-70.5m	56-70.5	27.9	89,300
MRWB7	575480	6679975		1984	100	195 mm uPVC	68.5-92.5	65-97.5	34.0	36,800
MSWB02	557225	6690545	316	2011	72	155mm uPVC	54-72m	54-72m	28.3	90,000
MSWB03	556958	6690702	317	2011	78	155mm uPVC	54-76m	54-76m	29.1	91,000
NWB1	575552	6671190	328.2	2015	108	155 mm uPVC	36-42; 66-102	60-104	40.0	58,000
NWB2	575363	6670210	346.1	2015	114	155 mm uPVC	30-48; 84-102	74-114	57.9	65,000

4.2 PUMPING TESTS

The bores listed in Table 7 have all been test-pumped to determine pumping capacities and aquifer parameters. The PNC and Tropicana bore tests are described in GRC (1985) and MWES (2011), respectively, and the parameters derived from the test results are given in Table 8.

The tests on bores NWB1 and NWB2 are described below and the results are summarised in Table 8. The pumping test plots are included in Appendix III.

Bore	mE	mN	Rec. Yield	Т	КН	ΚV	SC
	(MGA)		(kL/d)	(m^2/d)	(m/d)	(m/d)	
MRWB4	557595	6691810	150	15	3.5		
MRWB5	563440	6687600	0	ND	ND	0.01-0.03	0.00025
MRWB6	557176	6690643	2100	450	37.5		
MRWB7	575480	6679975	3400	210	9		0.0002
MSWB02	557225	6690545	690	2330, 819	129, 45.5		ND
MSWB03	556958	6690702	690	1050	47.5		ND
NWB1	575552	6671190	1000*	4900, 5500	136-161		0.0004-0.0054
NWB2	575363	6670210	1000*	2500-5300	69-147		0.0002, 0.0009

Table 8: Results of Pumping and Recovery Tests

4.2.1 Bore NWB1

Bore NWB1, which intersects basal palaeochannel sands, was test-pumped by Harrington Drilling from 15th to 18th March 2015.

The initial test was a step-rate test with four one-hour steps at 430, 620, 790 and 920 kL/d. The purpose of the test was mainly to select a suitable rate for the constant-rate test, although that rate was limited by the capacity of the pump. The results were also analysed to determine bore efficiency: the efficiency decreased from 48 % in step 1 with a pumping rate of 430 kL/d to 30 % in step 4 with a pumping rate of 920 kL/d. A summary of the results is given in Appendix III.

The bore was then pumped at 1,210 kL/d for 48 hours. Water levels were monitored in the pumped bore; in bore NGW37 located 78 m to the south; and in NGW54C located 56 m north of NWB1. Drawdowns could not be monitored in NWB1 for the first 200 minutes of the test due to a bend in the access tube, and then fluctuated around 0.5 m to the end of the test. The drawdowns in the two monitoring bores followed straight-line trends on a semi-logarithmic scale for the first 800 minutes, typical of a laterally extensive aquifer. The drawdowns then stabilised, with minor fluctuations, indicating inter-aquifer leakage (Appendix III).

At the end of the test, water-level recovery was monitored in the three bores for a period of 80 minutes (NWB1) to 120 minutes (monitoring bores).

Drawdown and recovery plots for the bores are included in Appendix III. They were analysed using the Jacob method and Theis recovery method to determine aquifer transmissivity (T) and storativity (S). The transmissivity values were divided by the total screened interval in NWB1 (36 m) to determine average hydraulic conductivity (K) of the screened interval, which includes sand beds and any interbedded clayey layers. The results are given in Table 9.

^{*} Yield limited by casing diameter

Table 9: Results of Pumping and Recovery Tests, NWB1

Obs. Bore	Distance	Constant F	Rate Test	Recove	ry Test	K Av. (m/d)		
	(m)	T (m ² /d)	S	T (m ² /d)	S	CR Test	Recovery	
NWB1	0	ND	ND	5,400	ND	ND	150	
NGW37	75.5	5,500	0.0005	5,800	0.0054	153	161	
NGW54C	52	4,900	0.0004	8500??	0.013??	136	ND	

The results indicate that the aquifer is highly permeable, and more permeable near NWB1 and NGW37 than at NGW54C. The aquifer is confined with low values of storativity.

Measurements of salinity, temperature and pH were made on the pumped water at the start of the constant-rate test, and then every four hours. The results are given in Table 10.

Table 10: Physico-Chemical Measurements made during NWB1 Test

Time Since Test Start (Hours)	TDS (mg/L)	Temp (°C)	рН
0	65,400	23.7	3.90
3	68,600	23.5	3.79
7	69,200	24.2	3.98
11	69,200	23.3	3.97
15	69,100	21.8	3.99
19	70,700	20.5	3.99
23	68,600	22.3	4.01
27	68,800	23.8	4.02
31	67,600	24.0	3.98
35	67,800	23.2	3.97
39	68,700	22.6	4.02
43	69,200	21.7	4.07
47	68,400	21.7	4.07

The results show that both pH and salinity fluctuated during the test, but possibly increased overall. The results of the laboratory analyses show that salinity was slightly lower at the end of the test than at the start.

Water samples taken at the beginning and end of the test were analysed by SGS laboratories. Salinity decreased slightly from 66,000 mg/L TDS at the start to 65,000 mg/L TDS at the end. The water was of a sodium chloride type; with elevated magnesium, sulphate and boron concentrations. Metal concentrations were low or below the reporting limits. Laboratory pH values were 4.0 (start) and 4.1 (end) showing the water to be acidic.

4.2.2 Bore NBW2

Bore NWB2, which also intersects basal palaeochannel sands, was test-pumped by Harrington Drilling from 12th to 15th March 2015.

The initial test was a step-rate test with four one-hour steps at 340, 600, 770 and 940 kL/d. The purpose of the test was mainly to select a suitable rate for the constant-rate test, although again that rate was limited by the capacity of the pump. Groundwater levels rose during the first step indicating the bore was still being developed. The results were analysed to determine bore efficiency: the efficiency decreased from 51 % in step 1 with a pumping rate of 340 kL/d to 28 % in step 4 with a pumping rate of 940 kL/d. A summary of the results is given in Appendix III.

The bore was then pumped at 950 kL/d for 48 hours. Water levels were monitored in the pumped bore; in bore NGW30 located 52 m to the south; and in NGW55 located 23 m north of NWB2. The water-level in the production bore drew down relatively rapidly in the first five minutes, and then declined very gradually to only about 0.3 m at the end of the test. Drawdowns in the two monitoring bores were relatively steep for the first 50 minutes, and then were very flat before steepening slightly towards the end of the test (Appendix III). These results show that the aquifer is highly permeable, and that the rate of drawdown was reduced by inter-aquifer leakage.

At the end of the test, water-level recovery was monitored in the three bores over a period of 60 minutes.

Drawdown-time and recovery plots for the bores are included in Appendix III. They were analysed using the Jacob method and Theis recovery method to determine aquifer transmissivity (T) and storativity (S). The transmissivity values were divided by the total screened interval in NWB2 (36 m) to determine average hydraulic conductivity (K) of the screened interval. The results are given in Table 11.

Table 11: Results of Pumping and Recovery Tests, NWB2

Obs Bore	Distance	Constant Rate Test		Recovery Test		K Av. (m/d)	
	(m)	T (m ² /d)	S	T (m²/d)	S	CR Test	Recovery
NWB2	0	2,500	ND	3,500	ND	69	97
NGW30	49.5	5,300	0.0002	ND	ND	147	ND
NGW55	32	4,500	0.0009	3,800	ND	125	106

The results indicate that the aquifer is highly permeable, particularly near NGW30 and to a lesser degree, NGW55. The aquifer is confined with low values of storativity.

Measurements of salinity, temperature and pH were made on the pumped water at the start of the constant-rate test, and then every four hours. The results are given in Table 12.

Table 12: Physico-Chemical Measurements made during NWB1 Test

Time Since Test Start (Hrs)	TDS (mg/L)	Temp (°C)	рН
0.5	61,700	22.6	3.82
4	60,200	25.2	3.97
8	60,200	25.4	3.93
12	62,000	23.3	4.02
16	62,100	22.7	4.07
20	61,100	21.0	4.11
24	62,000	22.8	4.06
28	58,600	26.1	4.03
32	59,700	25.7	3.98
36	60,100	24.4	4.07
40	61,600	23.9	4.13
44	61,500	23.1	4.08
48	61,300	23.4	4.08

The results show that both pH and salinity fluctuated during the test, and pH possibly increased overall. The results of the laboratory analyses show that salinity was slightly lower at the end of the test than at the start.

Water samples taken at the beginning and end of the test were analysed by SGS laboratories. Salinity decreased slightly from 59,000 mg/L TDS at the start to 58,000 mg/L TDS at the end. The water was of a sodium chloride type; with elevated magnesium, sulphate and boron concentrations. Metal concentrations were low or below the reporting limits. Laboratory pH values were 4.5 (start) and 4.4 (end) showing the water to be acidic.

4.3 SLUG TESTS AND LOW-FLOW PUMPING TESTS

Fifty-five slug (falling-head) permeability tests, and five low-flow recovery tests following pumping for sampling, were conducted by Vimy on monitoring bores in the Ambassador/Princess area.

The slug tests consisted of introducing a slug of water, generally 20 litres, and monitoring the rate of water level decline using pressure transducers and data loggers. The data were analysed using the method of Bouwer and Rice (1976).

The low-flow recovery tests consisted of monitoring water-level recovery following pumping. The results were analysed using the method of Theis (1935).

The results of the tests are given in Table 13. Where there was no measurable water-level recovery during the tests, the permeability (hydraulic conductivity, K) is recorded as being very low. Where the water-level recovery was too rapid to be measured during the slug tests, the permeability was recorded as being high (> 5 m/d).

5 NUMERICAL GROUNDWATER MODELLING

A numerical groundwater model was constructed of the planned mining and re-injection areas, and run to estimate the dewatering requirements and the impacts of pumping, re-injection and tailings seepage. It is based on the conceptual hydrogeological model, described below.

5.1 CONCEPTUAL HYDROGEOLOGICAL MODEL

The Mulga Rock deposits lie within an oxbow basin/palaeochannel that remains after the capture of three trunk palaeochannels by the Ponton Creek palaeochannel.

The Mulga Rock palaeochannel is probably still hydraulically connected to the Ponton Creek palaeochannel some 65 km to the south along the eastern arm.

The water table is about 50 m deep, and is overlain by mainly fine-grained sediments, except along the eastern arm south of Ambassador where there is a substantial thickness of unsaturated sand (e.g. Figs. 8 and 9). The mineralised zones are mainly just below the water table and in fine-grained carbonaceous sediments. Sand and gravel beds of Eocene age become more common towards the base of the palaeochannel. These basal sands and gravel have moderate to high permeability and form the main zone of groundwater flow.

The water table is very flat-lying in the "Narnoo Basin" which contains the Mulga Rock deposits, showing there is little groundwater flow into, and out of the basin. Hydraulic gradients indicate there is probably minor groundwater flow into the basin from the northwest and north, and from the north-east along a tributary channel which contains the Ambassador deposit. The flow in Eocene sands along the tributary channel is greatly restricted by a basement high between the western and eastern parts of the Ambassador deposit.

Table 13: Results of Slug and Low-Flow Pumping (Recovery) Tests

Bore	mE	mN	Test Type	Open depth	SWL	K	Model Layer
ļ, ,				(m)	(m bgl)	(m/d)	
NND5029	575965	6681554	Low-flow rec	52.5	36.91	0.2	1,2
NND5030	575544		Low-flow rec	54.1	35.37	> 0.3	1,2
NND5031	579499		Low-flow rec	54.7	33.66	0.007	1,2
NNA5198	575539		Low-flow rec	51.7	35.92	0.003	1,2
NNA5227	576237	6680967	Low-flow rec	41.4	27.84	V. Low	1,2
NNA5177	576185	6682159	Slug Test	43.7	39.61	V Low	1
NNA5178	576216	6682140		41.6	39.11	0.01	1
NNA5198	575539	6682048	Slug Test	55.7	35.38	0.02	1,2
NNA5200	578614	6682405	Slug Test	39.6	37.10	V Low	1
NNA5201	578623	6682398	-	42.5	37.67	V Low	1
NNA5209	577232	6682510	Slug Test	40.8	40.85	0.00	1
NNA5210	577308	6682464	Slug Test	41.9	41,19	High	1
NNA5211	577374	6682425	Slug Test	41.0	40.60	?	1
NNA5213	577174	6682539	Slug Test	43.0	41.85	0.02	1
NNA5214	577099	6682591	Slug Test	43.1	43.11	High	1
NNA5215	577027	6682625	Slug Test	58.3	43.35	V Low	1,2
NNA5219	577144	6682792	Slug Test	41.5	33.47	V Low	1
NNA5220	577210	6682754	Slug Test	41.5	35.78	V Low	1
NNA5221	576271	6681162	Slug Test	42.3	33.87	V Low	1
NNA5222	576337	6681123	Slug Test	38.7	37.67	V Low	1
NNA5226	576155	6681009	Slug Test	43.1	35.58	V Low	1
NNA5227	576236	6680967	Slug Test	41.4	38.64	V Low	1
NNA5228	576293	6680926	Slug Test	45.9	38.94	V Low	1
NNA5229	576367	6680885	Slug Test	45.0	36.92	V Low	1
NNA5230	576434	6680844	Slug Test	38.1	36.75	0.07	1
NNA5231	576556	6680766	Slug Test	38.9	31.11	V Low	1
NNA5232	576493	6680799	Slug Test	26.8	19.35	V Low	1
NNA5234	576019	6680570		42.8	36.78	0.05	1
NNA5235	575004	6679932	Slug Test	52.9	39.34	0.11	1,2
NNA5236	574933	6679974	Slug Test	46.2	38.37	0.18	1
NNA5238	574792	6680063	Slug Test	40.5	40.49	High	1
NNA5239	574714	6680104	Slug Test	55.3	41.39	V Low	1,2
NNA5240	574645	6680151	Slug Test	50.3	40.29	0.25	1
NNA5289	579988	6682770	Slug Test	31.0	30.88	0.04	1
NNA5301	580153	6682866	Slug Test	29.9	22.61	V Low	1
NNA5321	579933	6682698	Slug Test	40.9	32.06	V Low	1
NNA5465	575179	6680575	Slug Test	40.3	32.70	0.27	1
NNA5589	580088	6684614	Slug Test	40.8	42.59	0.38?	1
NNA5614	578964	6683963	Slug Test	48.0	41.38	0.11	1
NNA5623	578774	6684324	Slug Test	46.0	42.46	0.15	1
NNA5628	579432	6683938	Slug Test	47.5	37.62	0.07	1
NNA5630	579451	6684166		44.5	44.50	V Low	1
NNA5634	579135	6684302	Slug Test	45.4	43.75	0.16	1
NNA5639		6684370	_	53.2	48,48	0.08	1
NNA5641	579005	6683723		60.8	44.64	0.13	1,2
NNA5644	578770	6683872	Slug Test	50.1	44.87	0.17	1
NNA5647	578838	6683579	Slug Test	42.0	39.19	V Low	1 1 2
NNA5740	579643	6684560		53.5	41.99	0.32	1,2
NNA5749	579238	6683679		40.6	36.23	0.19	1
NNA5753		6684007	Slug Test	52.5	43.25	0.12	1
NND5028		6681735		47.6	37.30	0.61	1 1 2
NND5029	575965	6681554	Slug Test	52.3	36.81	1.28	1,2
NND5030	575544	6681137	Slug Test	55.6	35.30	1.91	1,2
N N D 5032	578632	6682382	_	51.5	38.50	1.10	1,2
NND5033	579138	6682819	Slug Test	49.1	40.83	2.72	1
NND5034		6681300	Slug Test	46.0	39.85	2.15	1
NND5035	- 0.00	6682472		46.4	37.30	1.71	1
NND5036	576591	6682391	Slug Test	50.7	39.24	1.16	1
NND5037			Slug Test	44.6	35.90	0.97	1 1 2
NND5038		6682522		51.4	39.26	2.30	1,2
NND5039	579796	6682656	_	51.2	34.04	1.05	1,2
NND5040	580034	6682734	Slug Test	43.6	32.93	0.32	1
NND5041		6682899		37.8	32.67	0.32	1
NND5077	576148	6682189	Slug Test	49.8	39.67	V Low	1
NND5078	577076	6682606	Slug Test	53.2	48.60	1.52	1

Groundwater possibly flows from the basin to the south along the western arm of the palaeochannel; and probably also south along the eastern arm, although the flow rate is low and is restricted by the mainly fine-grained sediments in at least part of the palaeochannel (Section Line 92,500 N, Uranerz 1986), about 25 km south of Ambassador.

Groundwater in the palaeochannel is saline to hypersaline and generally acidic, and contains low metal concentrations.

5.2 DESCRIPTION OF NUMERICAL MODEL

A numerical groundwater model has been constructed of the Mulga Rock palaeochannel. It consists of a rectangular grid of 142 rows, 104 columns and three layers covering an area of 45 km east—west by 65 km north—south (Fig. 15). Cell sizes are 500 m by 500 m in general, and 250 m by 250 m in the Ambassador area.

Layer 1 represents fine-grained sediments near the water table; Layer 2 consists of interbedded sands and clays and admixtures; and Layer 3 the basal sand/gravel. The base of Layer 3 i.e. the base of the palaeochannel (Eocene sediments) and the top of the Eocene sediments were defined from data provided by Vimy for the numerous holes drilled for the Mulga Rock Uranium Project; and from the Uranerz geological sections.

The model was utilises Processing Modflow Pro version 8.0.2 (Simcore Software, 2010), which includes Modflow, finite difference groundwater modelling software designed by the U.S. Geological Survey (McDonald and Harbaugh, 1988).

5.3 MODEL PARAMETERS

The model was initially set up with parameters determined from the pumping and slug tests; and assumed values based on grain sizes and our experience in modelling similar hydrogeological environments. The parameters, particularly horizontal hydraulic conductivity of the main aquifer, Layer 3, were varied in the calibration of the model. Parameters adopted on calibration of the model are given in Table 14.

Table 14: Adopted Aquifer Parameters

Parameter	Units	Layer 1	Layer 2	Layer 3
Horiz. Hydraulic Cond.	m/d	0.02-0.7	0.2-9	0.2-140
Vert. Hydraulic Cond.	m/d	0.01	0.1	0.5
Specific Yield	v/v	0.05	0.1	0.1
Storage Coefficient	v/v	NA	0.0004	0.0004
Recharge	m/d	0, 0.00001		

Horizontal hydraulic conductivity values were predominantly 0.1 m/d in Layer 1, 1 m/d in Layer 2, and 9 m/d in Layer 3. Values in Layer 1 in the Ambassador area were altered to utilise the results of the low-flow pumping tests and slug tests described in Section 4.3 above. In Layer 2, a variety of values were used in the Ambassador area depending on sand content in the zones to be mined, and the results of slug tests from deeper drillholes; and a low value of 0.2 m/d was adopted for the basement high between the two parts of the deposit. In Layer 3, there were higher values (70–140 m/d) in the planned injection area; and some lower values in the southern part of the eastern arm, and in the north-eastern tributary channel, particularly at the basement high at Ambassador as for Layer 2.

Recharge was assumed to be zero for much of the modelled area, except for a very low rate of 0.000001 m/d on the north-western edge of the basin and in part of the north-eastern tributary.

5.4 MODEL CALIBRATION

The model was first calibrated in steady-state mode to groundwater levels measured at various times in representative bores/holes over the Mulga Rock area. This was achieved by varying horizontal hydraulic conductivity of the main, basal sand aquifer (Layer 3), and to a much lesser degree, recharge in small areas in the north-west and north-east. The parameters adopted for the minor aquifers/aquitards and aquicludes of Layers 1 and 2 have negligible impact on the calibration; and storativity (specific yield and storage coefficient) is not part of a steady-state simulation.

A comparison between measured and model-calculated water levels is shown in Figure 16. There is a close correspondence and the root mean square error for all the calibration bores is 2.22 %, much lower than the 5 % limit recommended in the 2000 groundwater modelling guidelines (Middlemis, 2000), and 5 % or 10 % (if achievable) given in the more-recent guidelines (Barnett et. al., 2012).

The model was then calibrated in transient mode by simulating the bore NWB1 and 2 pumping tests. For the early data, (the first 10 to 60 minutes) a good match was achieved between calculated and observed drawdowns in the monitoring bores during the tests (Figs. 17 to 20) with a confined storage coefficient of 0.0008, at the upper end of the range of values indicated from the pumping test results. Although all the calculated drawdowns are within 0.16 m of the measured values, there is a divergence in the later stages of the test as the calculated values cannot replicate the reduced drawdowns resulting from inter-aquifer leakage, and they are also increased by the impact of boundaries to the aquifer. With long-term pumpage the effects of leakage are expected to disappear and the palaeochannel boundaries will increase the rate of drawdown.

5.5 MODEL SIMULATION AND RESULTS

The mine water balance dated 18 May 2015 has the following key components:

- Pit Dewatering flows to the processing plant are 96.8 kL/hr (2,323 kL/d);
- Water pumped from (low-salinity) borefield is 151.7 kL/hr (3,641 kL/d)
- Extraction from Tropicana mine's bore located in the Emperor pit (MSWB02) was included at a rate of 50 kL/d (the average for the period (July 2011 to November 2014); and
- Tailings seepage is 28.6 kL/hr (686 kL/d).

Any excess water from dewatering, plus 2.2 kL/hr reject water from the desalination plant, will be reinjected at the borefield south of Ambassador.

The mine plan for the Ambassador and Princess deposits is as shown in Fig. 21 and mine plans for the Emperor and Shogun deposits are shown in Fig. 22, and each area was subdivided into assumed annual pit areas. Modflow's Drain package was used to simulate dewatering with annual stress periods, with drain elevations set at the elevations of the planned base of mining which is presented in Fig. 23 for the Ambassador and Princess deposits and in Fig. 24 for the Emperor and Shogun deposits. Drain conductances are based on horizontal hydraulic conductivity values at the drain positions and model cell sizes.

Modflow's Well package was used to simulate: (1) tailings seepage from previously mined pits; (2) reinjection in years where average dewatering flows exceeded 2,323 kL/d and (3) extraction from the Tropicana bore.

Model-calculated average flows for each year are given in Table 15.

The results indicate that the maximum dewatering flows will be in Year 10 when an area is mined down to 255 m AHD on the western side of Ambassador West. There are also relatively high flows in Year 3 when a low area is mined on the northern side of Ambassador East. In those years, surplus water will be injected. In the other years all dewatering water will be used for processing ore or dust suppression.

Table 15: Calculated Dewatering Flows and Injection Rates

Year	Annual Dewatering Vol.	Av. Flow	Av. Injected	Dewatering
	(kL)	(kL/d)	(kL/d)	Location
1	105,846	290	0	
2	411,761	1,128	0	
3	1,419,378	3,889	1,566	lor
4	89,190	244	0	ssac
5	800,239	2,192	0	Princess & Ambassador
6	486,206	1,332	0	Am
7	91,326	250	0	SS &
8	115,725	317	0	nce
9	58,490	160	0	Prii
10	1,497,545	4,103	1,780	
11	73,520	201	0	
12	103,414	283	0	or
13	486,181	1,332	0	Emperor
14	607,460	1,664	0	Επ
15	633,905	1,737	0	Emperor &
16	395,128	1,083	0	Shogun

Model-calculated groundwater level drawdowns at the end of Year 10 are shown in Figs 25 and 26 for model Layers 1 (surficial) and 3 (basal Eocene sand), respectively. They indicate drawdowns around the area of active mining will extend about 3.6 km to the south, with a low mound in the area of tailings seepage. The rise in water levels around the reinjection borefield is less than 1 m. At the end of Year 16, drawdowns are around the western mining area (the Emperor and Shogun deposits), with drawdowns extending about 3.9 km to the south of the Emperor pit and negligible drawdown at the Shogun deposit due to the relatively shallow depth of mining (Figs. 27 and 28). Maximum model-calculated drawdowns at each mining location and at the injection borefield are also presented in Figure 29 and show that the effects of dewatering will be localised during mining.

The model was then run to simulate the movement of conservative particles in the groundwater from a point at the southern end of the mining area (representing tailings seepage), and from the southern injection bore NWB2. The movement from both points would be very slow due to the low hydraulic gradients, with the groundwater only moving 2.8 km and 2.2 km, respectively, in 1,000 years (Fig. 30). In an expected worst case with double the horizontal hydraulic conductivities, and with 1,816 kL/d injected via NWB2 in the second-to-last year of mining, the distances travelled in 1,000 years would be 9 km and 4 km, respectively (Fig. 30).

5.6 SENSITIVITY ANALYSIS

The modelling described in Section 5.5 above was repeated to determine the impact on dewatering flow rates of the various model parameters. The value of each parameter was doubled and then halved in turn, which is about the expected maximum variation that is likely to occur.

The results are given in Table 16. They show that the model is most sensitive to horizontal hydraulic conductivity (KH) followed by specific yield (SY) and vertical hydraulic conductivity (KV). It is insensitive to the confined storage coefficient, recharge and drain conductance.

Table 16: Results of Sensitivity Analysis

Cana	Total Volume	Difference		
Case	Pumped (kL)	(kL)	%	
Adopted	7,375,314	0	0	
KH*2	9,914,636	2,539,323	34.4%	
KH/2	5,588,461	-1,786,853	-24.2%	
KV*2	8,369,283	993,970	13.5%	
KV/2	6,381,852	-993,462	-13.5%	
SY*2	9,594,769	2,219,456	30.1%	
SY/2	6,066,511	-1,308,803	-17.7%	
SC*2	7,442,535	67,222	0.9%	
SC/2	7,366,360	-8,954	-0.1%	
Rech.*2	7,403,267	27,953	0.4%	
Rech./2	7,386,573	11,260	0.2%	
Drain Cond.*2	7,339,324	-35,990	-0.5%	
Drain Cond./2	7,353,616	-21,698	-0.3%	

In a likely worst case with double the adopted horizontal hydraulic conductivities, dewatering flows could be 34% higher overall than the calculated flows, and up to 50 % higher in the high-flow years when mining intersects the deep Eocene sands.

5.7 DISCUSSION OF MODELLING RESULTS

Although the model is well calibrated to steady-state conditions, aquifers in the area have not been stressed except by short-term pumping tests, and so there are few data available for transient calibration. The modelling results should, therefore, be taken as best estimates – actual dewatering pumping rates could be significantly different to those predicted.

Groundwater levels and pumping rates should be closely monitored once mining and dewatering commences, and the data used after six to twelve months of pumping to recalibrate the model and to update the predictions.

6 POTENTIAL ENVIRONMENTAL RECEPTORS

6.1 QUEEN VICTORIA SPRING

The Queen Victoria Spring Nature Reserve lies down-gradient of the MRUP: the northern boundary of the reserve is 14 km south of the planned injection borefield and 24 km south of the Ambassador deposit.

The Queen Victoria Spring was first encountered by a European by Giles in September 1875 (Giles, 1889). At that time, it was "150 yards in circumference and two to three feet deep and was surrounded by numerous native wells". He believed it to be a permanent body of water that was supplied by drainage of the sand hills that surround it, and that rests on a substratum of impervious clay.

The presence of numerous wells is a good indication that the spring was not a permanent feature. In April 1896, Carnegie (1898) visited the spring and found that it and all the native wells were dry. He managed to obtain sufficient water by digging a shallow well in the base of the spring.

The spring was said by Giles to be surrounded by clumps of "funereal pines", presumably sheoaks that would have been sustained by this shallow, perched groundwater.

The spring can be seen as a small oval-shaped depression on Google Earth at 555170 mE, 6633710 mN at an elevation of about 323 m AHD, and looks to have been dry when the image was taken on 4 October 2013.

The spring is interpreted to be a local, ephemeral, perched water source, located 14 km from the nearest water injection site for the MRUP. It is not, therefore, an environmental receptor that could be impacted by the planned mining at Mulga Rock.

6.2 PALAEOCHANNEL AQUIFER

The palaeochannel aquifer and overlying sediments contain saline to hypersaline groundwater. The water table is too deep, and the groundwater too saline to support vegetation; and it is very unlikely that there will be any other users of the groundwater within the area that could be impacted during mining and within 1,000 years thereafter.

Groundwater at the planned injection borefield has salinity of about 60,000 mg/L TDS, compared with about 20,000 to 30,000 mg/L TDS at the Ambassador and Princess deposits. Provided the pH is similar, any excess water that is reinjected should be of better quality than the receiving water.

Groundwater in the planned mining areas has the potential to become more acidic – this should be addressed in environmental investigations; as well as any treatment required for tailings, and for water to be reinjected.

7 CONCLUSIONS

Most of the sediments to be mined are fine-grained and of low permeability, and so dewatering flow rates will be low. Some high dewatering flows will be required when deep mineralised zones associated with Eocene sands are mined. Much or all of the dewatering water will be used in the processing plant. This will be supplemented by low-salinity water from the Kakarook North borefield and water recycled from the in-pit beneficiation plant.

Any water reinjected into the palaeochannel aquifer is expected to be of lower salinity than the receiving water, and should be of better quality provided the pH is controlled if necessary.

Seepage from in-pit tailings will infiltrate to groundwater of similar salinity to that at the Ambassador deposit. The zone where seepage would reach the water table includes reactive carbon-rich layers that will tend to fix any metals in the leachate.

The results of numerical groundwater flow and flow-path modelling indicate that the impacts of dewatering, tailings seepage and any reinjection will be localised during mining, and should not extend further than three to four kilometres south of the mining area or the reinjection borefield within 1,000 years of the end of mining. Even in a worst case, any water introduced to the palaeochannel aquifer is indicated to not extend further than 4 km south of the injection borefield over that period due to very low hydraulic gradients.

Dated: 29 October 2015 Rockwater Pty Ltd

M J Taylor Senior Hydrogeologist

M. Taylor

P H Wharton Principal

What -

REFERENCES

- Barnett *et al.*, 2012, Australian groundwater modelling guidelines. Waterlines report series No.82, National Water Commission, Canberra.
- Bouwer, H., and Rice, R.C., 1976, A slug test for determining hydraulic conductivity of unconfined aquifers with completely or partially penetrating wells. Water Resource Res. 12:423-248.
- Carnegie, D., 1898, Spinifex and Sand. Reprinted by Project Gutenberg Australia.
- De Broekert, P. and Sandiford, M., 2005, Buried Inset-Valleys in the Eastern Yilgarn Craton, Western Australia: geomorphology, age, and allogenic control. Journal of Geology Vol. 113 p. 471-493. University of Chicago.
- Douglas, G.B., Gray, D.J., and Butt, C.R.M., 1993, Geochemistry, mineralogy and hydrogeochemistry of the Ambassador multi-element lignite deposit, Western Australia. Unpub. report to PNC Exploration (Australia) Pty Ltd.
- English, *et al.*, 2012. Water for Australia's arid zone identifying and assessing Australia's palaeovalley groundwater resources: summary report, Waterlines report, National Water Commission, Canberra.
- Giles, E., 1889, Australia Twice Traversed. Reprinted by Dodo Press.
- GRC, 1984, Lake Minigwal Uranium Prospect, groundwater study for PNC Exploration (Australia) Pty Ltd.
- GRC, 1985, Mulga Rock Prospect, Stage 2 hydrogeological investigation for PNC Exploration (Australia) Pty Ltd.
- GRC, 1986, Report on groundwater exploration at Mulga Rock Prospect, 1985, for PNC Exploration (Australia) Pty Ltd.
- Luke, G.J., Burke, K.L., and O'Brien, T.M., 1988, Evaporation data for Western Australia. Tech. Report No. 65 (2nd Ed), W.A. Dept. of Agriculture.
- Magee, J.W., 2009. Palaeovalley groundwater resources in arid and semi-arid Australia, a literature review. Geoscience Australia Record 2009/03. 224 pp.

- McDonald, M.G., and A.W. Harbaugh, 1988, A Modular Three Dimensional Finite Difference Ground Water Flow Model. Book 6, Chapter A1, Techniques of Water Resources Investigations. U.S. Geol. Surv., Washington, DC. (A:3980).
- Middlemis, H., 2000, Groundwater Flow Modelling Guideline. Report to Murray-Darling Basin Commission.
- MWES, 2011, Tropicana Gold Project, Minigwal south borefield, H2 level hydrogeological assessment. Report to Tropicana J.V.
- Rockwater 2010, Ambassador deposit scoping study, assessment of dewatering requirements and water supply sources. Report for Energy and Minerals Australia Ltd.
- Rockwater 2013, Mulga Rock project, hydrogeology, and assessment of dewatering requirements and water supply sources. Report for Energy and Minerals Australia Ltd.
- Simcore Software, 2010, Processing Modflow, An integrated modelling environment for the simulation of groundwater flow, transport and reactive processes.
- Theis, C.V., 1935, The relation between the lowering of the piezometric surface and the rate and duration of discharge of a well using groundwater storage. Am. Geophys. Union Trans., Vol 16 p. 519 524.
- Uranerz Australia, 1986, East Yilgarn project, Report No. 320-11.
- Van de Graaff, W. J. E., Crowe, R. W. A., Bunting, J. A., and Jackson, M. L., 1977, Relict early Cainozoic drainages in arid Western Australia: Zeitschrift für Geomorphologie N. F., v. 21, pt 4, p. 379-400.

FIGURES

FIGURE 1 Tropicana Gold Mine ▲ 🛮 🗗 🎝 🕽 🖯 🖟 🖺 🖯 GREAT VICTORIA DESERT SHIRE OF LAVERTON CITY OF KALGOORLIE-BOULDER SHIRE OF MENZIES SHIRE OF LEONORA

figure 1.srf

CLIENT: Vimy Resources

PROJECT: Mulga Rock

DATE: June 2015

Dwg No: 345.0/15/1-1

LOCATION OF THE MULGA ROCK

URANIUM PROJECT



FIGURE 2

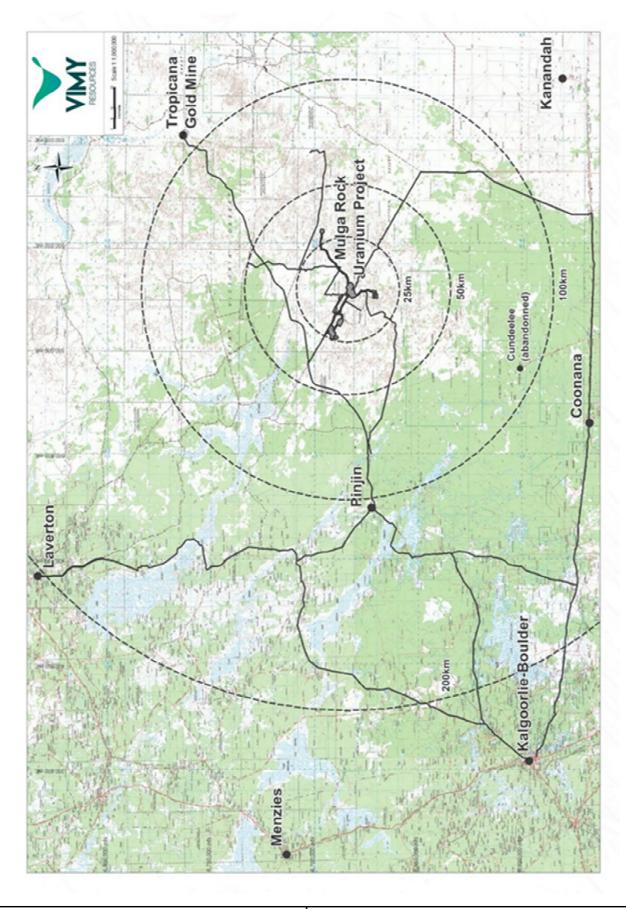


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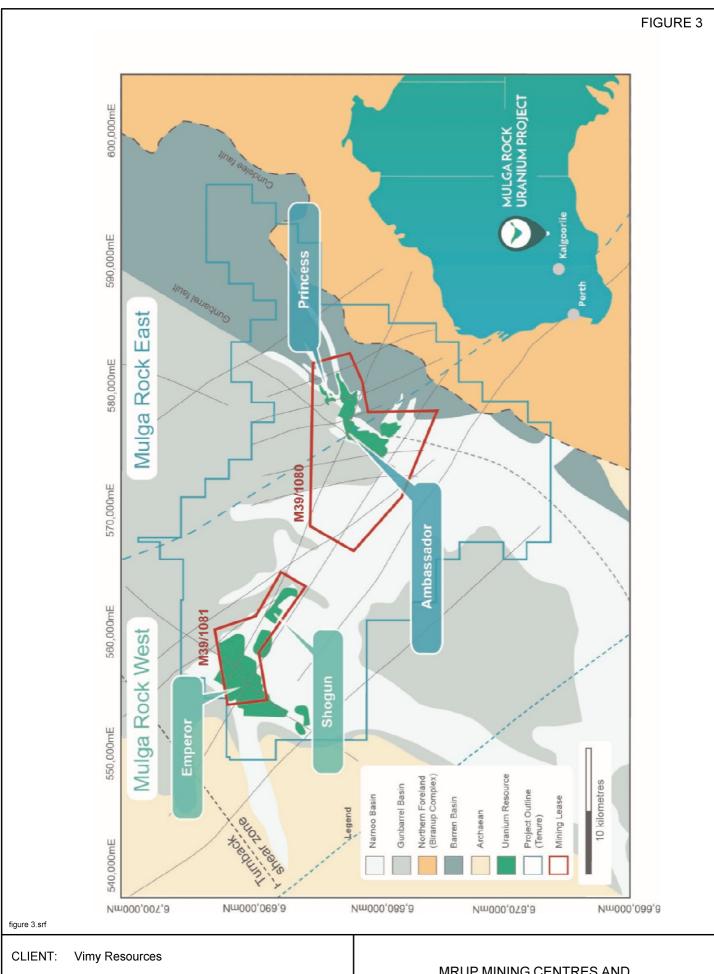
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MRUP AND NEARBY COMMUNITIES

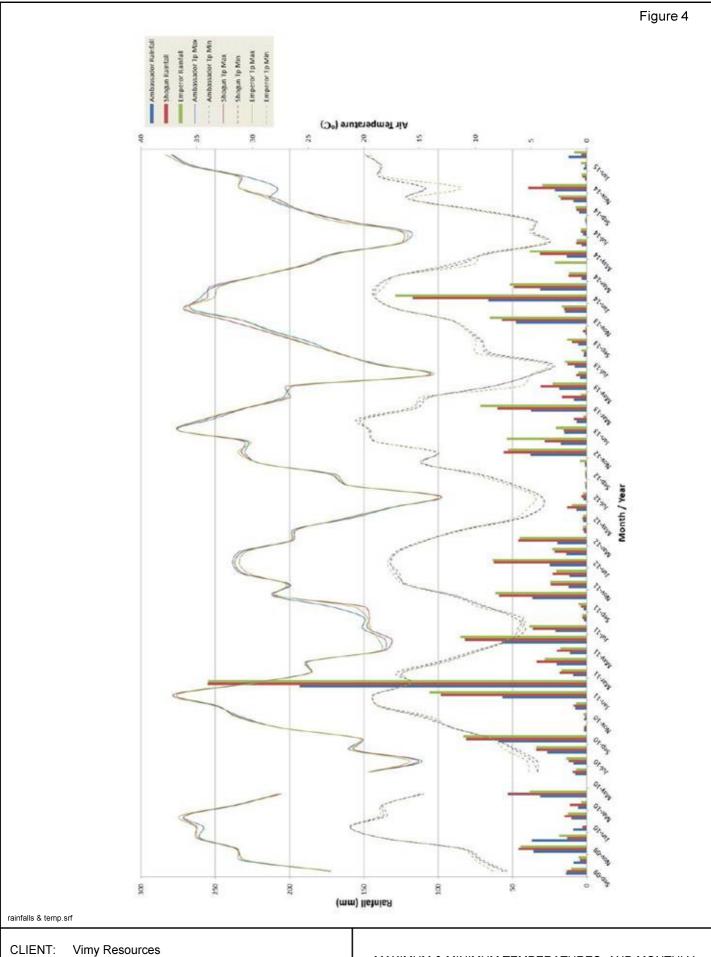




PROJECT: Mulga Rock
DATE: June 2015
Dwg No: 345.0/15/1-3

MRUP MINING CENTRES AND ASSOCIATED RESOURCES



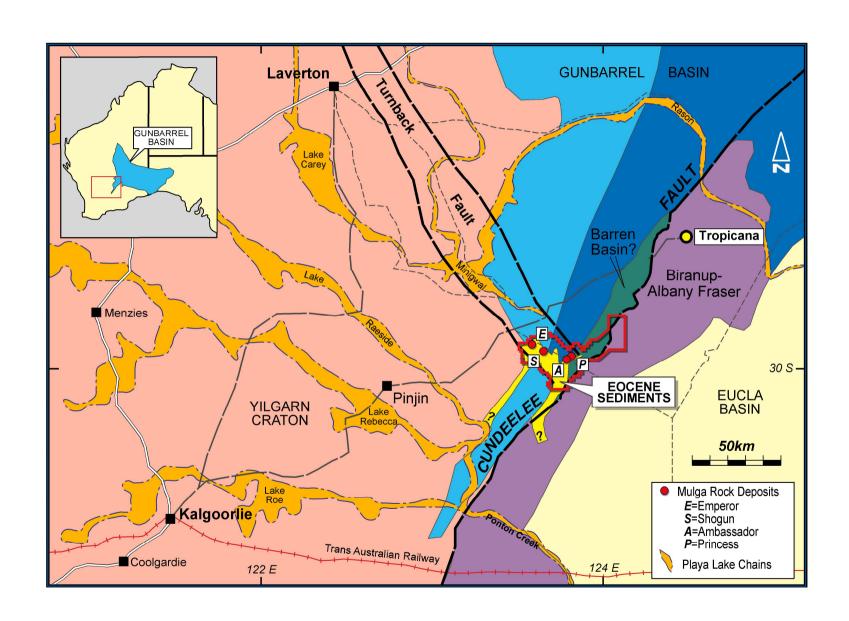


PROJECT: Mulga Rock Hydrogeology

DATE: May 2015 345.0/15/2-4 Dwg No:

MAXIMUM & MINIMUM TEMPERATURES, AND MONTHLY RAINFALLS, MULGA ROCK WEATHER STATIONS





geological setting.srf

CLIENT: Vimy Resources

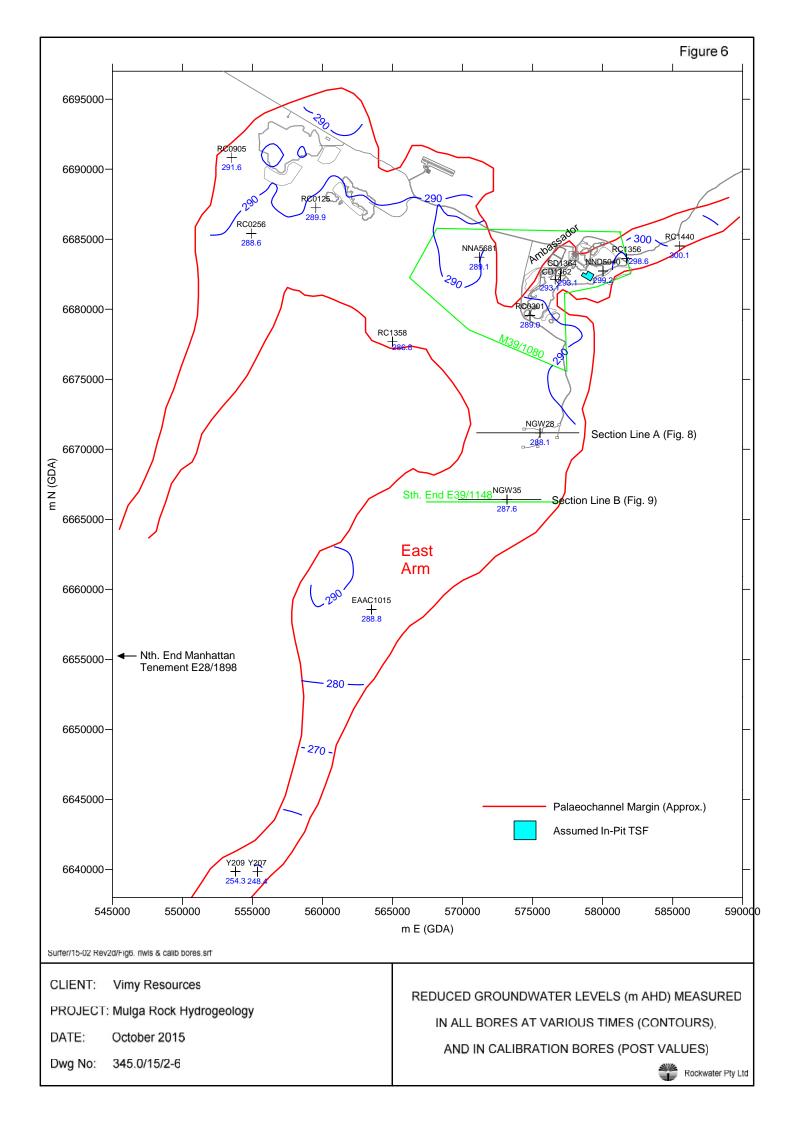
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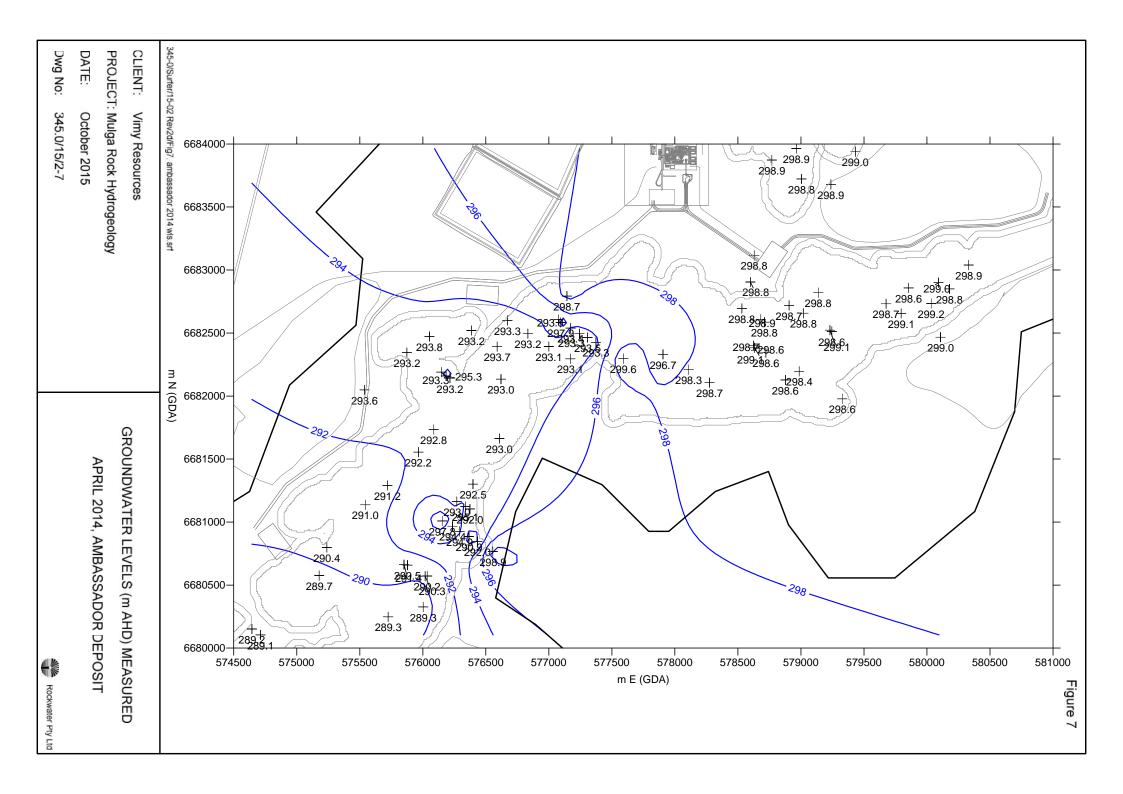
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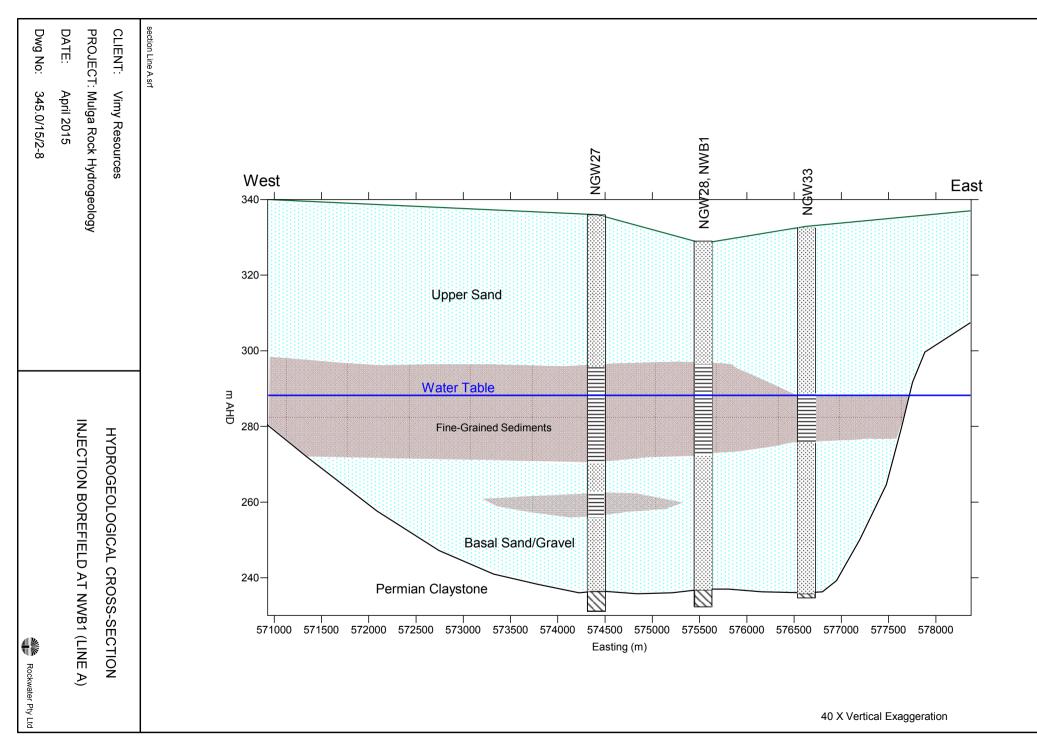
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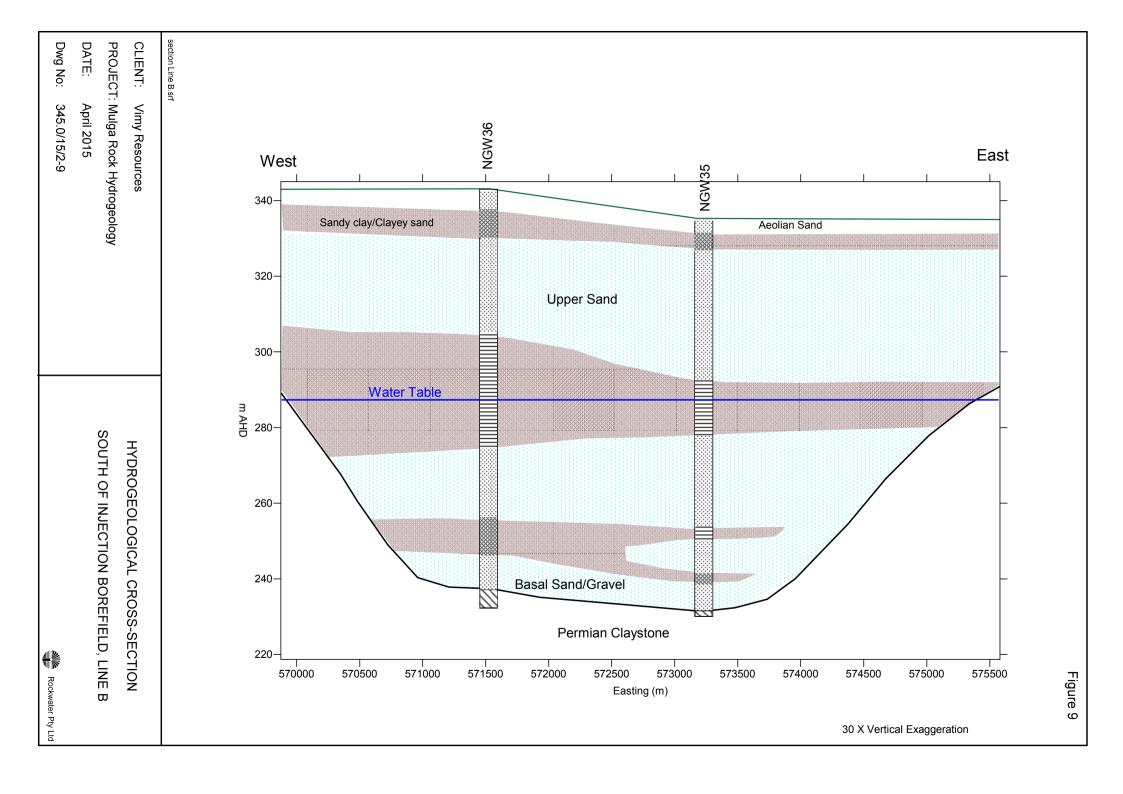
REGIONAL GEOLOGICAL SETTING

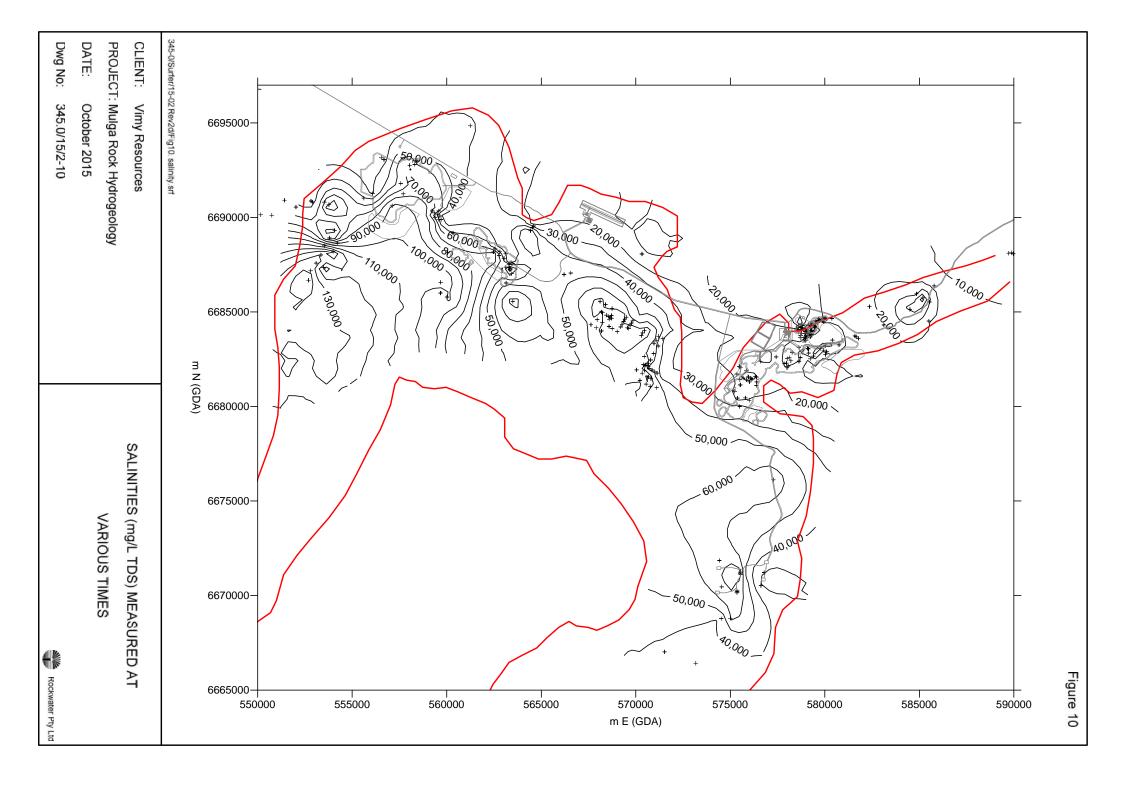


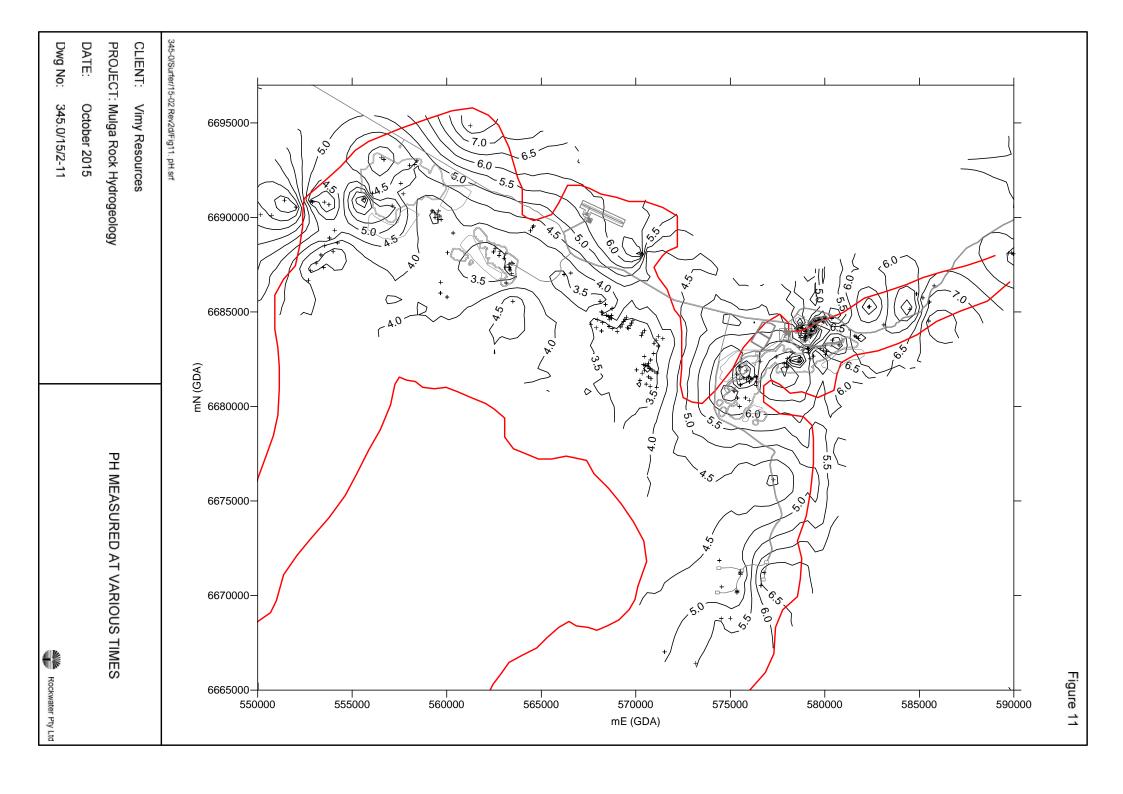














CLIENT: Vimy Resources Ltd

PROJECT: Mulga Rock Hydrogeology

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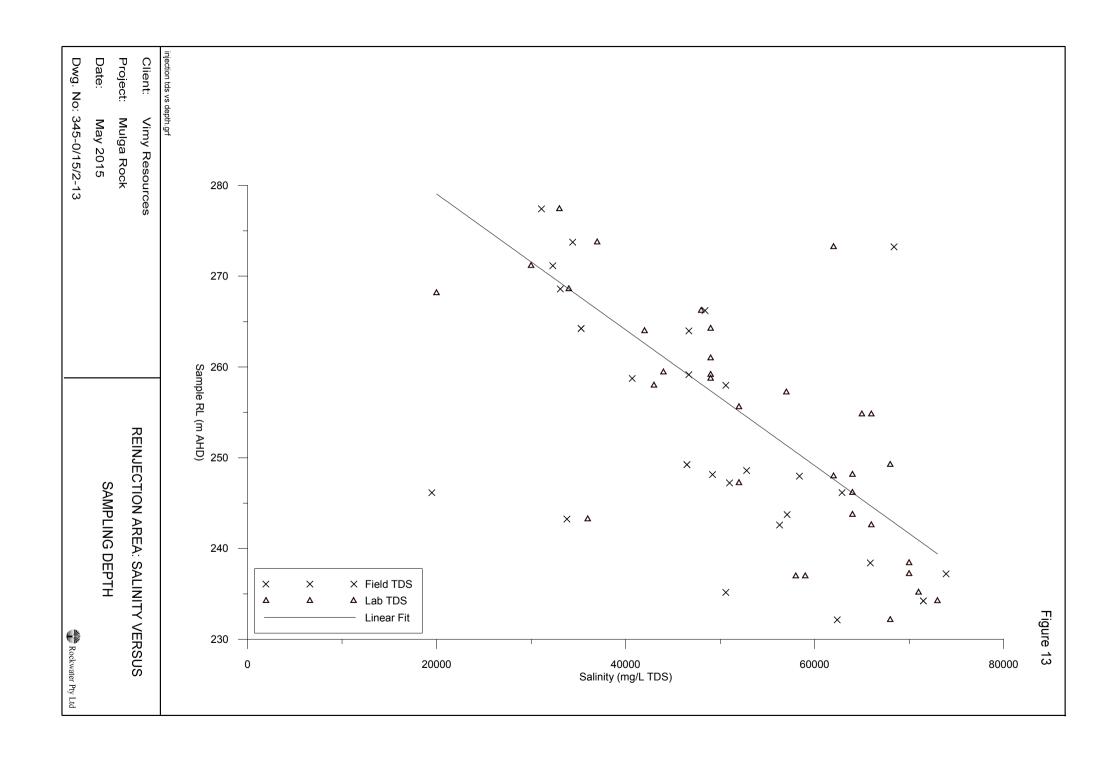
DATE: May 2015

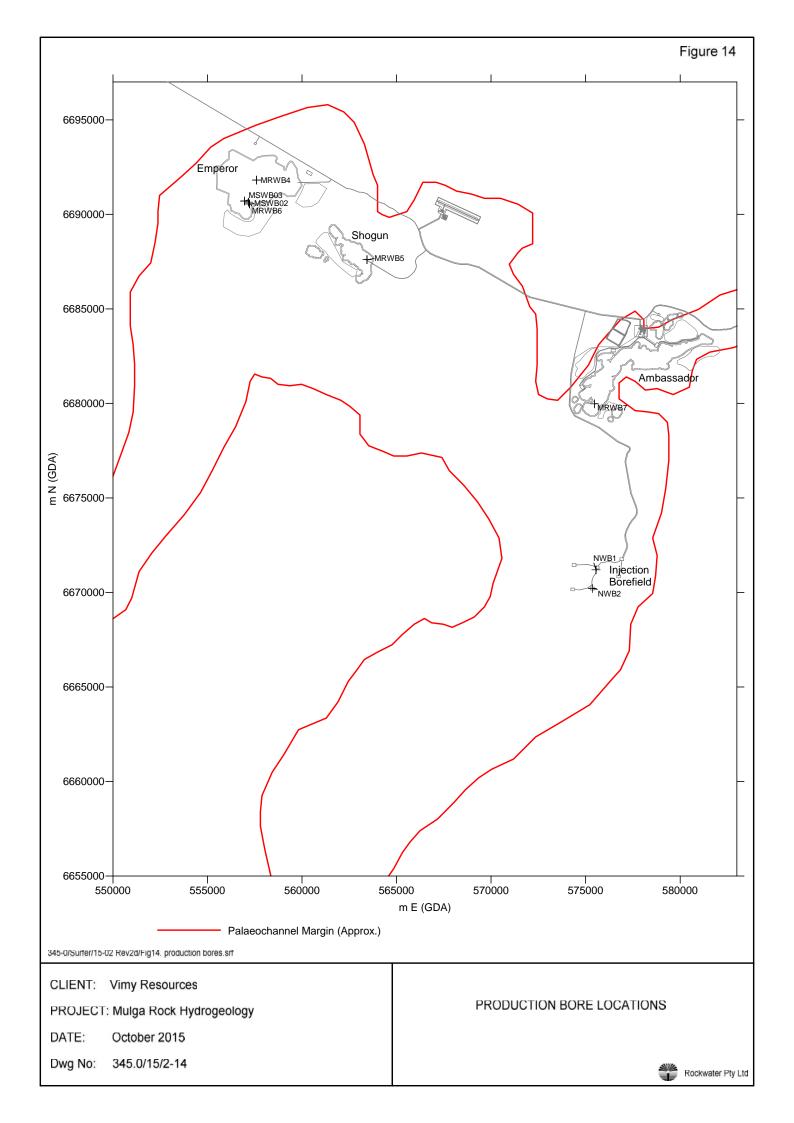
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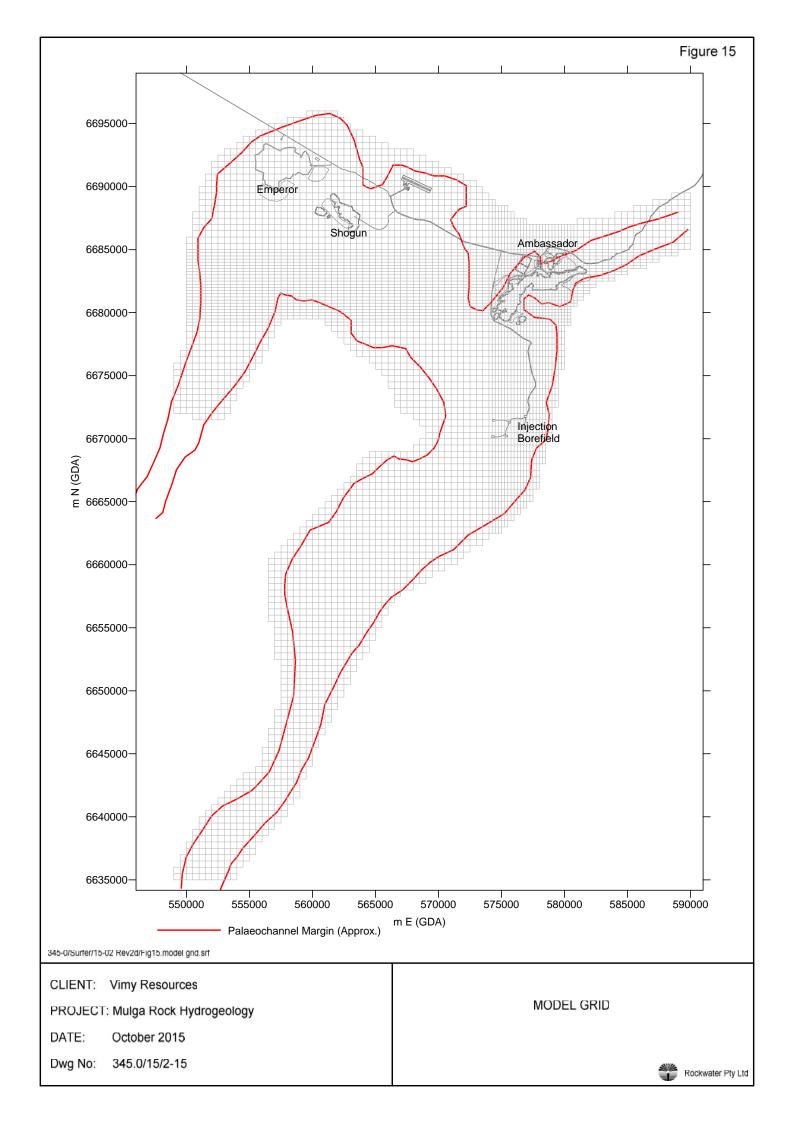
PIPER DIAGRAM
OF GROUNDWATER SAMPLES
MULGA ROCK DEPOSITS

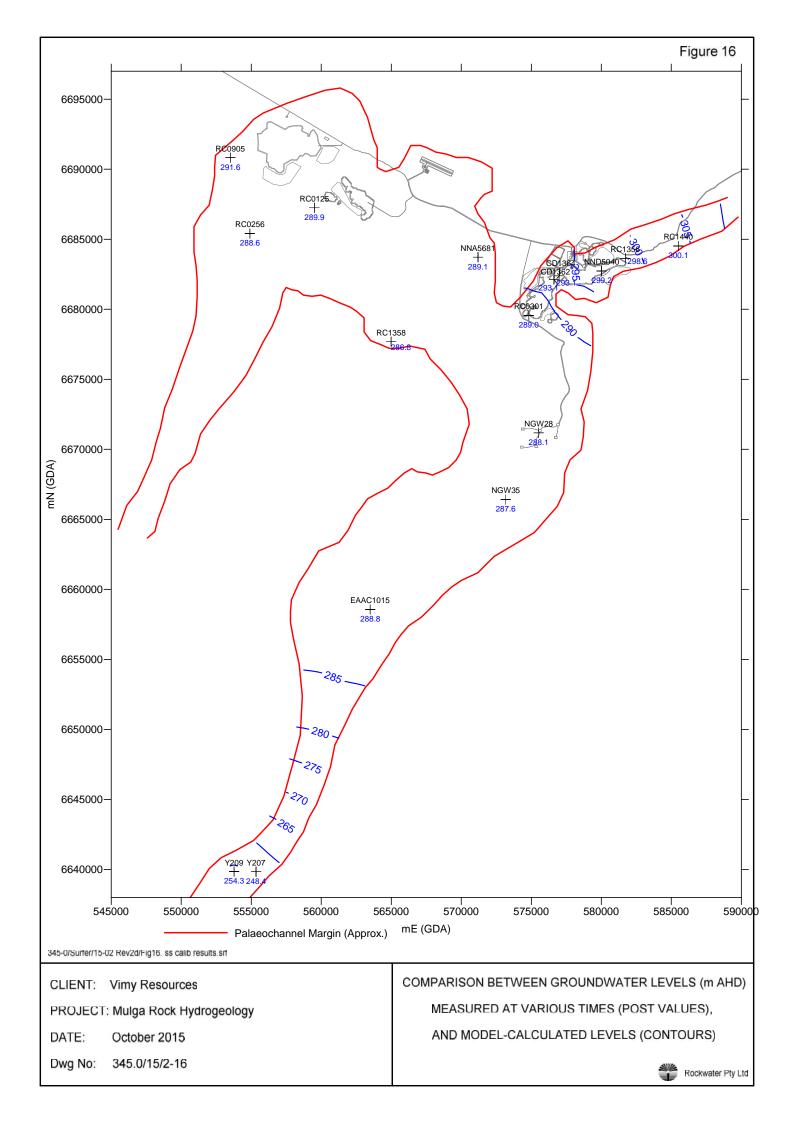
ANIONS

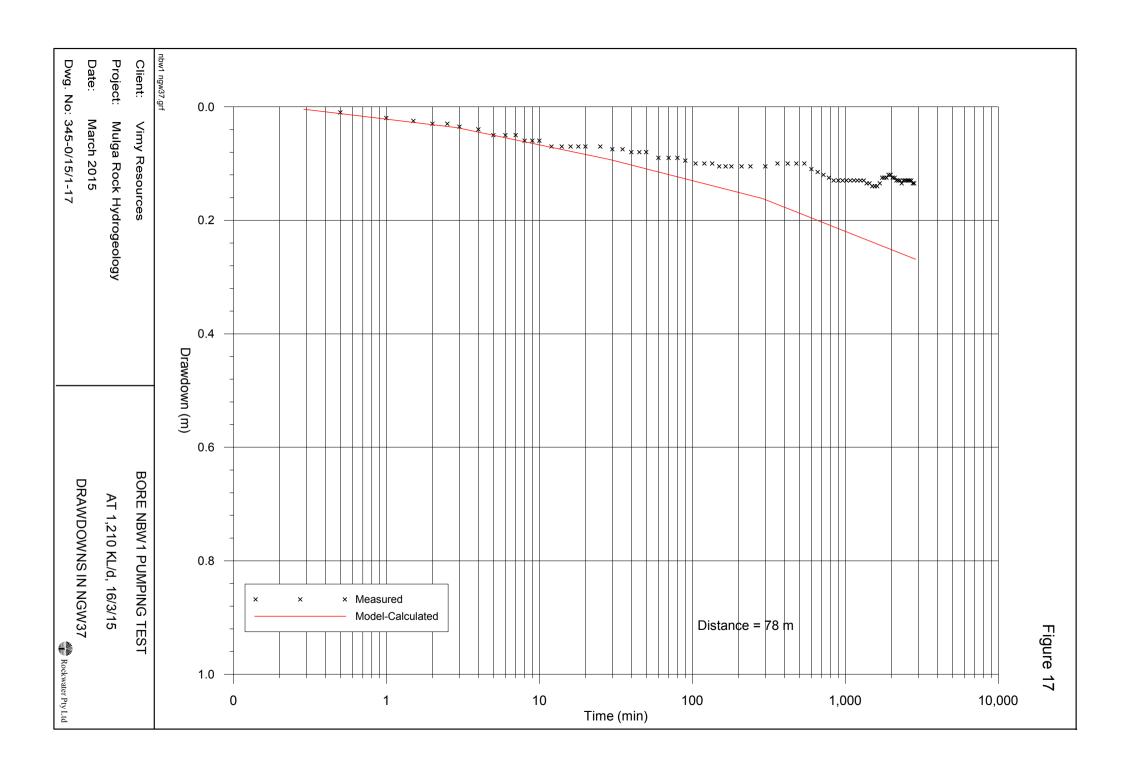


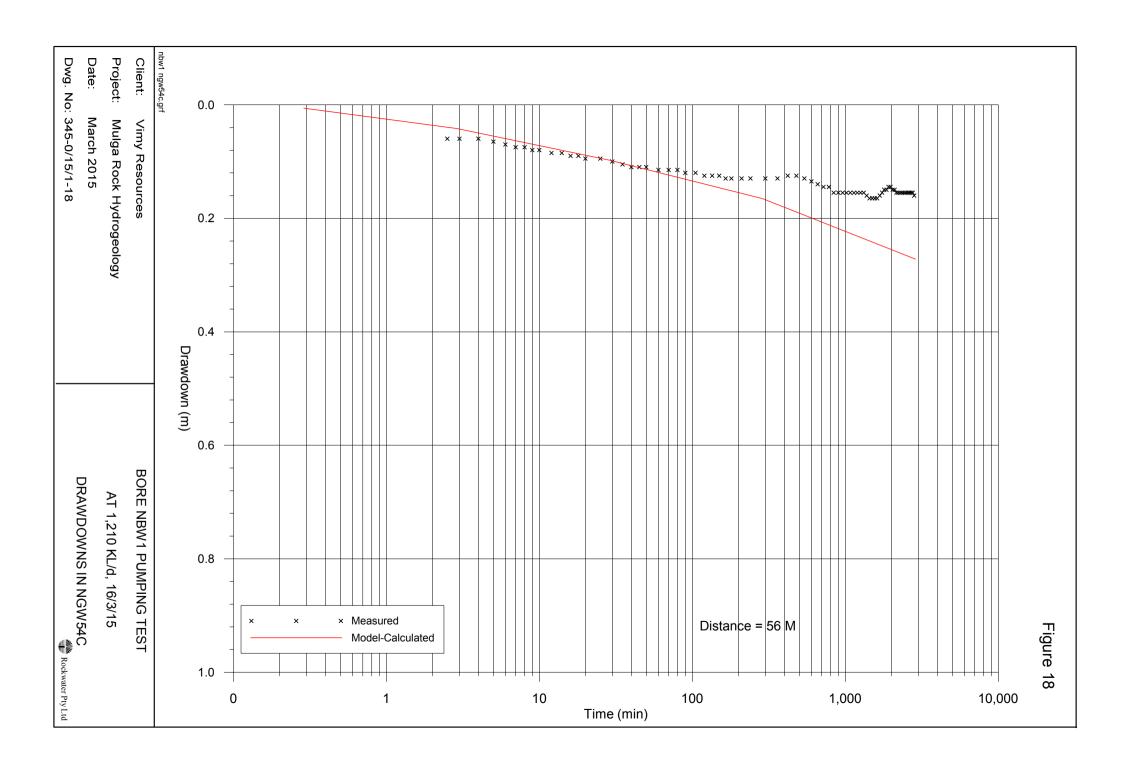


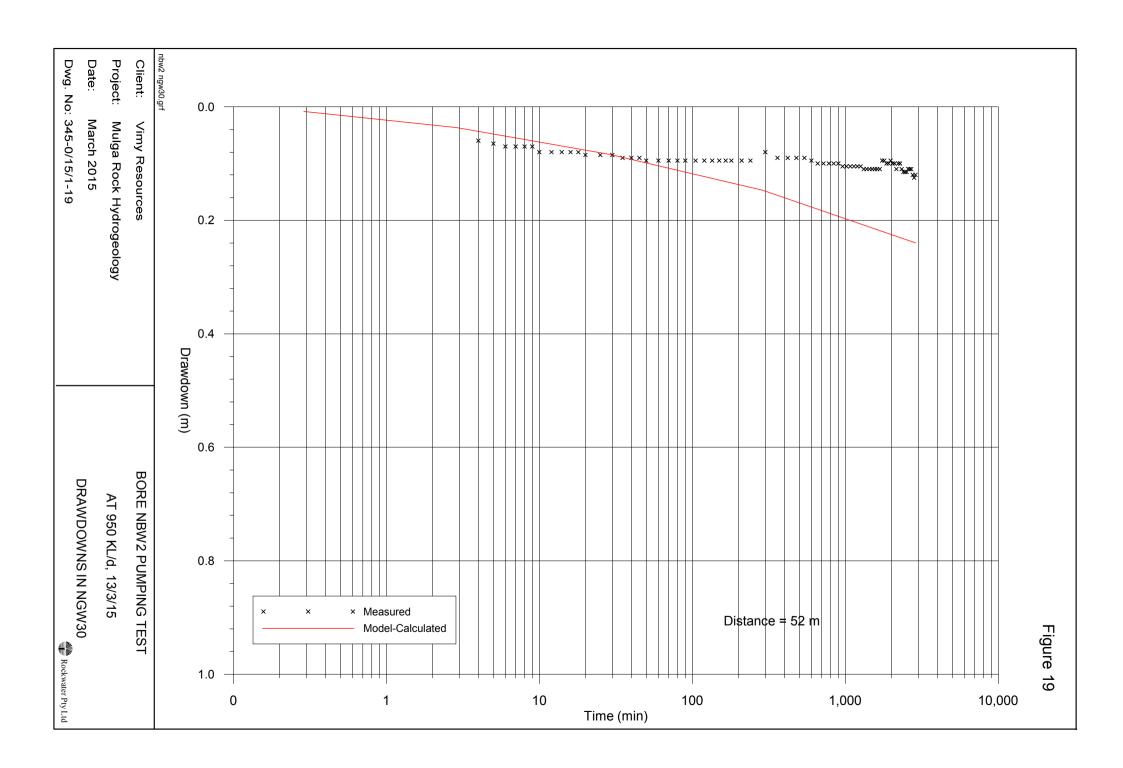


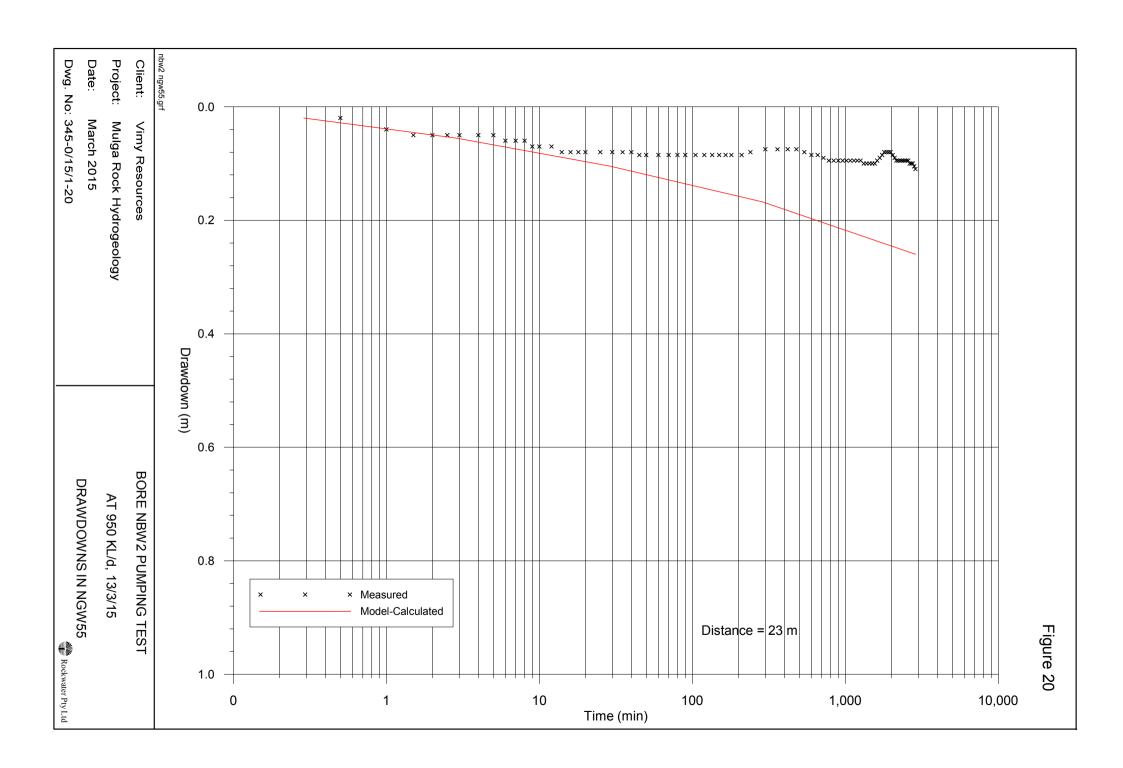


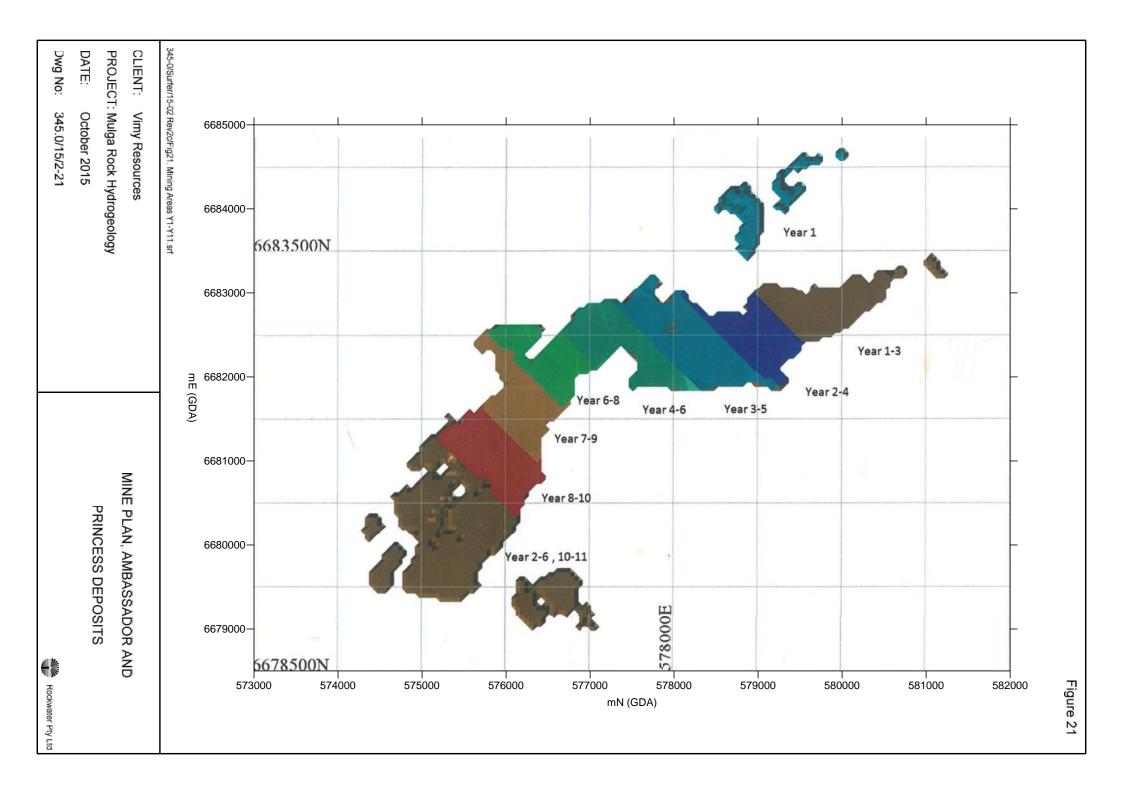


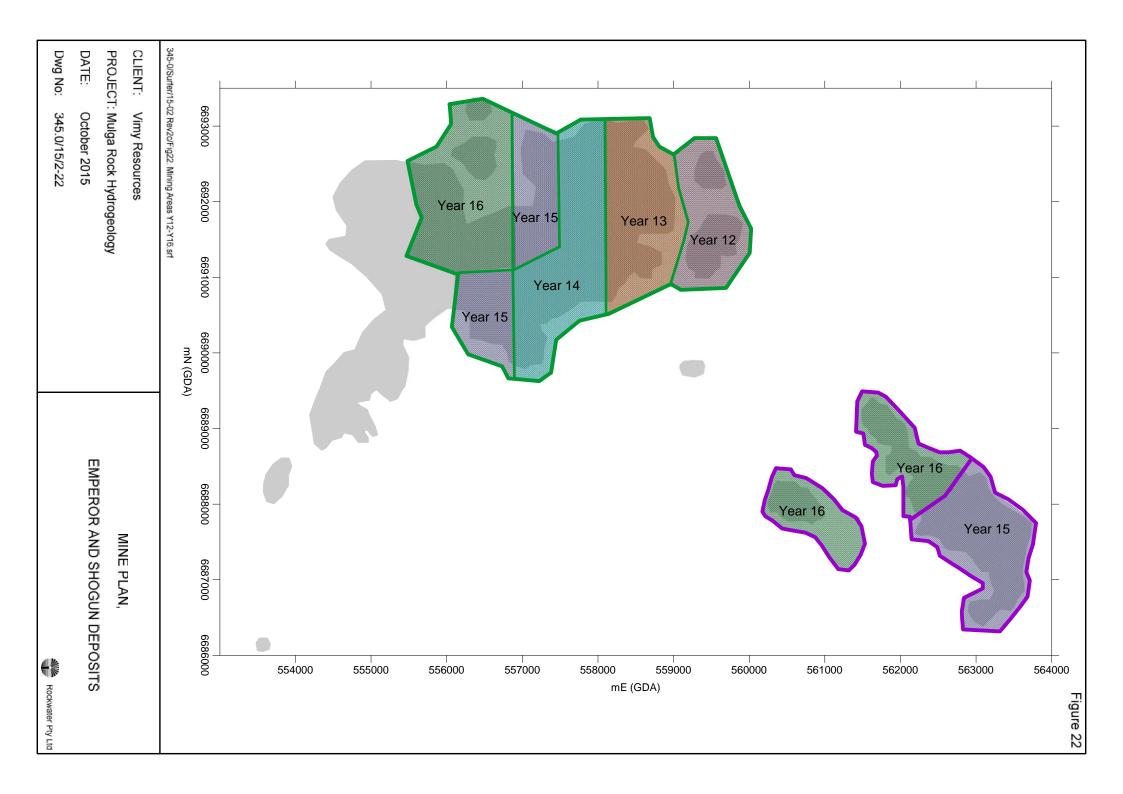


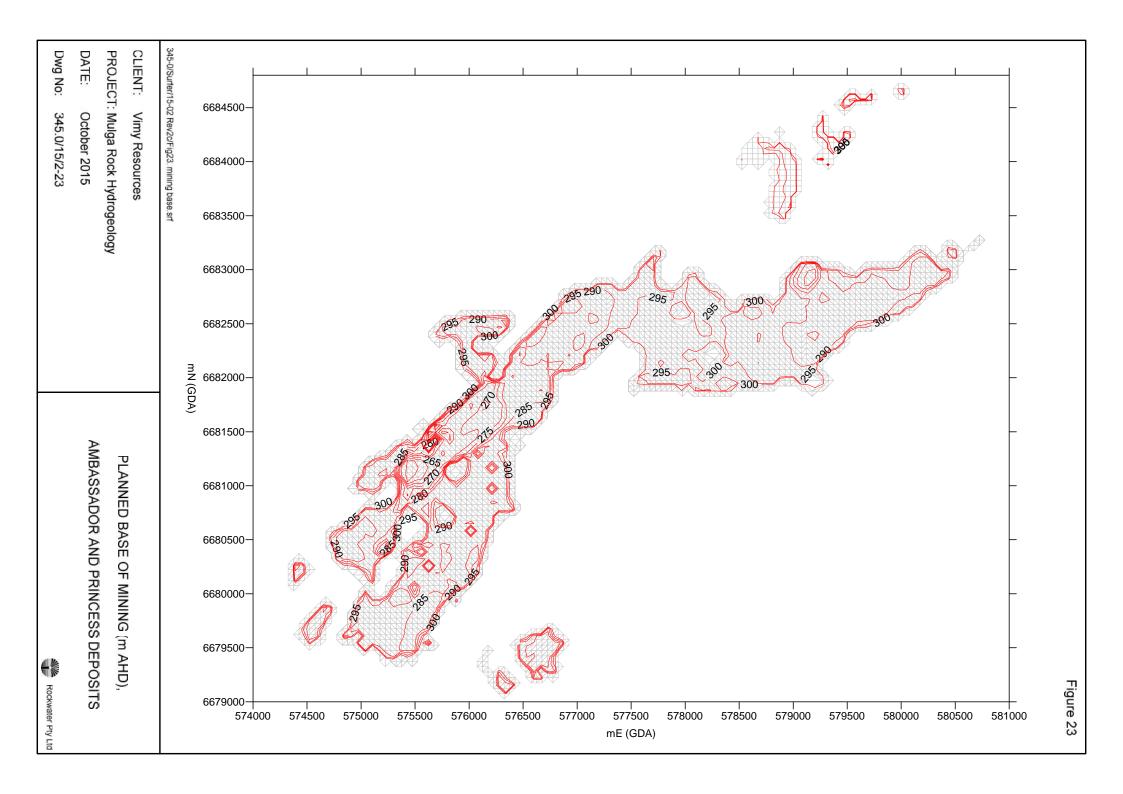


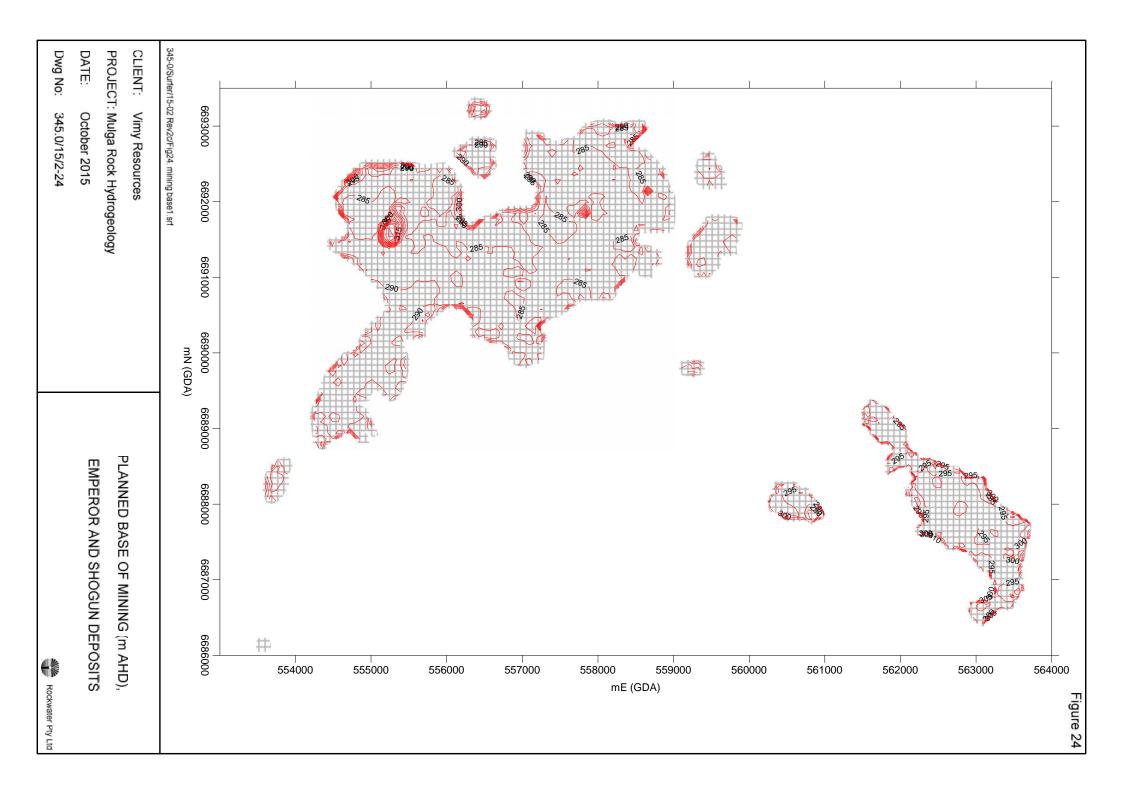


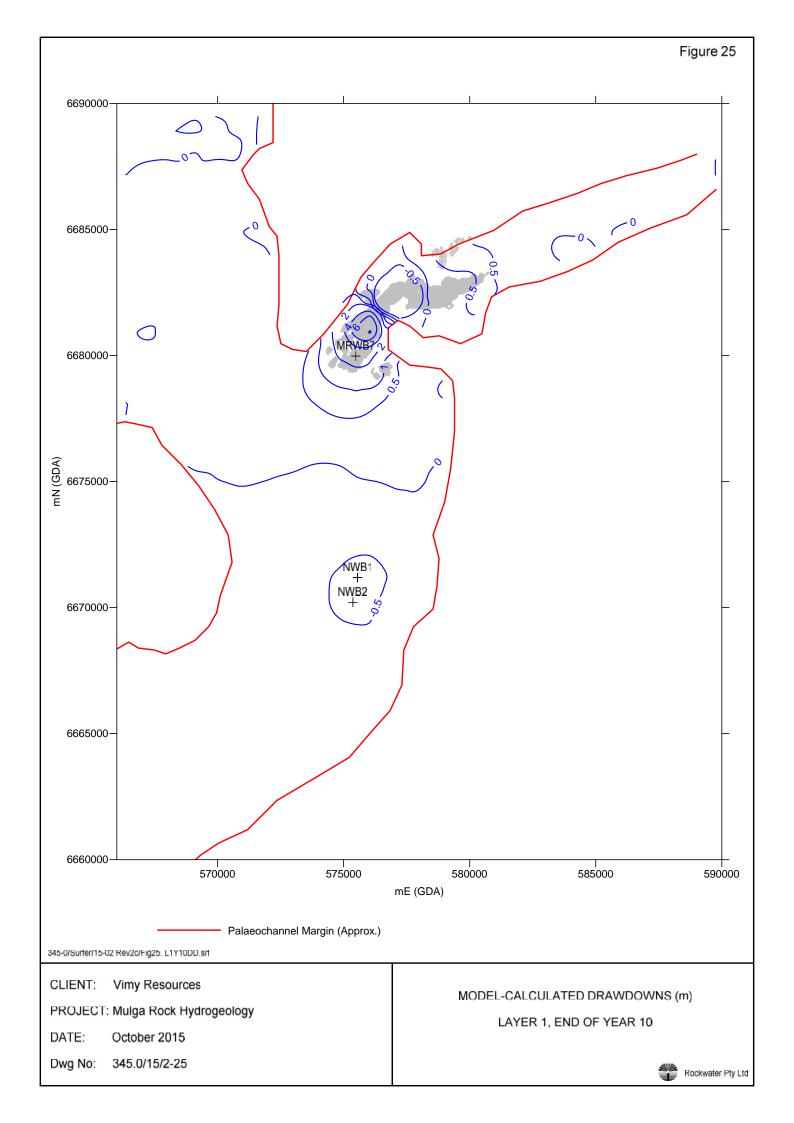


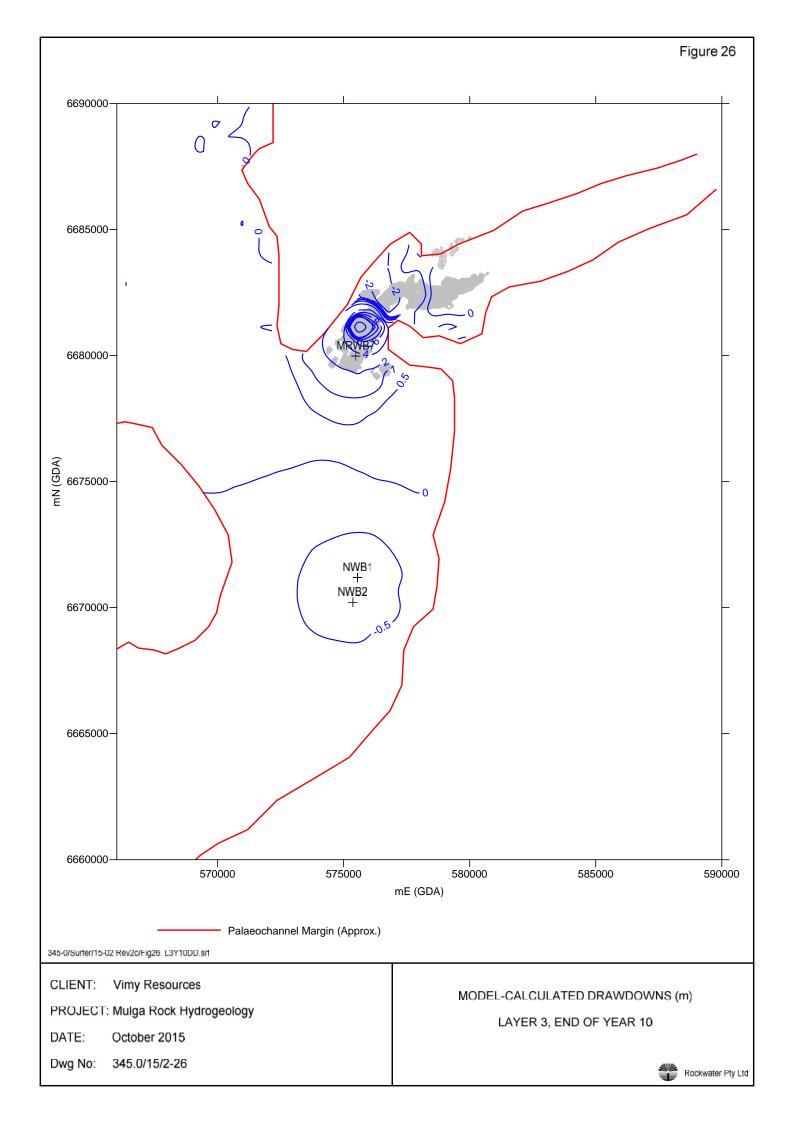


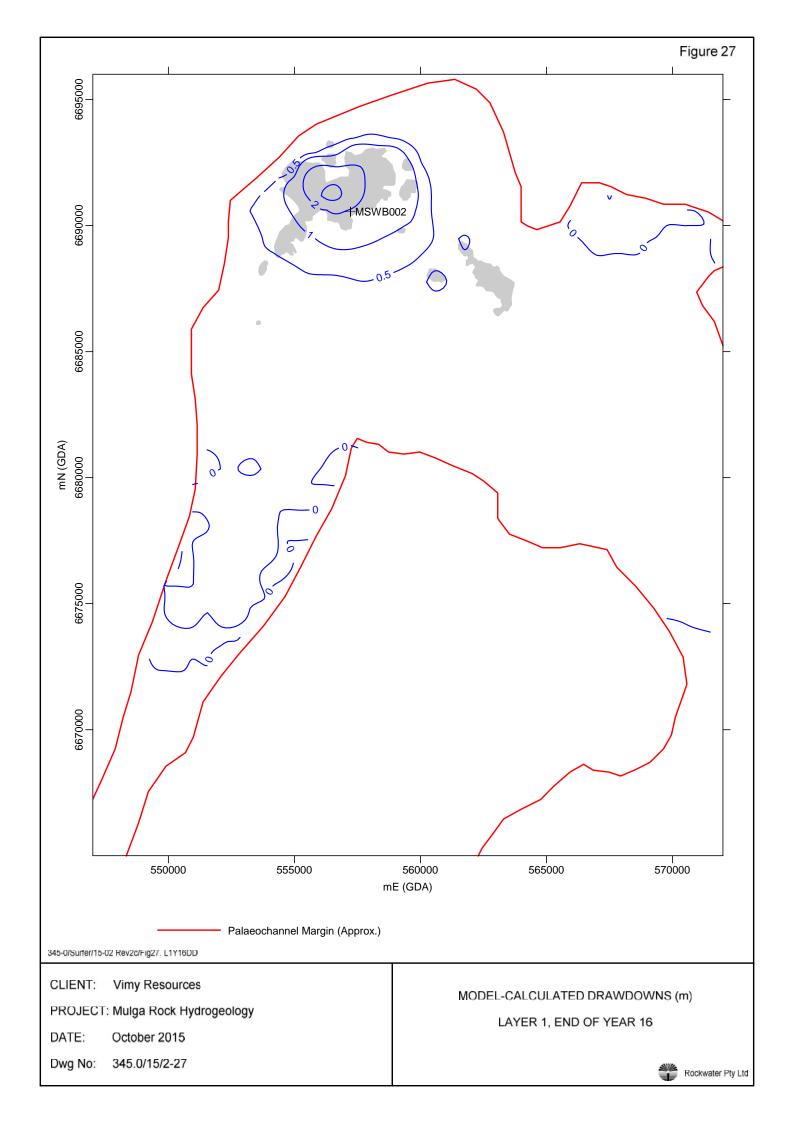


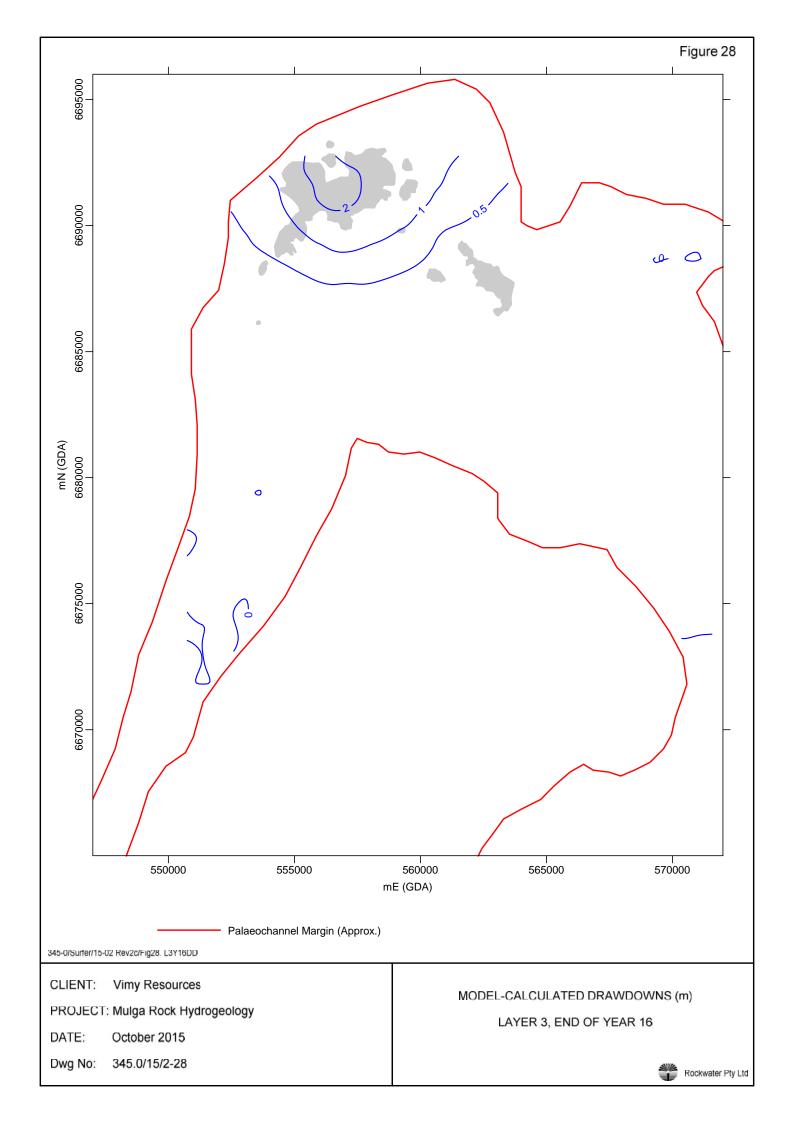


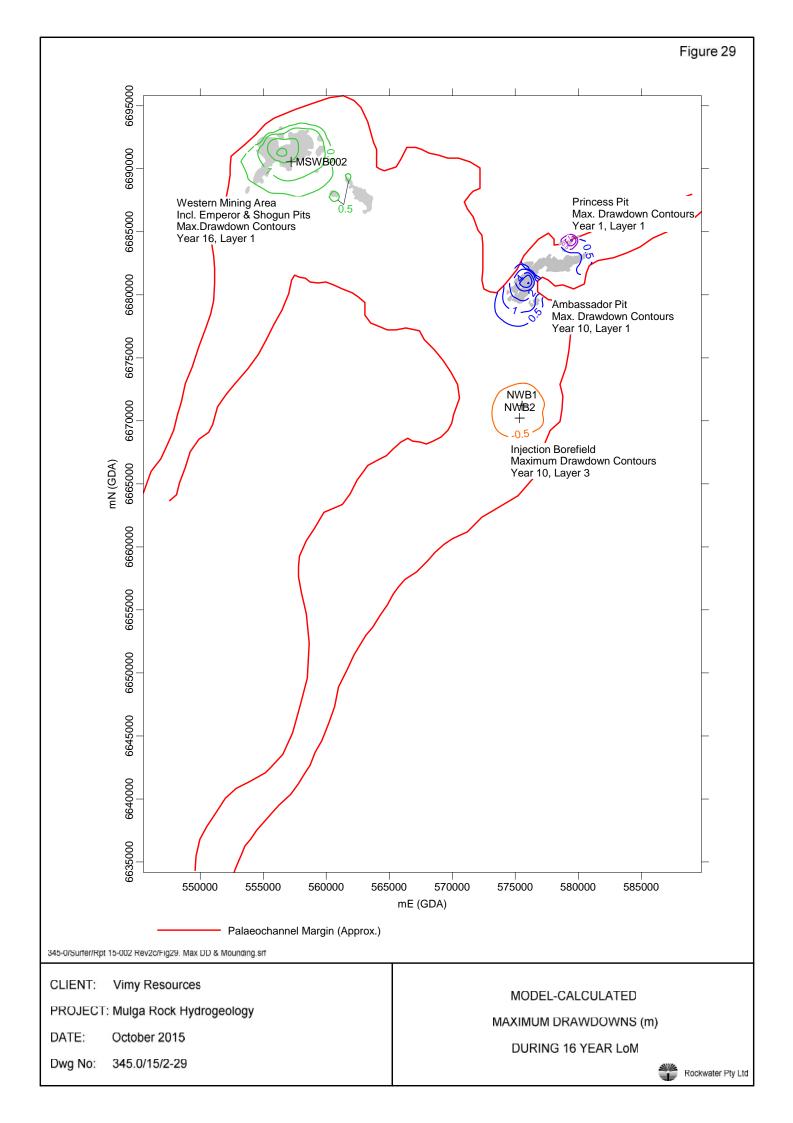


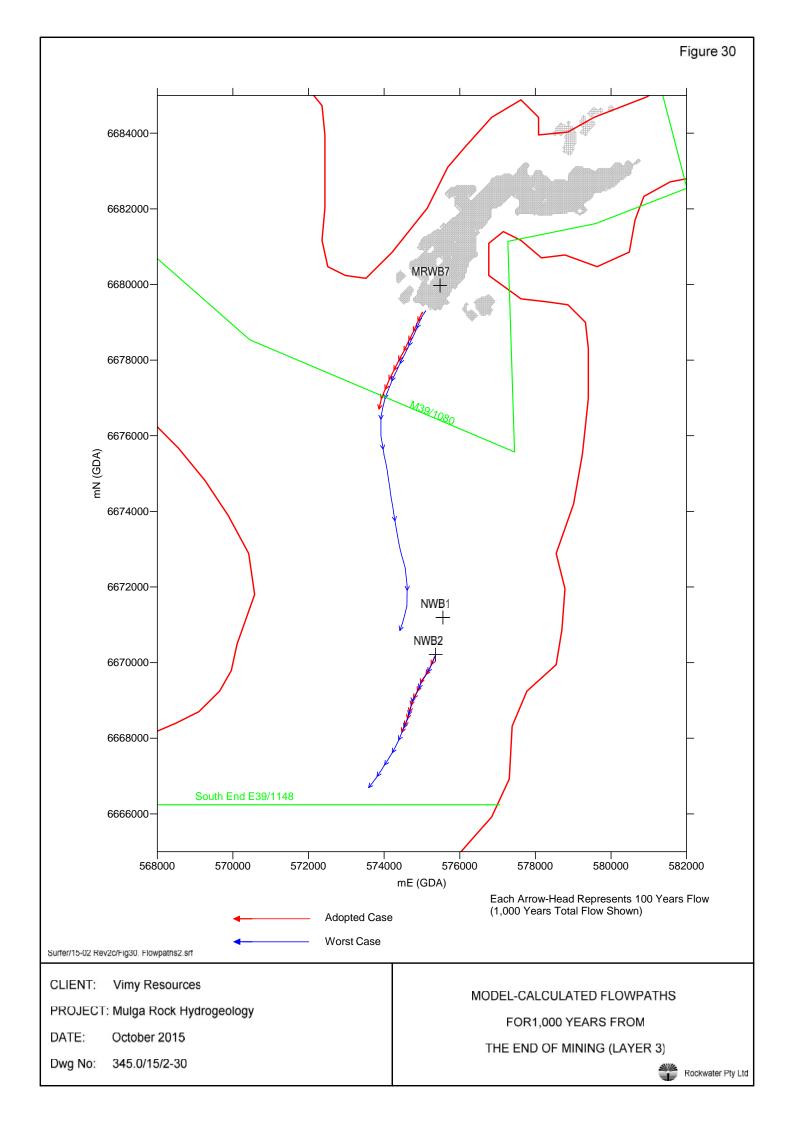




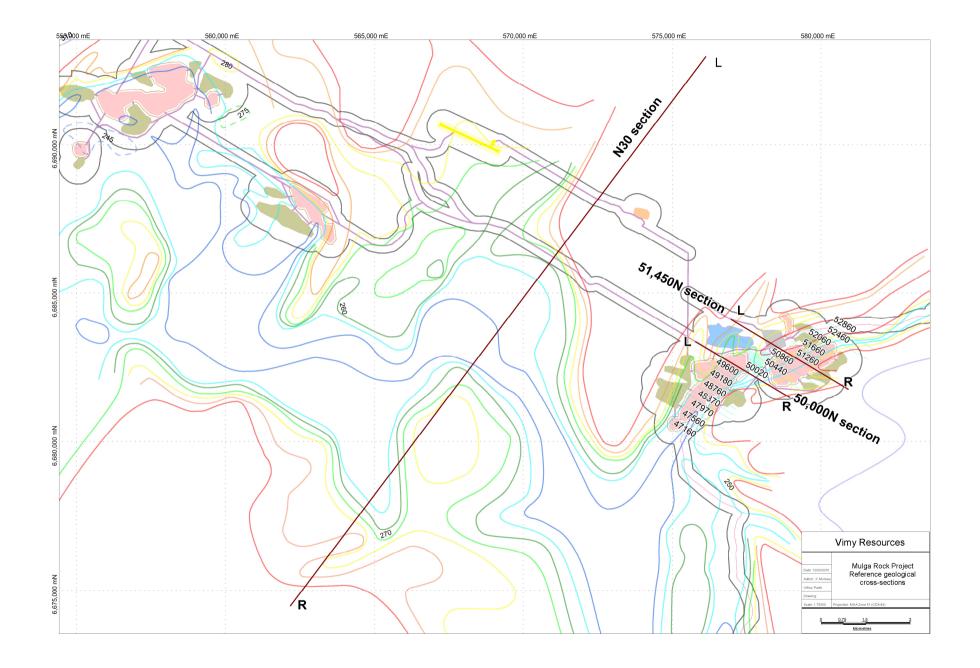


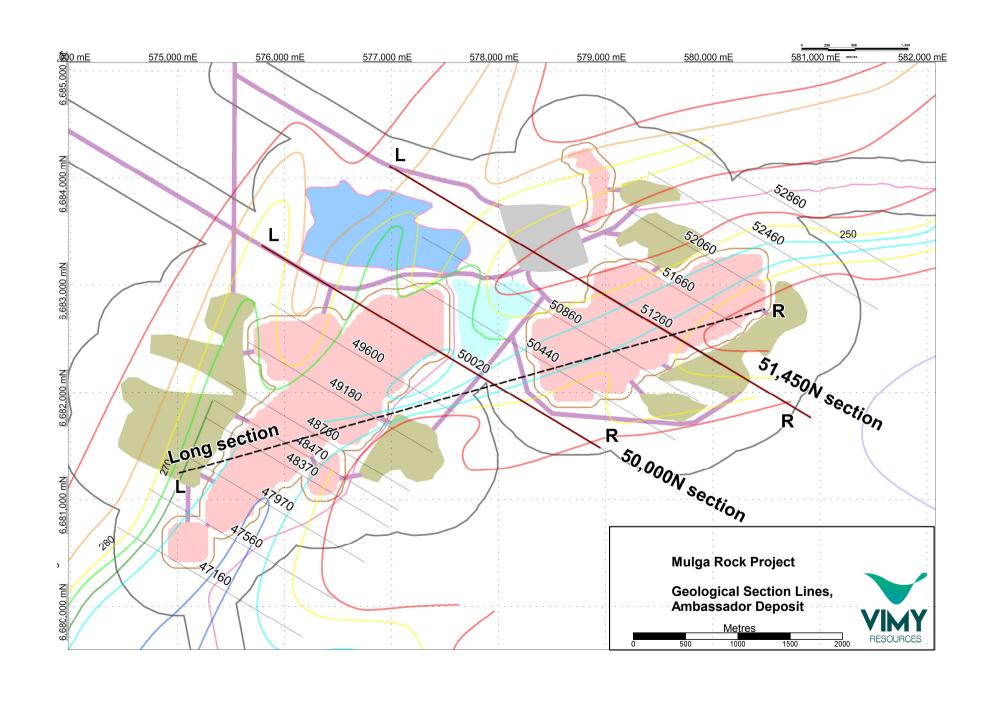


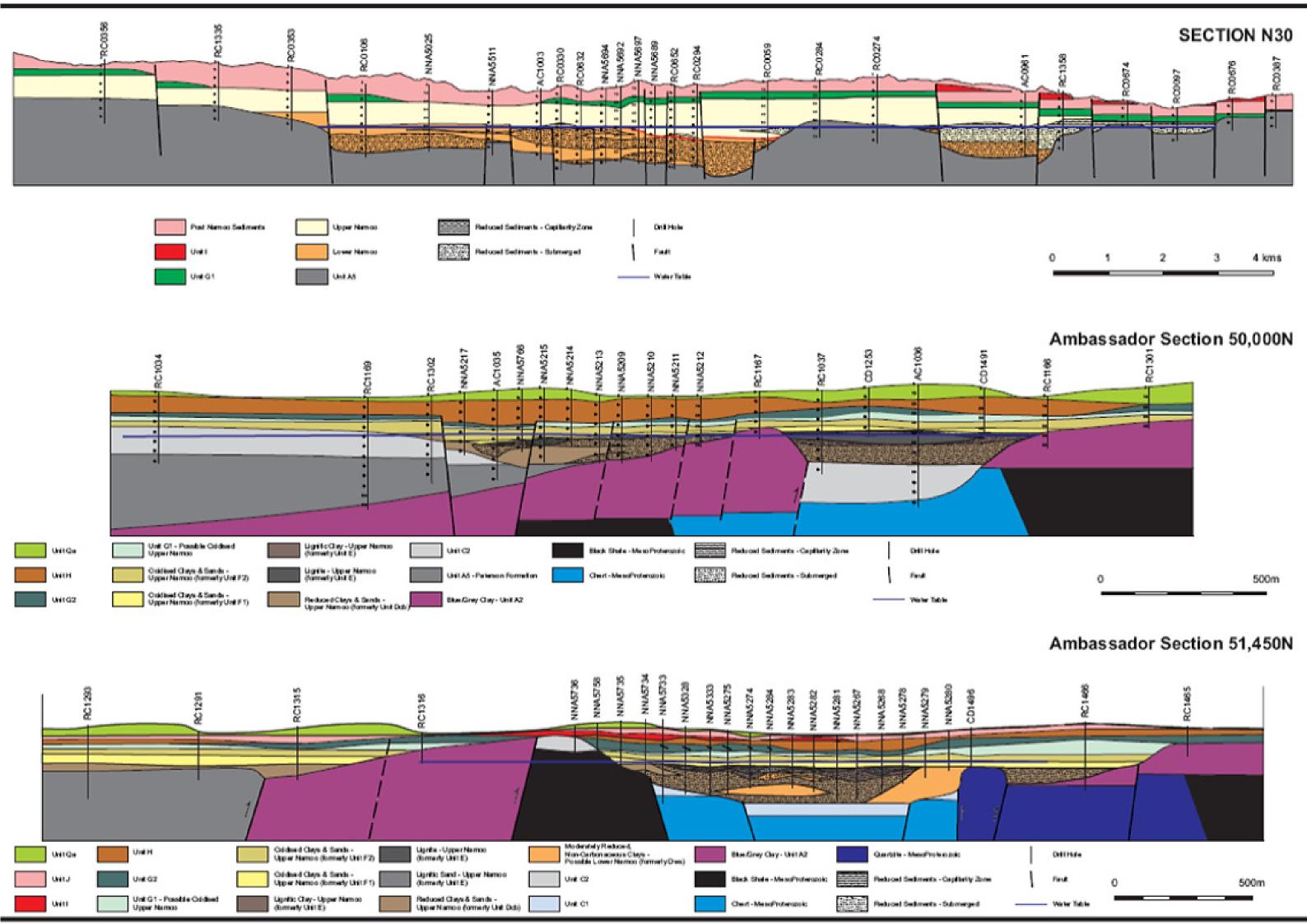


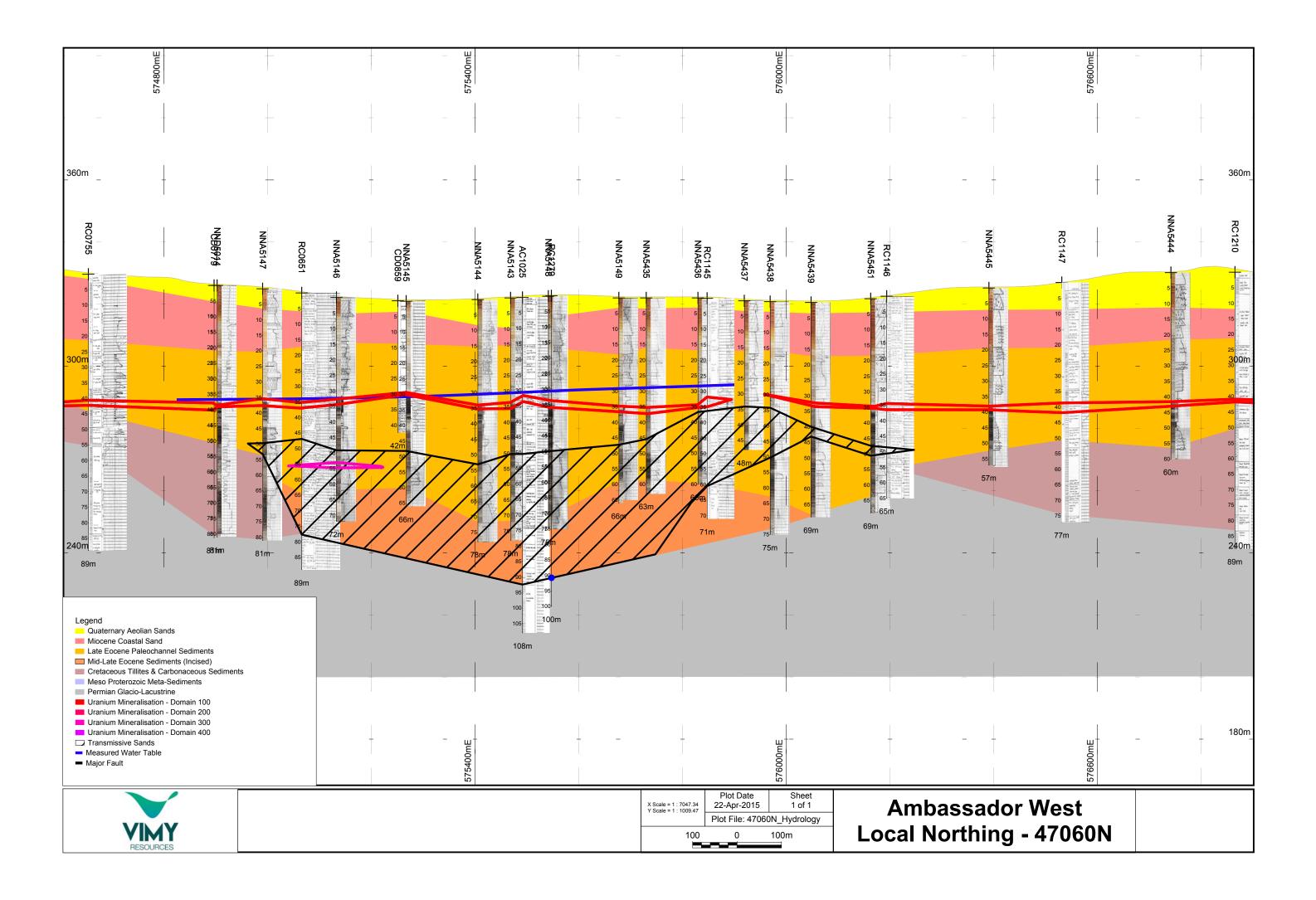


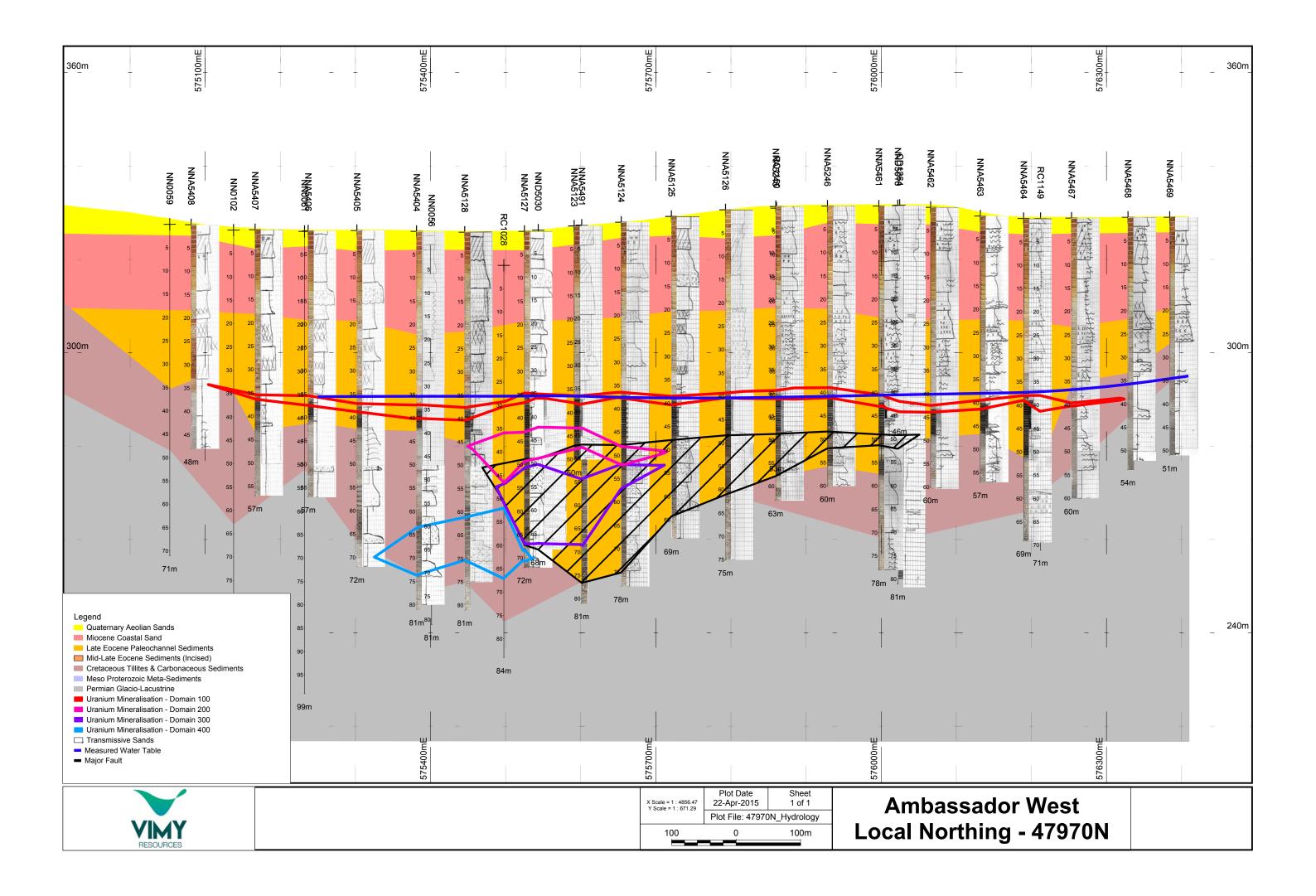
APPENDIX I GEOLOGICAL SECTIONS

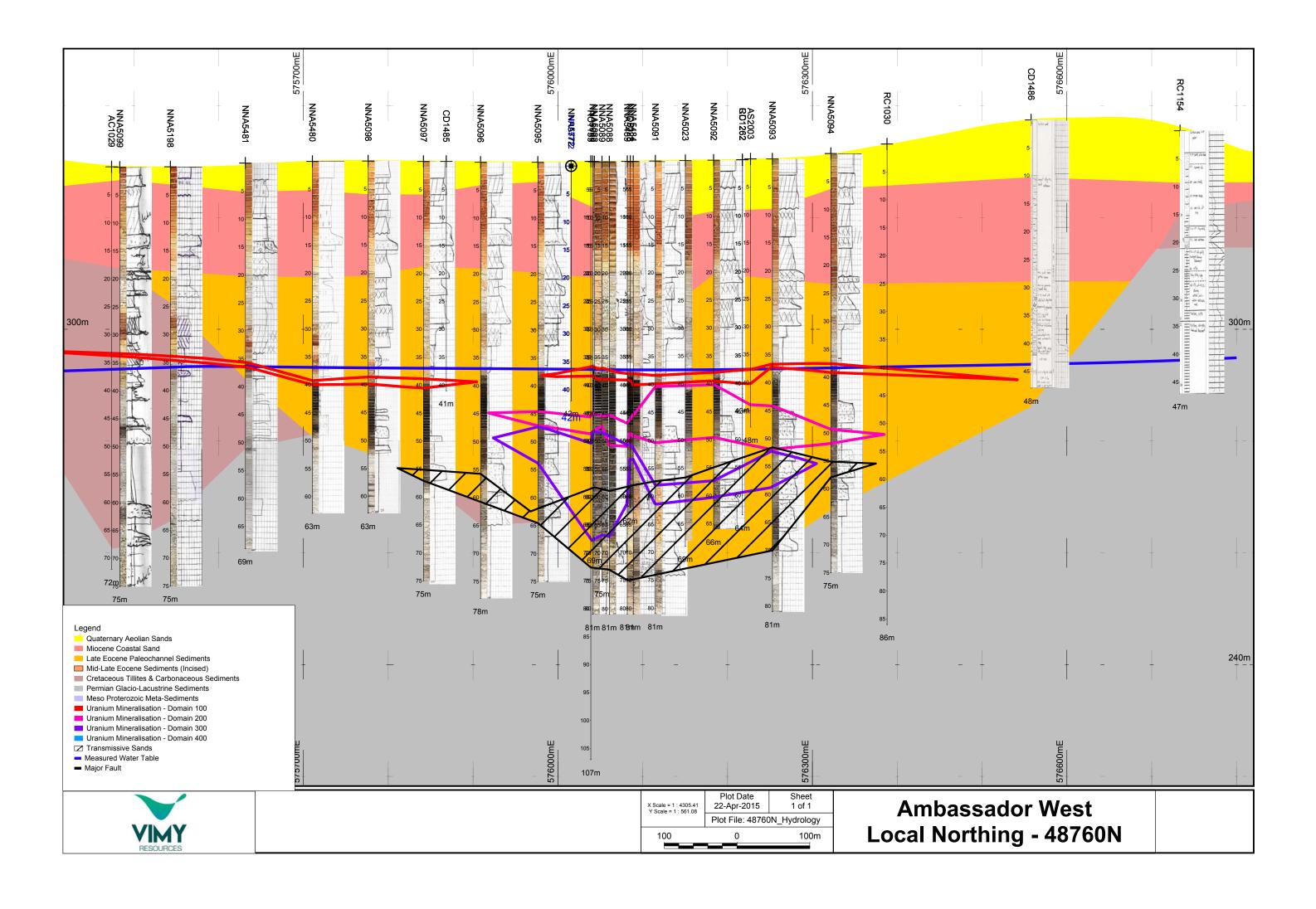


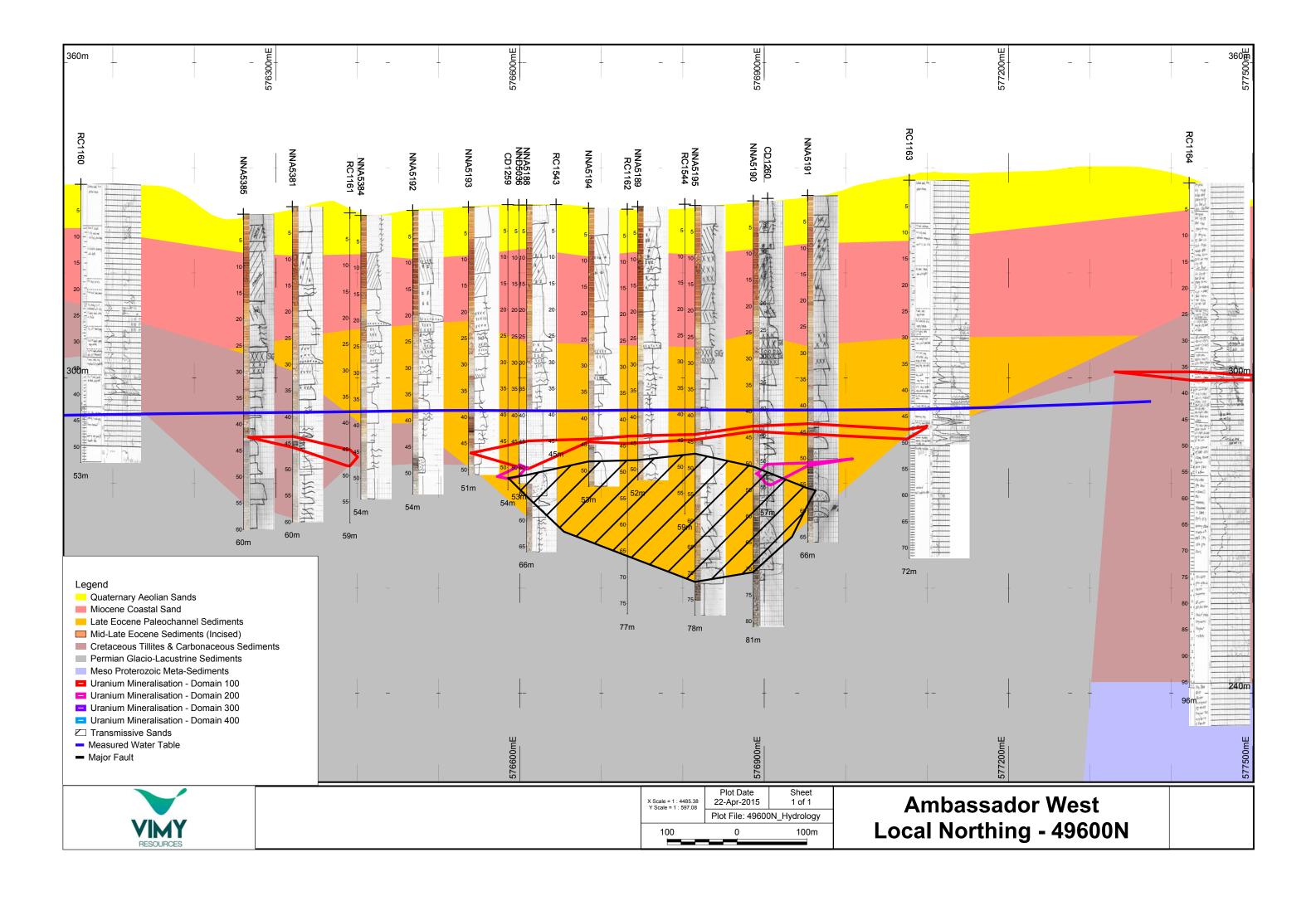


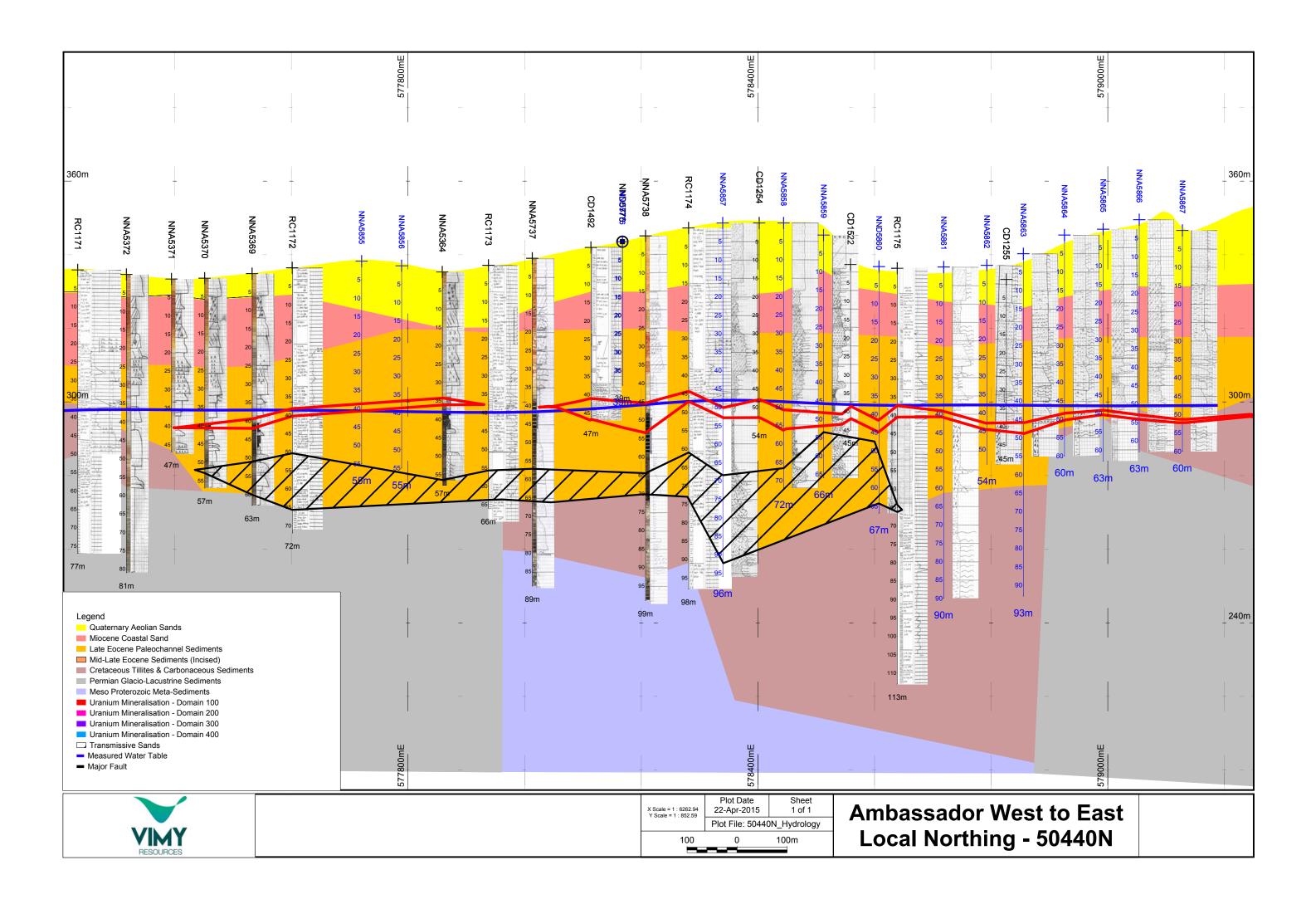


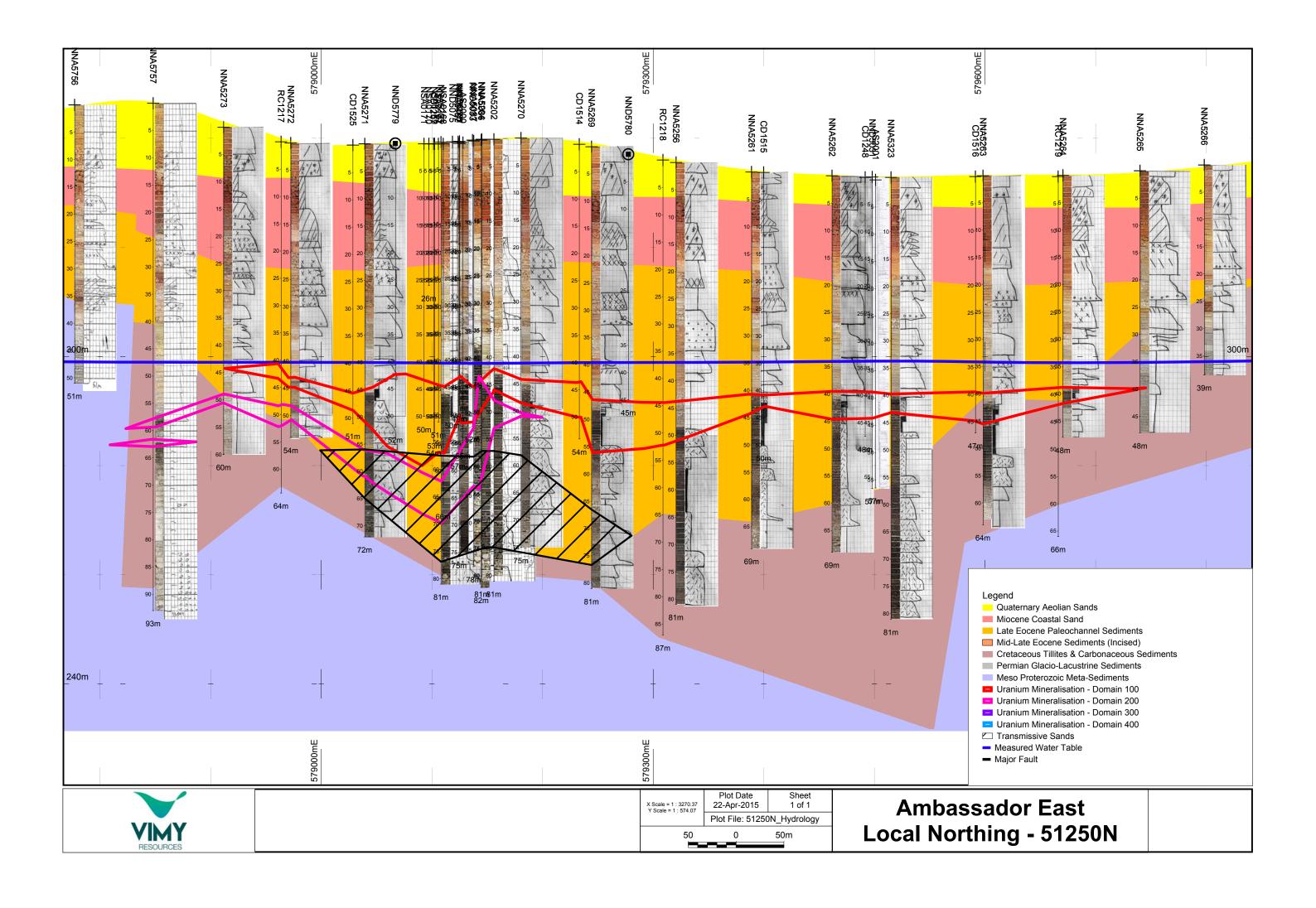


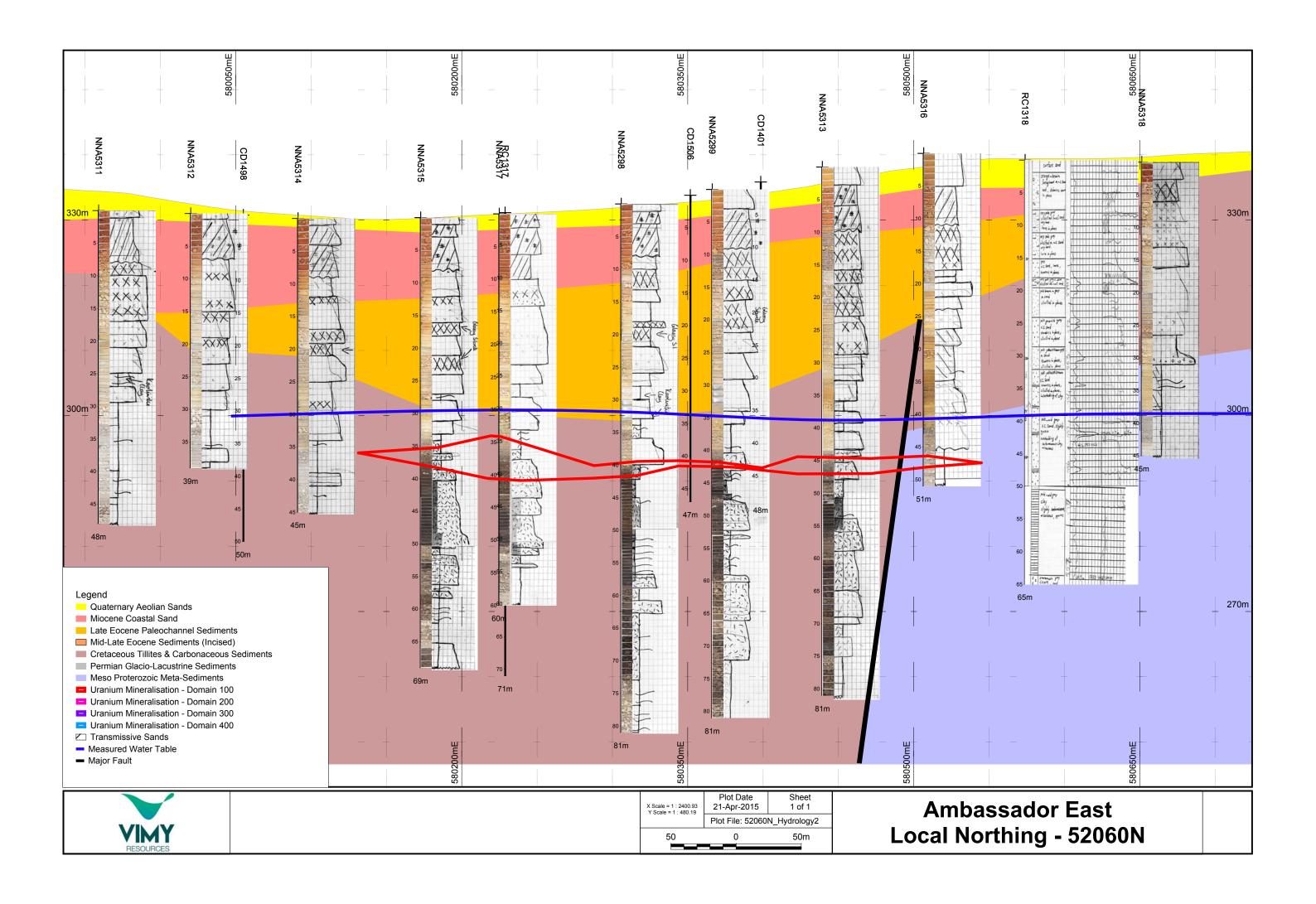


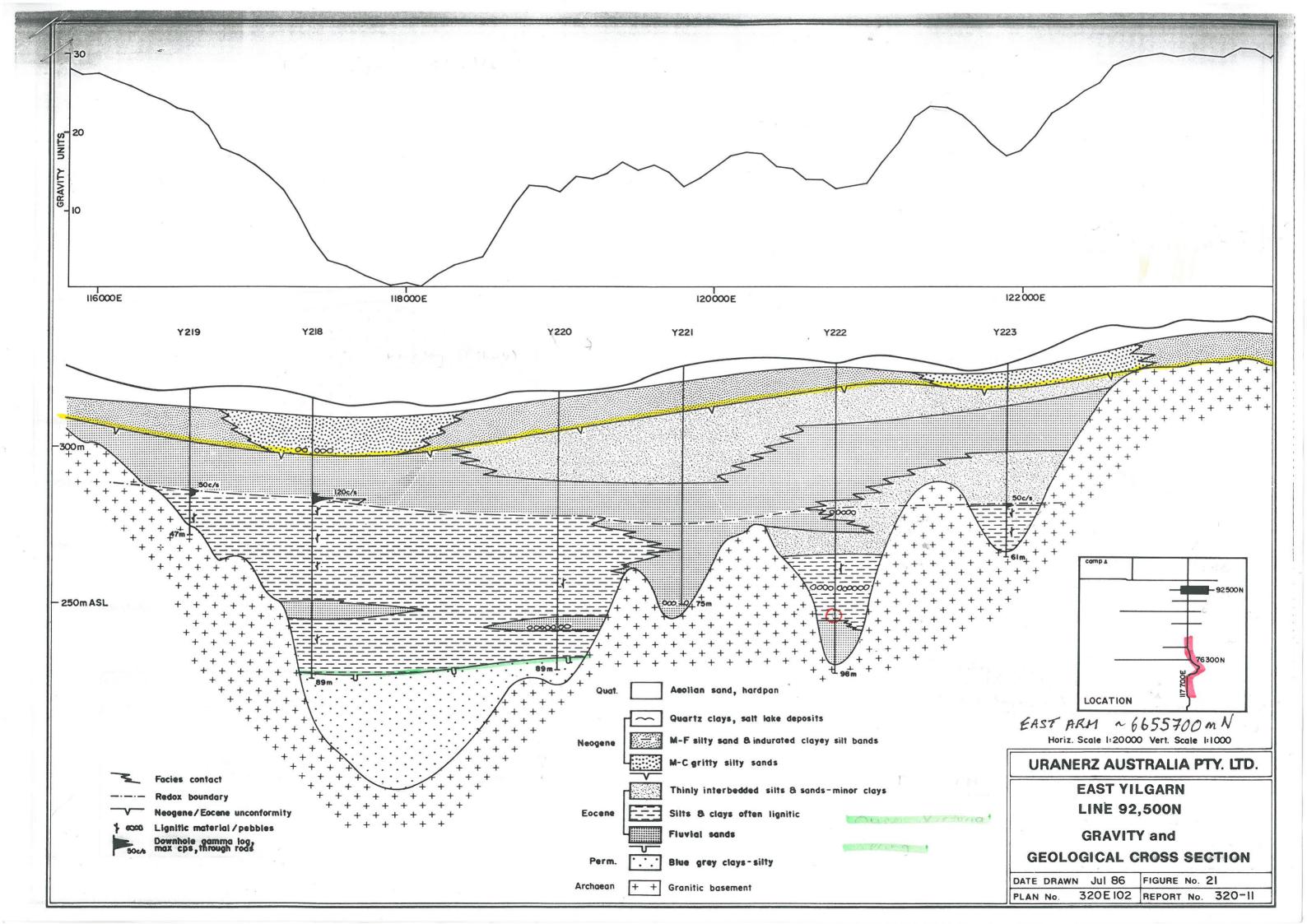












APPENDIX II RESULTS OF CHEMICAL ANALYSES

				1		1					1			1	1		1	ı																			_
Area	Hole ID	Date Sampled	GDA East	GDA North C	a Mg Na	к	CI	нсоз	SO4 NO3	RL	Sample DEPTH	Sample RL	T.F.R.	TDS	Cond	pH OR	P Hard	Alkalinity	он	Fe	Al	F S	i Br	1	U Th	Au	As_Sol	Ba_Sol Cd	Sol Cr_	Sol Cu_Sol	Co_Sol Pb_Sol	Mn_Sol	Ni_Sol	Sb_Sol	Sr Zn	V_Sol W	1
				mq	/L mg/L mg/L	mq/L	mg/L	mg/L	mg/L mg/L	m AHD			mg/L	mg/L	μS/cm	m\	/ mg/l	mq/l	mg/l	mq/l	mg/l i	mg/l me	g/l mg/l	mg/l	ug/l ug/l	ug/L	mq/l	mg/l m	g/I mo	y/I mg/I	mg/l mg/l	mq/l	mg/l	mg/l i	ng/l mg/l	mg/l mg	1/1
EMP + SHO	AC1139	27/3/1984	550163 550748	6690138 48	3 1,635 14,880								Ŭ	Ŭ	73,500	6.70	Ĭ		Ť	1.8					Ĭ	Ť	Ť					Ť	Ĭ				
EMP + SHO	AC1138 AC1051	27/3/1984	551420	6690908	8 1,585 14,880	448	25,210	37	3,522 16.6	346.2	65	281.2	45,760	45,760	73,900	7.10				2.0					<5 <5												
EMP + SHO	AC1050	8/07/1984	552025 552690	6690548 6686672 53	E 3.00E 4E.000	025	75 620	-0.6	13,600 2.8	342.4	53	289.4		52,670	229,600	7.75				190					<5 6												4
EMP + SHO	AC1204 AC1203	8/07/1984			5 3,995 45,000						?	250.9			218,000					140					<5 <5 <5 9												
EMP + SHO	AC0865 AC0865	25/1/1984 25/1/1984	552822 552822	6690867 56 6690867 66	1 2,030 21,550			<.6	7,542 2.2	335.6 335.6		271.1 262.6			103,700 128,800	4.20	-			110 2.6		0.7 3 0.8 2			30												_
EMP + SHO	NNA5707	Feb-12	552911		1 2,333 28,030	670	44,590	<.0	7,302 2	334.4		274.4		43,552	77,649	4.54				2.0		0.6 2	5		30												
EMP + SHO	AC1201 AC1200	8/07/1984 8/07/1984	553097 553353	6687579 53 6688015 53					13,440 0.5 13,090 0.7						217,000 212,400					34.5 26			_		<5 <5 <5 <5												_
EMP + SHO	AC1202	8/07/1984	553492						9,262 1.1			245.4	99,200	99,200	155,000	3.65				11					7 7												
EMP + SHO EMP + SHO	NNA5708 AC1198	Feb-12 8/07/1984	553528 553529	6690810	0 2.645 27.000	525	46 150	<0.6	8,178 1	334.7		262.7 262.0	92,160	67,522 92,160	117,939 144,000		-		-	10			_	1	<5 <5												_
EMP + SHO	NNA5709	Feb-12	553775	6690673	0 2,645 27,000	333	46,130	<0.0	0,170	332.6	59	273.6	92,160	39,387	70,424	3.68				10					<5 <5												
EMP + SHO	NNA5709 AC1196	Feb-12 8/07/1984	553775 553797	6690673 6688914 26	8 1.098 11.750	329	19.880	2	2.890 0.9	332.6 318.6		237.6 260.6	41.470	95,487 41,470	164,689 64.800		-			2.9					<5 <5												_
EMP + SHO	AC1199	8/07/1984	553996						13,020 0.9	_	60	252.8	142,100	142,100	222,000	3.20				27					<5 6												
EMP + SHO EMP + SHO	AC1195 AC1197	8/07/1984 8/07/1984	554080 554243	6689319 31 6688648 34			23,080		3,846 0.4 6,467 2.1	323.4		281.9 260.4	48,640 85,500	48,640 85,500	76,000 133,600					2.1					<5 <5 <5 <5												_
EMP + SHO	CD0737	27/9/1982	555622	6691014 23	2 947 10,800				2,460 0.1	324.6					55,600	7.60				1.2		0.3 <	2														
EMP + SHO	AC1246 NNA5710	Feb-12	556088 556539	6691253 6693155						327.5 334.9		280.7 274.9	37,630		64,559	3.77								1	<5 <5												_
EMP + SHO	NNA5711	Feb-12	556682	6693055						335.4	60	275.4		34,797	62,434	3.48																					
EMP + SHO	MSWB003 MSWB003	16/02/2012 24/07/2012	556958 556958		0 1,800 19,000	580	31,000	4	4,000 <0.1	318.4 318.4		240.4 240.4			94,000 78,000		8200	4	<1	13			-	++				<	0.1	<0.25	<0.01	0.67		-	+		\dashv
EMP + SHO	MSWB003	20/08/2012	556958	6690702		1				318.4	78	240.4		55,000	76,000	4.70	1								\perp										\bot		コ
EMP + SHO EMP + SHO	MSWB003 MSWB003	17/09/2012 28/10/2012	556958 556958	6690702 6690702 60	0 1,500 16,000	610	26,000	6	2,800	318.4 318.4		240.4 240.4		56,000 57,000			6800	6	<5	9.6	3.9	-+	-	++	-	+ -	<0.05	<0	.01	<0.01	0.05 <0.03	+ +	0.09	 	0.23		\dashv
EMP + SHO	MSWB003	26/11/2012	556958	6690702	,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,		1,,,,,,			318.4	78	240.4		58,000	81,000	4.50												-									コ
EMP + SHO	MSWB003 CD0735	22/01/2013 27/11/1984	556958 557121	6690702 6690615 55	0 550 28,100	695	48,200	<5	8,560 20	318.4 317.5	78	240.4		52,000	74,000 105,000		+	1	+	6.8		_	+	++	+			+	-			\vdash			+++		\dashv
EMP + SHO	CD0735	Late 1990-Mid 1991	557121	6690615 45	7 3,269 30,342	685	50,900	155	9,570	317.5	1	0.45 5		95,423		5.82 10	В			50	0.8	3.	3 71.4	0.94	<2	0.004		0.025		0.012			0.02	<0.005	8.8 0.015	<0.002 <0.00)15
EMP + SHO EMP + SHO	MSWB001 MSWB001	17/02/2012 24/07/2012	557176 557176		0 2,500 26,000	880	40,000	<1	5,600 <1	317.3 317.3		242.8 242.8		78,000 79,000	124,900 102,100		12000	<1	<1	13								0.0	033	0.006	0.85	2.8					-
EMP + SHO	MSWB001	20/08/2012	557176							317.3					100,000																						
EMP + SHO EMP + SHO	MSWB001 MSWB001	17/09/2012 28/10/2012	557176 557176	6690643 6690643 42	0 2,300 23,000	870	40,000	<5	5,100	317.3 317.3	74.5 74.5	242.8 242.8		79,000 75,000	108,130 108,766		11000	<5	<5	0.25	8.2		-	+			<0.05	<0	.01	<0.01	0.01 0.54		0.02		0.08		-
EMP + SHO	MSWB001	26/11/2012	557176	6690643						317.3	74.5	242.8		81,000	110,000	3.90																					_
EMP + SHO	MSWB001 MSWB002	22/01/2013 14/11/2011	557176 557225	6690643 6690545						317.3 317.0		242.8 245.0		75,000 86,000					1													1					-
EMP + SHO	MSWB002	22/01/2012	557225	6690545 47		1,000			7,600 <2	317.0		245.0		88,000			13000		<1	_									002	9.6	0.56						_
EMP + SHO	MSWB002 MSWB002	16/02/2012 18/03/2012	557225 557225	6690545 51 6690545	0 3,200 32,000	860	45,000	2	7,700 <0.1	317.0 317.0		245.0 245.0		87,000 88,000			15000	2	<1	83								<	0.1	3	0.021	1.4					_
EMP + SHO	MSWB002 MSWB002	15/04/2012 14/05/2012	557225 557225	6690545 6690545 47	0 2,500 25,000	920	4 700	5	7,700 <0.1	317.0 317.0		245.0 245.0		88,000 89,000	143,000 144,400		12000	5	<5	13							<0.03	0.0	009	2,6	0.011 0.18	0.98	0.68		26		4
EMP + SHO	MSWB002 MSWB002	14/05/2012	557225	6690545 47	0 2,300 23,000	920	4,700	5	7,700 <0.1	317.0		245.0		89,000	144,400	5.80	12000	5	<5	13							<0.03	0.0	009	2.0	0.011 0.18	0.96	0.00		20		\dashv
EMP + SHO	MSWB002 MSWB002	28/06/2012 24/07/2012	557225	6690545 6690545						317.0 317.0		245.0 245.0			146,400 108,400																						_
EMP + SHO	MSWB002 MSWB002	20/08/2012		6690545						317.0		245.0			108,400																						
EMP + SHO	MSWB002 MSWB002	17/09/2012 28/10/2012	557225 557225		0 2,600 25,000	030	46,000	21	6,300	317.0 317.0		245.0 245.0		89,000 81,000	117,884 113,272		12000	21	<5	34	1.6			-			<0.05	-0	.01	0.14	<0.01 <0.03		<0.02		0.76		_
EMP + SHO	MSWB002 MSWB002	22/01/2013	557225	6690545	0 2,000 23,000	330	40,000	21	0,300	317.0		245.0		81,000			12000	21	ζ3	34	1.0						<0.03	ν.	.01	0.14	20.01		C0.02		0.70		
EMP + SHO EMP + SHO	RC0885 RC0502		557572 557575							321.4 321.4	67	254.4	78,000 76,670			4.15								1	10 <5				-								_
EMP + SHO	RC0502	15/7/1983	557575	6691799 60	0 2,350 21,800		37,060			321.4	O/	204.4	70,070	70,070	117,200	5.10				7.9		0.2 2	5														
EMP + SHO EMP + SHO	RC0502 RC0502	25/11/1983 31/10/1984	557575 557575	6691799 50 6691799 62		509	39,050 37,400			321.4 321.4					120,200 87,000		-		-	7				+	15							-			-		-
EMP + SHO	RC0502	Late 1990-Mid 1991	557575	6691799 51	1 1,930 19,066	444	32,900	24	5,920	321.4				60,854		5.11 10	В			39			.7 30.9	0.63	<2	0.002		0.026	0.0	12 0.004	<0.005 0.017	0.95	0.07	<0.005	7.7 0.155	<0.002 <0.00)15
EMP + SHO EMP + SHO	CD0723 NNA5699	27/9/1982 Feb-12	557699 559222	6691244 25 6690338	2 1,160 14,400	251	22,930	<.6	3,070 0.2	316.7 315.7	63	252.7		76.107	71,200 132,644		+		+ +	2.1		0.6 <	2	+ +	-									-	+++		\dashv
EMP + SHO	NNA5700	Feb-12	559348	6690242						314.9	42	272.9		80,102	139,359	3.51																					
EMP + SHO EMP + SHO	NNA5700 NNA5703	Feb-12 Feb-12	559348 559383	6690242 6690004	-					314.9 308.0		245.9 274.0		10,317	59,289 19,509																						-
EMP + SHO	NNA5703	Feb-12	559383	6690004						308.0	58	250.0		74,577	130,349	3.43			$\downarrow \downarrow \downarrow$																		コ
EMP + SHO		Feb-12 Feb-12	559502 559502	6690171 6690171	+ +		+ +			312.7 312.7		288.7 252.7			11,689 128,734			1	+	-				++					_			+ +		-	+		\dashv
EMP + SHO	NNA5702	Feb-12	559580	6690341 6690341		1					30	285.8		23,237	42,459	3.60	1	ļ					1	\Box	\perp										\Box		コ
EMP + SHO	NNA5702 NNA5705	Feb-12 Feb-12	559580	6689903						308.0		272.0		29,272	123,209 52,829	2.89						<u></u> L_		ш													
EMP + SHO	NNA5705 NNA5698	Feb-12 Feb-12		6689903 6690073			\Box			308.0 309.0		251.0 270.0			128,989 68.894				$+\Box$	1												\vdash			\Box		7
EMP + SHO	NNA5698	Feb-12	559640	6690073						309.0	45	264.0		39,047	69,999	3.55								世													
EMP + SHO	AC1192 AC1191	8/07/1984 8/07/1984	559672 559685	6685994 47 6686563 49	5 2,545 25,000 5 3,195 34,500	500	41,890	1 1	7,399 1.4	318.0					133,600 177,200		1		$+$ \Box	22 19	-F		_		<5 <5 <5 <5			-				$\vdash \exists$	- I		+		\dashv
EMP + SHO	NNA5704	Feb-12	559709	6689880						308.2	36	272.2		28,932	52,404	3.50																					ゴ
EMP + SHO	AC1193 RC1194	8/07/1984 8/07/1984			0 3,095 30,500 5 2,595 23,500				10,100 1 8.100 1.5						163,600 127,000			-	+	23.5			-		<5 5 <5 <5							\vdash			+		\dashv
EMP + SHO	AC0891	25/1/1984	560339	6689173 63	6 1,030 11,030	292	17,470	<.6	4,562 4.6	308.2	35.5	272.7			56,400	4.00				16		0.2 4	0		<10												コ
EMP + SHO	RC1329 RC1329	1985 28/10/1985		6694849 71 6694849	0 1,200 12,350	250	21,160	166	3,870 12.3		Composite 65			41,340 51,200	80,000		-		+	<0.05				++	<5 <5			-+	_			\vdash			+		\dashv
EMP + SHO	RC1329	28/10/1985	561251	6694849						349.2	75	274.2		40,768	63,700	6.20									\perp												コ
EMP + SHO	NNA5719 NNA5719	Feb-12 Feb-12		6688171 6688171		-	 			317.8 317.8		269.8 248.8			93,374 127,374		-	1	+	-			-	++					_			1		-	+		\dashv
EMP + SHO	NNA5713	Feb-12	562564	6688343						318.4	42	276.4		35,562	64,134	3.54									\perp												コ
EMP + SHO	NNA5713 NNA5718	Feb-12 Feb-12		6688343 6687990	+ +	+	+		+	318.4 323.3		267.4 254.3			79,434 128,394		+		+	-+	-+	_	-	++	-+			+	-			+ +	-	-	+		\dashv
EMP + SHO	NNA5718	Feb-12	562769	6687990						323.3	78	245.3		76,787	133,834	2.91																					コ
EMP + SHO	NNA5714 NNA5717	Feb-12 Feb-12	562817 563038	6688183 6687833	+ +	+	+ +		+	319.2 326.1		274.2 266.1			77,564 95,074		+		+	-+		_	-	++	-			+	_			+ +	-	-	\rightarrow		\dashv
EMP + SHO	NNA5717	Feb-12	563038	6687833						326.1	60	266.1			96,604	3.45																					コ
EMP + SHO		13/12/1983 Feb-12		6687494 1,0 6688070	20 1,275 12,750	317	22,150	<.6	4,618 1.5	292.0 319.8		268.8		32,672	69,700 58,609		-	 	+	1.6				++	350 <5		-					\vdash			+		\dashv
EMP + SHO		Feb-12		6687367							45				70,207																						ゴ

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		1										Sample	Sample	.1																								
Area	Hole ID	Date Sampled	GDA East	GDA North Ca	a Mg	Na	К	CI	HCO3	SO4 N	103 RL	DEPTH		T.F.R.	TDS	Cond	pН	ORP Hard	Alkalinity	ОН		Al F		Br I	U		Au			_	Cu_Sol Co_					Sr Zn	V_Sol	w
EMP + SHO	NNA5731	Feb-12	563142	mg/ 6686527	/L mg/L	mg/L	mg/L	mg/L	mg/L	mg/L m	ng/L m AH 323					μS/cm 72.707		mV mg/l	mg/l	mg/l	mg/l	mg/l mg/l	mg/l r	mg/l mg/l	ug/l	ug/l i	ug/L	mg/l mg/l	l mg/l	mg/l	mg/l m	g/I mg/	/l mg/l	l mg/l	mg/l	mg/l mg/l	mg/l	mg/l
EMP + SHO	NNA5731	Feb-12		6686527							323.					74,607																						
EMP + SHO	NNA5722 RC0472	Feb-12	563289 563318	6687498 6687355								48		84,930	41,852 84,930		3.39 4.33		1	+			+		<5	<5		+									+	
EMP + SHO	RC0472	5/07/1982	563318	6687355 59	5 2,500			41,610			2.2 317.	,		0.,000	,	127,20	0 4.40				20	0.4			7													
EMP + SHO	RC0472 RC0472	7/01/1982 25/11/1983	563318 563318	6687355 60 6687355 57		27,400 26.600		45,440 44.870			2.2 317. 2.4 317.			1			0 4.00 0 3.80		+	+	2.1 36	0.7	5						-	-		-	-		 		+-+	
EMP + SHO	RC0472	23/10/1984	563318	6687355 65				44,400			11 317.						3.00				21.4																	
EMP + SHO	RC0472	Late 1990-Mid 1991	563318		2 2,871	25,594	506	43,200	12	9,000	317.		247.7		81,839		5.28	167			30	2	4.4	46.4 0.52	<2	C	0.009	0.02	6	0.077	0.013 0.0	11 0.00	1.45	0.07	<0.005	10.1 0.035	<0.002	:0.0015
EMP + SHO	NNA5725 RC0162	Feb-12 18/11/1984	563348 563414	6687218 6687607 79	0 790	18,200	410	31,500	<5	6,150	316. 18 319.		247.7		71,572		7 3.18				18.5		1										-		1		+	
EMP + SHO	RC0162	Late 1990-Mid 1991	563414		7 1,640			27,900		5,410	319.				51,725		5.47	152			55	0.1	14.7 2	22.5 0.3	<2	<	:0.001	0.03		0.002						9.7 0.18	<0.002 <	<0.0015
EMP + SHO	RC0162 WB5-10S	28/02/2013 30/11/1984	563414 563414	6687607 69 6687597 85	0 840 0 850			19,000 28,800		3,900 6,380	319. 24 319.				37,500		3.80	151	+		22.8		+		-			<0.1	<0.005	<0.025	<0.025	<0.1	1	0.05			+-+	
EMP + SHO	WB5-50S	30/11/1984	563414	6687557 64			220	15,300		2,850	50 319.						3.30				24.3																	
EMP + SHO	NNA5727 NNA5727	Feb-12 Feb-12	563439 563439	6687019 6687019							320. 320.				45,172 66,072		7 3.56 7 3.28			+			+						-	1		-	-		 		+-+	$\overline{}$
EMP + SHO	NNA5720	Feb-12	563503	6687552							318.	51	267.5		45,932	81,729	3.43																					
EMP + SHO	RC1343 AC0987	1985 25/11/1983	564471 564600	6708311 6689549 29	4 410	4 275	120	7,313	<.6	1.826	407. 1.3 342.				48,330		7.00			+	1.8				<5	<5									-		+	
EMP + SHO	RC1134	27/3/1984	566215			4,350		7,515			6.6 323.						3.30				160																	
EMP + SHO	RC1131	27/3/1984 Feb 12	566569	6687057 43 6684321	8 358	4,150	123	7,029	1	1,570 2	2.7 328.				E0 070		3.80				11														lacksquare		$\sqcup \Box$	
EMP + SHO	NNA5685 NNA5686	Feb-12 Feb-12	567916		-				 		337. 339.					106,10			+				+ +		— 				-	1			-	-	1		+	
EMP + SHO	NNA5686	Feb-12	567916	6684162							339.	99	240.9		71,972	129,80	7 3.42																				\Box	
EMP + SHO EMP + SHO	NNA5682 NNA5682	Feb-12 Feb-12	567959 567959	6684595 6684595	-	+					334. 334.		250.5 226.5		64,760 76,160	117,089	9 3.27 9 3.29		1	+	 		+ +	-					+	1		-		-	1	-	+-+	
EMP + SHO	NNA5696	Feb-12	568118	6685554							325.	66	259.9		69,380	124,77	6 3.51																					
EMP + SHO	NNA5696 NNA5690	Feb-12 Feb-12	568118 568179	6685554 6684995	-	-			-		325. 334.		247.9 252.0			133,19				1	-		+-+	\dashv						1			-	-	-		+-+	
EMP + SHO	NNA5687	Feb-12	568194	6683993							339.	69	270.1		71,372	128,70	7 3.53																					
EMP + SHO	NNA5683 NNA5683	Feb-12 Feb-12	568236 568236	6684431 6684431							334.	69				137,90				+			-												-		+	
EMP + SHO	NNA5683	Feb-12		6684431								94				134,68																						
EMP + SHO	NNA5683	Feb-12	568236	6684431							334.					131,90																					\longmapsto	
EMP + SHO	NNA5691 NNA5695	Feb-12 Feb-12	568250 568400	6684953 6685387							332. 326.					118,23							1										-		1		+	
EMP + SHO	NNA5662	Jan-12	568448	6684831							331.					132,30																						
EMP + SHO	NNA5662 NNA5663	Jan-12 Jan-12	568448 568576	6684831 6684753							331. 332.					132,80			+	+			+							1		-					++	
EMP + SHO	NNA5663	Jan-12	568576	6684753							332.	93	239.2		77,370	138,37	6 3.05																					
EMP + SHO	NNA5684 NNA5684	Feb-12 Feb-12	568591 568591	6684228 6684228							334. 334.	63				105,40			+	+			+						-	-		-	-		 		+-+	
EMP + SHO	NNA5667	Jan-12	568597	6684605							330.	78	252.2		76,072	137,00	7 3.27																					
EMP + SHO EMP + SHO	NNA5664 NNA5664	Jan-12 Jan-12	568651 568651	6684709 6684709							331.	90				139,65				+			-												-		+	
EMP + SHO	NNA5666	Jan-12	568713	6684811								90				140,67																						
EMP + SHO	NNA5666 NNA5665	Jan-12 Jan-12	568713 568729	6684811 6684664							333. 332.				79,410 73,972	141,52	1 3.28 7 5.45																				\Box	
EMP + SHO	RC1135	25/1/1984	568749	6685177 53	6 1,680	15,550	342	24,990	1	5,200	1.8 330.				73,972) 4.10				8	1.5	20		35										1		+	
EMP + SHO	NNA5688	Feb-12		6684118								48	284.0			75,507																					\Box	
EMP + SHO	NNA5688 NNA5689	Feb-12 Feb-12	568760 569024	6684118 6683961								84				133,40																	-				+-+	
EMP + SHO	NNA5689	Feb-12	569024	6683961							337.	90	247.4		74,972	135,20	7 3.40																					
EMP + SHO	NNA5697 NNA5668	Feb-12 Jan-12	569206 569272	6684206 6684346							341. 337.					133,36				+			+						-	1		-	-		 		+-+	
EMP + SHO	NNA5668	Jan-12	569272	6684346							337.	84	253.8		80,772	145,10	7 3.05																				二寸	
EMP + SHO	NNA5692 NNA5692	Feb-12 Feb-12	569358 569358	6684490 6684490	-	-			-		334. 334.	66			34,240 66,672	63,551 120,60	3.86 7 3.56			1	-		+-+	\dashv						1			-	-	-	_	+-+	
EMP + SHO	NNA5693	Feb-12	569429	6684615							332.	63	269.7		32,740	60,951	4.26																				二	
EMP + SHO	NNA5693 NNA5694	Feb-12 Feb-12	569429 569502	6684615 6684721							332. 331.		248.7 256.8			134,38			1				1	+					-	1		-	-		1	_	\vdash]
EMP + SHO	NNA5694	Feb-12	569502	6684721							331.	84	247.8		72,865	130,64	1 3.67																				二	
EMP + SHO	NNA5670 NNA5670	Feb-12 Feb-12	569567 569567	6684161 6684161						-F	337.	90			53,072	93,034	3.69				$\vdash \vdash$		 	$-\Box$									-		↓		$+$ \Box	
EMP + SHO	NNA5670 NNA5671	Feb-12	569633	6684125							337.					101,53																	1					
EMP + SHO	NNA5671	Feb-12		6684125 6684284							338.	90	248.7			134,34																					\Box	
EMP + SHO	NNA5672 NNA5672	Feb-12 Feb-12		6684284 6684284	-					-	337.	57	268.9	1		44,074 98,389			1		 		+ +	+					+	+		+	+	+	+ +		+	
EMP + SHO	NNA5672	Feb-12	569705	6684284							337.	91	246.9		62,167	109,18	4 3.03																				口	=
EMP + SHO		Feb-12 Feb-12		6684402 6684533	-	+				-+		90				136,12			1	+ -	\vdash		+ +	\dashv					+	1		-		-	+ +	-+	\vdash	
	NNA5675	Feb-12		6684533								90				76,034																					二十	
Year	Bore/Hole	mE	mN	RLGL Samp	oled pH	TDS	CI	Na	К	Ca I	Mg Fe	CO3	HCO3	SO4	NO3	As	Au	B Ba	Be	Br	С	Cd Cr	Cu	Co F	Hg	1 1	Pb	Mo Mn	Ni	S	Sb I S	i Sn	Se	Sr	Th	U Zn	Zr	
Sampled Emperor:				(m AHD) (m		(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L) (m	ng/L) (mg/L) (mg/L)			(mg/L)	(mg/L)	(mg/L)	(mg/L) (mg/L)	(mg/L)	(mg/L)	(mg/L) ((mg/L) (n	ng/L) (mg/L)		(mg/L) (r	mg/L)	(mg/L) (mg/L	.) (mg/L)	(mg/L)	(mg/L) (mg	/L) (mg/L	L) (mg/L	.) (mg/L)		mg/L) (mg/L)	(mg/L)	
2014	NNA6007	558040	6692755							400 1			0				0	0 0		0	0	0				0	0	0	0	0	0 (1	0	0	0 0	0	
2014	NNA6007 NNA6010	558040 558308	6692755	323.91 76 324.06 63	3 4.5	86000	47000	26000	650	530 3	300 0		0		0			0 0			0	0				0		0	0	0	0 (0 0		
2014 2014	NNA6010 NNA6010	558308 558308	6692800	324.06 63 324.06 69	9 4.4	73000	39000	22000	560	530 2	2600 0	+	0	4300 8300				0 0			0	0		+		0					0 0		+			0 0		
2014	NNA6011	558431		325.92 69	4.5	49000	28000	16000	470	660 1	300 0		0	4200	0		0	0 0			0	0				0	0				0 (0 0		
Shogun: 2045	EAAC1015	563503	6685556	337.10 63	3 10			4400	160		200	<1	-6	4500	+	0		-	+	1		0 0				-	0.001		0.089	1		-	-	-	 	0.23	-	

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0 = Below limit of reporting

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Hole ID	Date Sampled	GDA East	GDA North	Ca Mg	Na	к сі	нсоз :	SO4 NO	03 RL	Sample Sar DEPTH F	mple RL T.F.F	R. TDS	TSS Co	pН	ORP P	PO4 Fe	AI F	Si Br	1	U Th	Au As_Sol	B_Sol Ba_	Sol Be_So	ol Cd_S	Sol Cr_Sol	Cs	Cu_Sol	Co_Sol Pb_Sol	Mo_Sol Mn_Sol Ni_Sol Sb_Sol Sn_Sol	Se_Sol	Sr Ti	Y	Zn Zr_Sol V_Sol	W Hg_Sol
RC1351	1985	584431	6685188	760 1,350	13,600	245 22,44		4,455 6.	.1 340.8	87 25	AHD mg/l 3.84	L mg/L 44,670	mg/L μS/c	n 4.35	mV m	mg/l mg/l r <0.05		mg/l mg/l		ug/l ug/l u	ıg/L mg/l	mg/l m	g/l mg/l	mg/	/I mg/I	mg/l	mg/l	mg/l mg/l	mg/l mg/l mg/l mg/l mg/l	mg/l	mg/l mg/l	/I mg/I	mg/l mg/l mg/l	mg/l mg/l
RC1346 RC1330	1985 1985	584985 585325	6685883 6685673	432 725 985 1,700	7,100 17,600	225 11,64 450 30,10	0 6 2 0 32 6	2,665 6. 6,285 8.	1 332.5 6 323.3	87 24 101 22	2.33	24,190 59,710		5.50 7.05		<0.05 <0.05				<5 <5 <5 <5														
RC1347 RC0065	1985 15/05/1980	585662 577282	6676116	980 1,400	11,250	228 19,59	98 2 96 154 4	4,144 7.	.1 322.8	41 28	8.28	26,770		7.00		<0.05 0.25		34.00		<5 <5 6.00 10.00														
RC0471B RC0471B RC0471B	30/06/1981 Jan-82 Mar-82	575160 575160 575160	6680830	415 490	5,730	154 9,62	9 61 2 1 40 2 8 41 2	2,430 <	.1 324.3				31,5	7.10 0 7.00 0 7.00		5.50 2.20 2.50	0.60	22.00																
RC0471B AC1029	25/11/1983 25/11/1983	575160 575486					8 41 2 3 45 2 0 5 1			62.5 26	66.5		32,30 23,30	0 7.40		0.50 0.50				10.00														
RC1030 AC1036	25/11/1983	576390 578005	6681554	378 530	5,225	194 9,017	7 76 2	2,087 1.	0 333.2	65 20	30.2 31.7		46,30	0 6.40 0 7.90		0.25 3.10				<5 <5														
AC1036 AC1036 RC1040	25/11/1983 25/11/1983 25/11/1983	578005 578005 580398	6682047 6682047 6683508	688 950 1,185 1,250	9,100 17,500 6,800	359 16,26 419 22,58 259 12,00	336 3 30 234 3 30 295 4 30 245 3 4 159 2 6 26 1	3,067 2. 4,000 1.	0 346.7 8 346.7	83 26 121 22 64 271	53.7 25.7		68,70	0 7.80 0 7.90 0 8.00		2.00 0.80 0.40				<5 <5 <5														
AC1048 AC0991	25/11/1983 1/12/1983	582366 570324	6685275 6688067	414 540 250 324	5,550	209 9,514 98 4,686	4 159 2 6 26 1	2,444 1. 1.032 0.	6 341.9 9 339.6	56 285 57.5 28	5.903		31,60	0 7.70		0.40	1.70	25.00		45.00														
AC0991 RC0065	1/12/1983 11/04/1984	570324	6676116	800 1,400	11,100	260 19,80	0 89 4	4,150 10	0.0 322.8	82.5 25	0/.1		16,25 52,00	0 7.30 0 6.50		<.1 12.80		140.00		7.00														
AC1232 AC1233	8/7/1984 8/7/1984	579769 580108					00 210 3 00 138 2			32 297 53 278	7.001 37,76 3.931 33,28	60 37,760 80 33,280		0 7.64 0 7.28		0.80 1.50				10.00 6.00 9.00 8.00														
AC1237 RC1279 RC0471B	8/7/1984 Jul-84 24/11/1984	580755 575498 575160	6679995	770 770	11,000	250 19,60	70 257 2 00 10 3 0 45 1	3,850 11	.0 322.3	95 237	7.261 25,28	80 25,280	49,0	0 7.96 0 5.80 0 6.50		0.80 16.20 20.80				6.00 5.00														
RC1351 RC1346	28/10/1985	584431 584985	6685188	490 490	5,200	170 9,220	0 45 1	1,900 8.	340.8	79 26 81 25		31,808 26,368	49,70	0 5.10 0 6.10		20.80																		
RC1346 RC1330			6685883							83 24 89 23	9.52	25,920 38,272	40,50	0 6.20																				
RC1347 RC1440	28/10/1985 26/8/1986	585662 585410	6684608	399 700			60 238 2			41 28 101 2	29 20,54		32,10	0 6.70 0 7.90		<0.05																		
NNA5099 NNA5097 NNA5100	Sep-09 Sep-09 Sep-09	575491 575843 575948	6681879	300 390 320 470 610 850	4,500	150 13,00	0 100 1 00 3 00 170 3	3,200 <0	0.2 330.0	75 25		15,000	1,096,240	0 6.80		0.86 56.00 0.42																		
NNA5102 NNA5094	Sep-09 Sep-09	576088	6681490	510 710 540 860	6,800	220 13,00	00 80 3	3,900 <0	0.2 328.9	64 26 70 26	64.9			0 7.00		<0.4 51.00																		
NNA5198 N5029	11/06/2010 Jul-10	575539 575965	6682048 6681554		7			0.	329.0 329.0	50 27 50 27			21,50 19,40	0					Ш															
N5030 N5040 N5041	Aug-10 21/12/2010	575544 580034	6682734						326.2 332.1	44 288	3.118		19,90 43,60	0	$=$ \blacksquare				LΤ															
N5041 NNA5529 NNA5529	21/12/2010 1/12/2011 1/12/2011	580092 570045 570045							331.6 343.2 343.2	72 27	71.2	58,372 66,172		0 07 3.57 07 2.57																				
NNA5528 NNA5530	40878 Dec-11	570226 570341	6681372 6681754						339.0 346.2	65 27 73 27	74.0	54,160 51,672	99,00 94,10	9 3.77 7 3.38																				
NNA5530 NNA5520	1/12/2011 Dec-11	570341 570404	6681754 6682215						346.2 338.7	114 23 87 25	32.2 51.7	74,372 60,625	133,7 109,3	07 2.84 91 3.05																				
NNA5520 NNA5542	1/12/2011 Dec-11		6682644						338.7 333.7	87 25 72 26	61.7	60,370 59,372	107,7	36 4.21 07 2.94																				
NNA5535 NNA5538 NNA5538	1/12/2011 1/12/2011 1/12/2011	570464 570482 570482	6682151							63 27 63 27 90 25	78.6	49,260 64,172 69,372	116,4	9 4.02 07 3.42 07 3.04																				
NNA5538 NNA5537	1/12/2011 40878		6682151						341.6	108 23 54 28	33.6	77,572 31,740	139,5	07 2.82																				
NNA5537 NNA5524	Dec-11 Dec-11		6681178						337.4 346.9	87 25 87 25	50.4 59.9	65,833 61,390	110,8	35 2.70 36 3.46																				
NNA5524 NNA5519	1/12/2011	570616							346.9 335.9 337.5	106 24		71,080 64,705	116,3	36 3.13 61 3.33																				
NNA5531 NNA5531 NNA5531	1/12/2011 1/12/2011 1/12/2011	570663 570663							337.5 337.5 337.5			21,360 21,560 42,060	40,41	9 5.06 9 4.42 9 3.98																				
NNA5531 NNA5518	1/12/2011 1/12/2011	570663 570670	6682093 6682280						337.5 334.8	90 24 81 25	17.5	66,540 66,830	120,3 120,1	51 3.14 36 3.30																				
NNA5522 NNA5522	1/12/2011 1/12/2011	570677 570677	6681559 6681559						343.2 343.2	110 23	33.2	68,530 73,160	123,2 131,7	46 3.40 39 3.18																				
NNA5539 NNA5526 NNA5526	1/12/2011	570716 570766	6681060						336.2 348.8 348.8	87 24 78 27 87 26	19.2 70.8	65,772 50,960 58,060	119,0 93,18	07 3.33 9 4.58 89 3.18																				
NNA5536 NNA5536	1/12/2011 1/12/2011 1/12/2011		6681060 6682462 6682462							66 26 84 24	65.0	54,940 64,960	99,8	3.28 39 3.43																				
NNA5523 NNA5532	1/12/2011	570808 570869	6681472						346.5 336.6	? 60 27	76.6	69,890 48,460	125,2	36 3.22 9 4.29																				
NNA5532 NNA5543	1/12/2011 1/12/2011		6682801						336.6 330.8	78 25 69 26	61.8	58,060 56,472	102,9	39 2.92 07 3.11																				
NNA5543 NNA5533 NNA5533	1/12/2011 1/12/2011 1/12/2011	570953 571012								78 25 60 27 75 25	73.9	53,972 48,360 51,840	88,5	7 3.39 9 3.15 1 3.21																				
NNA5527 NNA5527	1/12/2011 1/12/2011 1/12/2011	571110 571110								73 27	71.7	53,072 57,772	96,80	7 3.49																				
NNA5534 NNA5544	1/12/2011 1/12/2011	571128 571189	6681767						336.0		35.0	30,360 44,272	56,68	9 3.63 7 2.69																				
NNA5544 NNA5544	1/12/2011	571189 571189	6683192						328.2	81 24 81 24	17.2	46,672 45,972	84,40	7 3.93																				
NNA5545 NNA5545 NNA5556	1/12/2011 1/12/2011 1/12/11	571431	6683581 6683581 6684129						327.2 327.2 340.0	69 25 75 25 51 28	52.2	43,933 38,133 16,572	70,53	5 5.33 5 3.32 7 5.24																				
NNA5556 NNA5551	1/12/2011 Dec-11		6684129						340.0 339.6	51 28	39.0	16,072 19,033	30,60	7 5.88 5 6.41																				
NNA5551 NNA5551	Dec-11 Dec-11	578602 578602	6684253 6684253						339.6 339.6	57 28 57 28	32.6 32.6	19,533 19,433	37,13 36,83	5 4.14 5 4.09																				
NNA5552 NNA5552	Dec-11 Dec-11	578732							340.6 340.6	57 28 57 28	33.6 33.6	18,833 18,933	36,03	5 4.27																				
NNA5549 NNA5549 NNA5553	Dec-11 Dec-11 Dec-11	578793 578793 578833							339.9 339.9 339.8	45 29	32.9 34.8	20,072 19,472 20,333	36,9	7 5.99 7 5.48 5 4.25																				
NNA5561 NNA5561	Dec-11 Dec-11	578951 578951	6683851 6683851						340.2 340.2	54 28 54 28	36.2 36.2	19,433 18,933	36,73 35,83	5 5.72 5 5.65																				
NNA5554 NNA5554	Dec-11 Dec-11		6684070						340.5 340.5	57 28 57 28	33.5	18,333 17,433	33,3	5 6.11 5 6.18	$=$ \blacksquare				H															
NNA5547 NNA5563 NNA5563	Dec-11 Dec-11 Dec-11	579046 579093 579093							340.8	54 28 60 28 60 28	30.8	20,533 19,733 21,033	37,73	5 4.25 5 6.07 5 5.56																				
NNA5555 NNA5555	1/12/11 1/12/11		6683986						339.6	54 285 60 279	5.606	20,333 16,033	38,63	5 5.76 5 5.98																				
NNA5555 NNA5575	1/12/11 1/12/11	579115 579273	6683986 6684398						339.6 340.8	60 279 54 286	9.606 3.773	15,133 19,753	29,23 37,4	5 4.92 1 5.35					Ш															
NNA5575 NNA5568 NNA5568	1/12/11 1/12/11	579273 579285 579285	6684138						342.7		2.697	19,653 20,833	39,63	1 4.77 5 4.99																				
NNA5568 NNA5568 NNA5577	1/12/11 1/12/11 1/12/11	579285	6684138 6684138 6684344						342.7 342.7 341.1	66 276 66 276 57 284	6.697	18,933 18,833 21,672	35,83	5 5.33 5 5.98 7 6.05																				
NNA5577 NNA5577	1/12/11 1/12/11 1/12/11		6684344							66 275 66 275	5.143	23,153 22,153	43,47	1 6.72																				
NNA5574 NNA5574	1/12/11 1/12/11	579417 579417	6684305 6684305						342.6 342.6	75 267 75 267	7.626 7.626	22,253 23,853	42,01 44,91	1 6.69																				
NNA5571 NNA5571 NNA5514	1/12/11 1/12/11 1/12/11	579487 579487 579499							347.4 347.4 349.9	66 281 66 281 74 27	1.382	17,633 17,333 21,355	33,53 33,13	5 4.24 5 4.51 6 7.12																				
NNA5514 NNA5515 NNA5516	1/12/11 1/12/11 1/12/11	579569							349.9 350.1 350.2	80 270 70 280	0.118	21,355 24,245 21,865	45,30	6 7.12 11 7.54 16 6.92																				
NNA5581 NNA5581	1/12/11 1/12/11	579670 579670	6684634 6684634						340.0 340.0	54 285 60 279	5.967 9.967	20,253 19,053	38,41 36,11	1 5.58																				
NNA5581 NNA5578	1/12/11 1/12/11	579670 579728	6684603							60 279 57 282	9.967	19,653 21,453	40,4	1 5.61 1 5.92																				
NNA5580 NNA5580	1/12/11 1/12/11		6684554						339.0 339.0	E4 00-	7 902	20,353 21,053	40,07	1 6.25																				
NNA5582 NNA5582 NNA5582	1/12/11 1/12/11 1/12/11		6684689 6684689 6684689							54 287 63 278 63 278	3.893 3.893	23,972 21,072 20,272	39,9i 38,5i	7 4.21 7 5.30 7 6.32																				
NNA5584 NNA5599	1/12/11 1/12/11 1/01/2012	580030 578560	6684657 6684084						341.9 340.3	57 284	1.946	20,772	39,20 36,60	7 6.51 9 4.78																				
NNA5599 NNA5609	1/01/2012 Jan-12	578560 578619	6684084 6684166						340.3 340.8	54 28		18,960 18,960	36,00 35,90	9 4.62 9 3.95																				
NNA5609 NNA5649	Jan-12 Jan-12		6683654							54 28 51 29	90.2	19,360 15,150	28,98	9 3.89					H											$oxed{\Box}$	#			
NNA5649	Jan-12	578708	6683654						341.2	51 29	30.2	15,830	30,0	1 4.89					1											1	1			

Hole ID [Date Sampled	GDA East	GDA North	Ca Mg Na	к	сі нс	O3 SO4	NO3	RL Sam	nple Sample	e T.F.R.	TDS TSS	Co p	oH OR	P PO4 Fe Al	F Si Br	ı u	Th Au	As_Sol B_Sol	Ba_Sol Be_	_Sol Cd_Sol	Cr_Sol	Cs Cu	_Sol Co_Sol	Pb_Sol	Mo_Sol Mn_So	l Ni_Sol	Sb_Sol	Sn_Sol Se_Sol	Sr Ti	Y Zn Zr_So	V_Sol	W Hg_Sc
NNA5602	Jan-12	578724	6683756	mg/L mg/L mg/L	L mg/L	mg/L mg	g/L mg/L	mg/L m	AHD n	m AHE 4 288.3		mg/L mg/L 0.460	μS/cm 20,289 5	.83	V mg/l mg/l mg/l r	ng/l mg/l mg						mg/l				mg/l mg/l			mg/l mg/l		mg/l mg/l mg/l	mg/l	mg/l mg/l
NNA5644 NNA5644	Jan-12 Jan-12	578770						3	43.3 5	4 289.3 4 289.3	1	9,572 0,272	37,207 5 38,507 6	.39																		1	
NNA5623 NNA5623	Jan-12 Jan-12		6684324 6684324					3	40.6 40.6 4	8 292.6	1	6,960	117,007 2 32,289 5																			1	
NNA5623 NNA5622	Jan-12 Jan-12	578834	6684324 6684277					3	43.7 5	8 292.6 4 289.7	2	7,360 0,160	32,889 5 38,089 3	.64																		$\pm \pm \pm$	
NNA5645 NNA5645	Jan-12 1/01/2012	578912	6683522 6683522					3	39.2 5	4 285.2 4 285.2	. 2	2,715 0,172	42,666 5 38,107 5	.83																		$\pm \pm \pm$	
NNA5605 NNA5605 NNA5614	Jan-12 Jan-12		6683653					3	40.1 5 40.1 5 39.8 5	4 286.1 4 286.1	1	6,360 6,360	31,389 6 31,289 6 37,689 5	.02																		$\pm \pm \pm$	
NNA5614 NNA5614 NNA5606	Jan-12 Jan-12 Jan-12		6683963 6683963 6683585					3	39.8 5	5 284.8 5 284.8 4 284.0	1	9,760 9,760 0,660	37,689 5 37,789 4 39,089 3	.63																		##	
NNA5646 NNA5646	Jan-12 Jan-12 Jan-12	578983						3	40.1 5	7 283.1 6 274.1	2	2,970	42,751 3 40,051 4	.98																		$\pm \pm \pm$	
NNA5646 NNA5641	Jan-12 Jan-12 Jan-12	578983	6683486 6683723					3	40.1 6	6 274.1 7 285.5	2	10,340	38,651 4 41,051 5	.25																		###	
NNA5641 NNA5642	Jan-12 Jan-12	579005	6683723 6683671					3	42.5 5	7 285.5 1 288.2	1	1,750	22,691 5 40,626 5	.64																		1	
NNA5642 NNA5642	Jan-12 Jan-12		6683671 6683671					3	39.2 5	1 288.2 3 276.2	. 2	2,040	39,207 5 41,351 5	.50																		1	
NNA5642 NNA5616	Jan-12 Jan-12	579062 579105	6683671 6683886					3	39.2 6 35.6 4	3 276.2 8 287.6	2	1,572 0,860	40,807 5 39,589 5	.75																		1	
NNA5616 NNA5634	1/01/12 1/01/12	579135	6683886 6684302					3	35.6 4 42.1 5	8 287.56 1 291.10 1 291.10	7 2	0,660 8,775	39,089 5 16,996 6	.29																			
NNA5634 NNA5617	1/01/12 1/01/12	579177	6684302 6683836					3	33.6 5	1 291.10 1 282.59	1 2	8,740 0,960	17,051 6 39,589 5	.88																			
NNA5617 NNA5625	1/01/12 1/01/12	579251	6683836 6684020					3		4 286.23	1 2	0,760 0,260	39,289 5 38,389 5	.66																		$\pm \pm \pm$	
NNA5625 NNA5632	1/01/12 1/01/12	579278	6684020 6684251					3	39.7 5	4 286.23 7 282.68 7 282.68	6 1	9,400	39,089 5 36,631 6	.21																			
NNA5632 NNA5626 NNA5627	1/01/12 1/01/12 1/01/12	579317	6684251 6683995					3	38.1 5	4 284.06	9 1	9,360 0.460	39,096 6 36,589 5	.10																		##	
NNA5627 NNA5627 NNA5630	1/01/12 1/01/12 1/01/12	579383	6683961 6683961 6684166						35.3 4 35.3 4 42.7 5	8 287.29 8 287.29 7 285.67	1 2	0,160 0,160 0,060	38,089 6 38,489 6 38,089 5	.20																		##	#
NNA5630 NNA5636	1/01/12 1/01/12 1/01/12	579451	6684166 6684253					3	42.7 6 45.5 5	7 288.53 7 288.53	5 2	1,360	40,389 5 40,351 5	.64																		##	
NNA5636 NNA5661	1/01/12 1/01/12 1/01/12	579487						3	45.5 7	2 273.53 8 268.64	1 1	9,400	36,461 6 42,241 6	.22																		##	=
NNA5661 NNA5591	1/01/12 1/01/12	579491	6684365 6684520					3	46.6 7	8 268.64 4 284.99	7 2	1,040	40,051 6 39,889 6	.65																		<u>+</u> +	
NNA5591 NNA5592	1/01/12 1/01/12	579874 579930	6684520 6684477					3	39.0 5 39.3 4	4 284.99 8 291.30	6 1 5 1	9,760 9,553	37,789 6 37,171 6	i.48 i.97																		$\pm \pm$	
NNA5592 NNA5589	1/01/12 1/01/12	580088	6684477 6684614					3	41.3 6	8 291.30 0 281.32	1 2	9,660 0,860	37,289 7 39,589 6	.40																			
NNA5589 NNA5589 NNA5587	1/01/12 1/01/12 1/01/12	580088	6684614 6684614					3	41.3 6 41.3 6	6 275.32 6 275.32	1 2	0,760 0,860	39,089 6 39,589 6	.44																		$\pm \pm \pm$	
NNA5678	1/02/12	570296	6684654 6683748					3	38.0 4 29.3 4	8 290.00 8 281.3	1 1	9,360 8,172	36,889 4 105,907 3	.12																		$\pm \pm \pm$	
NNA5678 NNA5677 NNA5677	1/02/2012	570367						3	34.9 7	8 281.3 4 245.3 1 263.9	6	2,372 1,972	130,607 3 112,307 3	.31																		##	
NNA5676 NNA5676	1/02/2012 Feb-12 1/02/2012		6683889 6684009 6684009					3	29.3	9 245.9	8	3,982 10,102 17,692	129,159 3 139,444 3 118,279 3	.03																		$\pm \pm \pm$	
NNA5679 NNA5679	1/02/2012 1/02/2012 1/02/2012	570969								7 242.3 1 264.5 1 264.5		4,372 5,872	99,107 3 101,707 3	.01																		1 1	
NNA5680 NNA5680	1/02/2012 1/02/2012	571080	6683498 6683498					3	25.8 6	4 261.8		8,660 7,660	106,589 3 105,189 3	.25																		1	
NNA5681 NNA5681	1/02/2012 1/02/2012	571201 571201	6683712 6683712					3	29.0 5 29.0 6	4 261.8 1 278.0 9 260.0	1 5	9,760 17,460	37,789 4 104,489 4	.36																		1	
NNA5737 NNA5737	1/02/2012 Feb-12	578015	6682529 6682529					3	39.0 5 39.0 8	7 282.0 1 258.0	1 3	3,872 1,072	45,107 5 57,907 5	.94																			
NNA5738 NNA5755	Feb-12 Feb-12	578625	6682413 6683929					3	45.1 6 42.4 4	0 285.1 8 294.4	. 1	9,772	43,907 5 37,207 4	.21																			
NNA5734 NNA5733	Feb-12 1/02/12	579141	6683078 6683046					3	50.1 9	9 281.1 0 260.07	7 2	0,072 4,872	37,907 4 46,707 7	.10																		$\pm \pm \pm$	
NNA5733 NNA5748	1/02/12 1/02/12		6683733					3	40.4 5	0 260.07 7 283.35	8 2	3,872 1,372	45,007 6 40,107 6	.08																			
NNA5748 NNA5749 NNA5746	1/02/12 1/02/12 1/02/12	579238	6683733 6683679 6683890					3	34.4 4	5 265.35 2 292.38	7 1	2,072 8,472	42,007 6 35,207 6	.22																		$\pm \pm \pm$	
NNA5740 NNA5757	1/02/12 1/02/12 Mar-12	579643	6684560 6682852					3	40.5 5	1 282.45 1 289.45 2 295.5	3 2	9,672 11,072 9,472	37,307 5 39,907 5 36,907 6	.67																		##	
NNA5757 NNA5762	Mar-12 1/03/12	578852	6682852 6683797					3	37.5 7	8 259.5	. 2	9,372	40,407 5 36,707 7	.69																		1	
NNA5760 NNA5769	1/03/12 1/03/12 1/03/12	579311	6683763 6683730					3	33.9 4	5 287.83 8 285.94 0 274.25	3 1	8,972 3,372	36,107 4 25,707 6	.68																		1	
NNA5768 NNA5767	1/03/12 1/03/12		6683676					3	34.8 3	9 295.82 6 271.23	1 1	4,372 4,572	27,507 4 27,907 5	.02																		1	
RC1279 RC1279	26/02/2013 26/02/2013	575498 575498	6679995 6679995	610 1,000 9,40	0 250	16,000 2	1 3,300	3	22.3 3	5 287.3	3	3,400 11,000	62,100 6 43,000 6	.40 46	6				<0.1		<0.005	<0.025	<0	0.025	<0.1		0.07					1	
N5030	26/02/2013 Feb-13	575544	6681137 6681137	220 320 4,50	0 190	6,600 8	3 1,300	3	26.2 26.2		1	1,600 2,100	20,600 5 20,000 5	.90 -13	35				<0.02		0.00	<0.005	<0	0.005	<0.02		0.01					1	
N5034	26/02/2013 26/02/2013	576399		300 480 4,90				3	32.3 32.3		1	4,550 5,400	25,400 6 24,000 6	.60 -20	05				<0.02			<0.005		0.005	<0.02		0.03						
N5032	27/02/2013 Feb-13	578632	6682382	170 230 3,30 260 450 3,70	0 240	6,300 15	1,600	3	32.9		1	9,660 2,700 0,500	16,000 6 20,000 6	.90 -24	18				<0.02 <0.02		< 0.001	<0.005	<0	0.005	<0.02		0.01					$\pm \pm \pm$	
N5038 N5040	27/02/13 27/02/13			250 390 3,40 15 19 190				3	38.3			723	17,000 8 1,300 6	.00 -36	19				0.03 <0.02		< 0.001	<0.005	0	0.005	<0.02		0.05					$\pm \pm \pm$	
NNA5508 RC0065	Feb-13 Feb-13	577282	6676116 667000E	260 310 4,50 400 2,400 24,00 554 1,007 9,42 704 1,248 11,20	0 740	38,000 <	5 5,600	3	24.3 22.8 22.3		7	3,700 5,200 11,510	21,000 7 91,000 4	.10 25	4	12.50 18.0	0 0 26 -2		<0.02 <0.1	0.03	<0.001	0.01 <0.025 <0.002	-0	0.005 0.025 0.004 <0.005	<0.02 0.65	1.20	0.02 0.07 0.01			8.70	0.01	<0.002 <	-0.0015
RC1279 Lat RC1213 Lat	te 1990-Mid 1991 te 1990-Mid 1991	575498 575684	6679995 6681498	704 1,248 11,20 246 350 3,76	02 231	20,800 7	1 3,880	3	22.3		3	8,144 2,506	6	.30 12: .22 12:	5 23.00 <0.1 8 0.46 <0.1	7.90 20.0 21.00 10.6	0 0.52 <2	<0.001 0.01		0.02		0.002	0.	0.004 <0.005 0.01 <0.005 0.03 <0.005	0.00	1.36	0.01 0.01	0.01			0.01	<0.002 < <0.002 < <0.002 <	<0.0015
RC1148 Lat	te 1990-Mid 1991	576004	6680326	532 742 6,80 450 700 5,64	0 248	11,800 8	6 2,490	3	25.3		2	2,678 9,522	5	.98 129	9 0.40 <0.1	21.00 23.1	0 0.64 <2	0.40 < 0.001		0.03		<0.002 <0.002	0	0.00 <0.005 0.00 0.01	0.00	0.20 0.13	0.01	<0.005	=	6.90 6.30 0.00	0.01	<0.002 <	<0.0015
RC1151 Lat	te 1990-Mid 1991	576375	6681103	319 467 4,39 316 850 7,93	2 169	7,810 10	1,560	3	26.0		1	4,784 5,324	6	.36 14	4 0.88 < 0.1	15.40 15.0	0 0.36 <2	<0.001 <0.001 <0.001		0.02		<0.002		0.01	0.00	0.24	0.02	0.01		4.00 5.80	0.01	0.00 <	<0.0015
CD1366 Lat	te 1990-Mid 1991	577430	6682621	461 290 2.27	1 84	4.210	1.140	3	38.3			3,461	6	.46 80	0.34 < 0.1	4.60 4.9	0.15			0.16 0.05		<0.002	<0	0.001 0.01 0.38 0.05	0.01	0.32 0.28	0.02	0.01	\equiv	2.20	0.05	<0.002 <	
RC1216 Lat CD1409 Lat	te 1990-Mid 1991 te 1990-Mid 1991	578630 578711	6683116 6682585	683 754 8,23 515 681 7,71 174 262 2,28	7 249 5 66	13,400 33 4,070 1,2	39 2,630 231 56	3	39.3 34.6			7,343 5,376 7,519	6	.45 9 .58 -16	1 0.00 7.80 <0.1 0.19 5.10 <0.1 67 4.89 0.22 <0.1	1.60 13.0 2.90 3.3	0 0.77 <2 0 0.32 <2	<0.001 <0.1 <0.001		0.02		0.00	0.00 <0	0.001 <0.005 0.001 0.01	0.01	0.17	<0.01	<0.005		1.70 :0.000	<0.01 <0.005 0.00 <0.005	<0.002 < <0.002	< 0.0011
CD1515 Lat CD1247 Lat	te 1990-Mid 1991 te 1990-Mid 1991	579398 579947	6682663 6682973	708 1,212 11,27 626 856 7,93 858 1,176 9,64	78 250 9 308	19,000 0 14,000 38	3,520 32 2,950	3	33.7 29.8		2	5,984 6,887	7	.27 14	7 0.49 0.18 <0.1 3 0.00 0.19 <0.1 5 0.01 0.00 <0.1	2.80 14.7 4.60 20.4	0 0.45	0 0.40 <0.001		0.05 0.03 0.05		0.00	<0	0.001 <0.005 0.01 0.01 0.001 0.02	0.01	1.34	0.04 0.02 0.04			7.90 5.10 0.00 (0.28	<0.002	0.00
CD1500 Lat	te 1990-Mid 1991	583088	6684326	415 651 5,27	6 207	9,820 10	07 2,020	3	30.5 28.0 32.6		1	2,875 8,459 4,535	6	.01 293	3 0.02 1.02 <0.1	4.00 16.6	0.32 <2	0.20 0.01		0.05 0.02 0.04		<0.002 <0.002	0.01 0	0.01	0.02	0.27	0.08	0.01		4.10 0.00	0.19	<0.002	0.00
NNA5027	ite 1990-Mid 1991	570336	6688064	300 522 4,18 197 301 3,03	8 101	7,430 28 5,311 <	5 1,355	0.4 3	36.5 8	2 254.5	. 1	0,668	17,780 4		3 0.10 6.30 <0.1 0.84	6.30 20.3	<5		<0.005 1.25		.005 <0.0005	<0.002	U.U1 0	0.01 0.01 0.03 0.08	0.02	<0.005 <0.005 3.21	0.02	<0.005	<0.005 <0.005	3.40 0.00	0.00 0.09	<0.002 <0.005	
RC0471B RC0324 AC1226		575161						3	24.3		20,420 2 13,260 1	8,900		.10			9.00															##	
AC1226 NNA5140 RC1279		575384	6681710 6680444 6679995	357 422 4,89 651 1.171 10.81	8 171	8,689 9	1,751	< 0.2	24.3 5		19,780 1	9,780 6,452 4,620	27,420 6 57,700 6	i.03 i.40	<0.2		<5 <5 <10	<5	<0.005 1.21	0.07 <0.	.005 0.00	<0.005	0	0.02 0.15	0.01	0.04 0.53	0.18	<0.005	<0.005 <0.005		0.16 0.16 0.09 0.09	0.01	<0.000
NNA5393 NNA5127		E7EE24	6601110	651 1,171 10,81 416 548 5,74 463 531 5,71	0 107	40.022 4	0 2227	-02 2	260 6	3 254.8	1	8,720 8.840	31,200 4 31,400 5	.20	<0.2 6.53 0.20		28.00 32.00	01 1 1	<0.01 0.85 <0.005 1.61 <0.005 1.41	0.06 <0.	.005 0.02	< 0.005	0	0.63	< 0.005	0.01 1.25	0.63	< 0.005	<0.01 <0.01 <0.005 <0.005 <0.005 0.01		3.25 3.25 0.27 0.27	<0.005	<0.00 <0.00 <0.00
NNA5127 NNA5198 NNA5155		575539 575805	6682048 6680453	274 336 4,11 362 488 5,08 620 834 8,13	6 128	7,558 < 9.677 3	5 1,633 1 1.827	<0.2 3	29.0 6	4 265.0 1 274.5	1	3,836 7,034	23,060 3 28,390 6	.50	50.81		<5 <5 68.00	-	<0.005 1.41 <0.005 1.01 <0.005 1.35 <0.01 1.69	0.05 0. 0.05 <0	.02 0.00	<0.005	0	0.02 0.72	0.04	<0.005 1.37 0.01 0.56	1.15	<0.005	<0.005 0.01 <0.005 0.01 <0.005 <0.005 <0.01 <0.01		6.65 6.65 0.07 0.07	<0.005	<0.000 <0.000
NNA5107 NNA5103		576153	6681450	580 772 7.60	2 257	13.693 <	5 2.875	< 0.2	28.9 6	6 262.9	2	7,034 16,820 15,020	44,700 4 41,700 4	.80	<0.2 <0.2 0.76		68.00	0	< 0.01 1.72	0.07 <0	0.01	0.01	1 0	.90 2.29 0.63 3.96	3.08	<0.01 2.35 <0.01 1.61	2.91	<0.01	<0.003		12.89 12.89 5.26 5.26	<0.01 <0.01	<0.000
NNA5199		578636	6682399	614 833 8,19 604 900 8,65	7 316	16,462 <	5 3,273	<0.2 3	36.1 5	5 281.1 5 264.79	2	7,000 8,680	45,000 4 47,800 6	.20	5.89 <0.2		<10 <10)	<0.01 2.13 <0.01 2.71	0.09 <0	0.001	< 0.01	0	0.02 0.65	< 0.01	<0.01 1.30 <0.01 1.96	1.72	<0.01	<0.01 <0.01 <0.01 <0.01		7.78 7.78 0.92 0.92	< 0.01	<0.000
NNA5086 AC1232		579150										0,210						0 <5															

I/345-0/Reports/13-001

APPENDIX II-bi Ambassador and Princess Raw Water Chemistry Data Rare Earths

Hole ID	Date Sampled	GDA East	GDA North	La	Се	Pr	Nd	Sm	Eu	Gd	Tb	Dy	Но	Er	Tm	Yb	Lu	REE (Total)	δ18Ο	δ2Η
				mg/l	(SMOW)	(SMOW)														
RC1213	Late 1990-Mid 1991	575684	6681498	nd	-3.18	-26.4														
RC1148	Late 1990-Mid 1991	576004	6680326	nd	nd	nd														
RC1152	Late 1990-Mid 1991	576022	6681299	0.0022	0.0038	0.0006	0.0029	0.0008	0.0002	0.0008	0.0001	0.0005	0.0003	0.0005	0.0001	0.0005	0.0001	0.0134	nd	nd
CD1366	Late 1990-Mid 1991	577430	6682621	nd	-2.08	-14														
RC1177	Late 1990-Mid 1991	578272	6682855	nd	-3.47	-32.6														
RC1216	Late 1990-Mid 1991	578630	6683116	nd	-3.59	-32.2														
CD1409	Late 1990-Mid 1991	578711	6682585	0.0011	0.0009	0.0002	0.0008	0.0008	0.0003	0.0007	0.0001	0.0004	0.0001	0.0004	0.0001	0.0006	0.0001	0.0066	-3.5	-24

1

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Year Bore/Hole mE mN	RLGL S	ampled pH	TDS	CI	Na	K	Ca	Mg	Fe	CO3	HCO3	SO4	NO3	As	s Au	В	Ba	Be	Br	C	Cd	Cr (mg/L) (Cu	0	F	Hg	- 1	Pb	Mo	Mn	Ni	S	Sb	Si	Sn	Se	Sr	Th	U	Zn	Zr
Sampled	(m AHD)	(m)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	Mg (mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg	g/L) (mg/	L) (mg/L) (mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L) ((mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)	(mg/L)
2014 NGW27 574421 6671852	335.96	72 4.7		24000	14000	410	470	1500		0	0	4700																						i '	į ,	ı		1		1	
2014 NGW27 574421 6671852	335.96	75 4.6	49000	27000	16000	450	360	1700		0	0	4900																						ſ '		1			1		
2014 NGW27 574421 6671852	335.96	78 4.9	43000	23000	14000	400	460	1500		0	0	4400																							1	i		1	,	1	
2014 NGW27 574421 6671852	335.96	88 4.6	62000	33000	20000	560	470	2200		0	0	6500																							1	i		1	,	1	
2014 NGW28 575534 6671172	328.41	51 4.9	33000	18000	11000	350	510	1200		0	0	3500																							1	i		1	,	1	
2014 NGW28 575534 6671172		69 4.5	44000	24000	15000	410	450	1600		0	0	4900																							1	i		1	,	1	
2014 NGW28 575534 6671172	328.41	90 4.7	70000	41000	24000	610	460	2400		0	0	7200																							1	i		1	,	T .	
2014 NGW29 574546 6670455	326.59	58 4.7	34000	21000	12000	380	470	1300		0	0	3900																							1	i		1	,	T .	
2014 NGW29 574546 6670455	326.59	71 4.8	52000	32000	18000	520	430	1900		0	0	6000																						í '	ĺ			1		,	
2014 NGW29 574546 6670455	326.59	84 4.7	66000	37000	23000	610	440	2400		0	0	6900																						í '	ĺ			1		,	
2014 NGW30 575351 6670159	346.15	75 5.2	30000	18000	10000	330	460	1100		0	0	3700																						í '	ĺ			1		,	
2014 NGW30 575351 6670159	346.15	87 5.0	49000	31000	18000	430	440	1800		0	0	6000																						ſ '					,		
2014 NGW30 575351 6670159	346.15	98 4.8	64000	36000	22000	510	430	2200		0	0	7100																						ſ '					,		
2014 NGW30 575351 6670159	346.15	111 4.5	71000	36000	23000	510	450	2400		0	0	7200																						ſ '					,		
2014 NGW31 575010 6668792	339.73	66 4.7	37000	21000	13000	360	470	1300		0	0	4100																							1	i		1	,	1	
2014 NGW31 575010 6668792	339.73	81 4.8	49000	28000	18000	470	450	1800		0	0	5700																							1	i		1	,	1	
2014 NGW31 575010 6668792	339.73	96 5.1		38000		600	470	2400		0	0	7100																							1	i		1	,	1	
2014 NGW32 574523 6668776	332.87	5.6	39000	22000	13000	370	520	1200	0		6	3900	0			4.2	0.029					0.025	0.025			0.00013		0		0.93	0.11		0		0	0		0	0	0.24	
2014 NGW33 576626 6670522	332.87	6.5	29000			230	480	890	0		35	3400	0			5.1	0.051					0.025	0.041					0		1	0.18		0		0	0		0	0	2.4	
2014 NGW34 576791 6671217		6.9				230	460	840	0		99	3300	0			4.9	0.05					0.027						0		1.6	0.069		0	i '	0	0		0	0	0.26	
2014 NGW35 573179 6666413			31000			250	420	890	0		0	3400	0	0.0	26	4.8	0.03					0	0.052			0.00093		0		0.31	0.075		0	i '	0	0		0	0	0.48	
2014 NGW36 571529 6667012	343.13	4.9		24000	13000	400	470	1200	0		0	4000	0			4.3	0.026					0						0		0.61	0.038		0	i '	0	0		0	0	0.16	
2014 NGW37 575553 6671112	330.21	64 5.5	48000	26000	15000	420	500	1600	0		0	5700	0				0.065																	i '	į ,	ı		1		1	
2014 NGW37 575553 6671112	330.21	73 4.8	57000	30000	17000	480	540	1800	0		0	6300	0				0																	i '	į ,	ı		1		1	
2014 NGW37 575553 6671112		93 4.6				570	460	2300	0		0	8000	0				0																	i'	[
2014 NGW54 575554 6671245		80 5.3	52000			450	380	1700			0	6000																						i'	[
2014 NGW54 575554 6671245	327.20	110 4.5	70000	37000	21000	550	470	2200			0	7900																						L'	<u> </u>	1		I		<u> </u>	
2014 NGW54B 575555 6671244	327.20	54 4.1	62000	34000	20000	540	450	2100	0		0	7500	0				0																	L'	<u> </u>	1		I		<u> </u>	
2014 NGW54B 575555 6671244	327.20	84 4.2	36000	20000	11000	340	500	1100	0		0	4400	0				0																	L'	<u> </u>	1		I		<u> </u>	
2014 NGW54C 575552 6671246		63 5.0	49000		15000	400	490	1600	0		0	4800	0		0	0	0		0	0		0					0	0		0	0	0	0	0	[0	0	0	0	0
2014 NGW54C 575552 6671246	327.23	78 4.7	68000	34000	22000	560	470	2200	0		0	6000	0		0	0	0		0	0		0					0	0		0	0	0	0	0	1 7	1 1	0	0	0	0	0
2014 NGW54C 575552 6671246	327.23	93 4.7	73000	39000	23000	610	470	2400	0		0	6700	0		0	0	0		0	0		0					0	0		0	0	0	0	0	1	i I	0	0	0	0	0
2014 NGW55 575360 6670233	345.80	78 4.8				210	260	590	0		0	2100	0		0	0	0		0	0		0					0	0		0	0	0	0	0	1	i I	0	0	0	0	0
2014 NGW55 575360 6670233	345.80	100 4.5		35000		540	430	2000	0		0	6000	0		0	0	0		0	0		0					0	0		0	0	0	0	0	[i I	0	0	0	0	0
2014 NGW55 575360 6670233	345.80	114 4.6	68000	36000	21000	570	460	2200	0		0	6300	0		0	0	0		0	0		0					0	0		0	0	0	0	0	[i I	0	0	0	0	0
2015 NWB01 575552 6671190	327.96	4.5	59000	29000	18000	470	470	1800	8.7	0	0	5700	0	0)	6.6	0.026	0			0	0	0.32	0	0.4	0		0.11	0	1	0.079		0	15	0	0		0	0	0.45	
2015 NWB01 575552 6671190			58000			460	450	1800	7.5	0	0	5700	0	0)	6.6	0.02	0			0	0	0	0	0.5	0		0	0	0.96	0.023		0	15	0	0		0	0	0	
2015 NWB02 575363 6670210		4.0	66000	35000		490	440	2000	10	0	0	6500	0	0)	7.2		0			0	0	0	0.024	0.4	0		0.089	0	1.1	0		0	15	0	0		0	0	0.35	
2015 NWB02 575363 6670210	345.80	4.1	65000	34000	20000	490	440	2000	9.4	0	0	6300	0	0) —	6.9	0.023	0			0	0	0	0	0.5	0		0	0	1.1	0	1	0	12	0	0		0	0	0.34	

1

0 = Below limit of reporting

APPENDIX III CONSTRUCTION DETAILS AND PUMPING TEST PLOTS FOR PRODUCTION BORES NWB1 AND NWB2

OFFICE USE ONLY



Information to be provided on completion of a nonartesian well

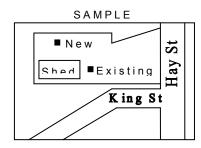
Information to be provided to the Department of Water under the *Water Agencies (Powers) Act 1984* and Section 26E of the *Rights in Water and Irrigation Act 1914* and Regulation 39 of the *Rights in Water and Irrigation Regulations 2000*

Please note:

- All information is to be written clearly and in block letters.
- If insufficient room please use a separate piece of paper.
- It is the responsibility of the person carrying out the works to fill out this form.

art 1: Details of any l	icence granted	for the wor	rk under the <i>Right</i>	s in Water And Irriga	tion Act 1914	section 26D
Licence number	CAW					
Licensee's full	☐ Individ	lual	Company			
art 2: Details of pers	on carrying out	the works				
	Company					
	Driller					
	ence number n-mandatory)			Driller classificat (non-mandato	-	
Po	stal address					
	Telephone			Facsin	nile	
	Email				<u> </u>	
rt 3: Location of we	II					
26D licence will list the emises on which well estruction is to occur.	Property addre	ss of well	or other tenure de	tails		
ne physical address of well is different from						
property address ed on the licence, stact the Department of tter prior to the	Zone I	asting/ atitude	Well c	Northing/ longitude	S reading	☐ Estimate
nmencement of istruction.	(e.g. GDA94/V	Datum VGS84)		GPS reliability		

Location plan – in the box below please sketch a plan showing position of well in relation to building, boundaries, road, nearest cross road and any additional information to assist in locating the well.



In the box to the right, please sketch a plan showing:

- location of all wetlands / watercourses / wells / soaks (existing and proposed).
- major improvements (house, large sheds etc).
- shaded sections to indicate areas under development.



Part 4: C	onstructi	ion details	(All measurem	nents are	to be take	n from ground level)
	F	Production	casing detail			Please complete well construction diagram in box provided
	Nomina	Diamete	r Wall	De	epth	below. If insufficient room please attach on separate piece of paper.
Material	bore	O.D (mm)	thickness (mm)	From (m)	To (m)	
	•	Compan		•	•	
Screens/s (type)		Diameter O.D (mm)	Aperture (mm)	Top of screen (m)	Bottom of screen (m)	
		Gravel pa	ck details			
Gravel size	(mm) 1.6		From (m)	То	(m)	
		Annul	ar fill			
Material t	ype		From (m)	T	o (m)	
		Cementi	ng detail			-]
Casing d		re cement		remmie		
Casing d (mm		Fre	om (m)	To (m)	
<u> </u>						
Total depti (from grour			Geophysica as conditio	ıl log requ n of licen	uired [Geophysical log taken?] Yes □ No (attach log and contractor □ Yes □ No details)
	From (n	n)	To (m)		Strata de	escription (If insufficient room attach on separate page)
1			I	1		

Part 5: Particular	s of well							
								1
	Well name / nu					<u></u>		
Drilling start date refers to the date drilling	Drilling	start			Drilling (completion		
begins. Do not include set up date.	Drilling method	used	Rotary air	☐ Cable	tool	Auger [] Rotary mu	d
Drilling completion date			Sludge	Other	(specify) _			
includes well development and testing.	Final status of	f well	Ready to oper	ate [] Decomn	nissioned		
			Other (specify))				
	Purpose (use) of	f well	Production Other (specify)	,	Investigat	tion	nitoring	
Part 6: Well deve	elopment		outer (opcomy)	/				
rait o. Well devi		d/mm/yy)				Duration of levelopment		hours
	Metho	od 🗆 A	Airlift	☐ Pump		Jetting	☐ Surgii	
				D	evelopme (e.g.	nt pump rate L/s, m³/day)		
Part 7: Pump tes	ting (If applicable)				, 0	, 3,		
	Date start (dd/mm/yy)		Date end (dd/mm/yy)			Duration o	of test	hours
		☐ Step	test 🗆	Constant	rate	Other		
	Constant rate - pump rate (e.g. m³/day)		ı	Pump typ	e (e.g sub	mersible)		
	iii /day/					rest level o test (m)		
	Measurements ta	ken from □	☐ top of casing	n (TOC)	-	d level (GL)		
	mododromonto ta	_	other (speci		· ·			
Final drawdown is the distance between the	Elevation of meas		☐ GPS	☐ Estin	nate			
static water level measured prior to the test	(metres AHD)	KIIOWII	other ((specify) _				
and the water level measured at the end of the pumping test.	Final drawdown	I	m Reco	ommende	d supply (e.g. m³/day)		
Part 8: Field sam	nlos							
rait o. Field Sall	-							
Specify unit measurements.	Collection method (e.g	. pump test airlift						
	Conductivity (e.g. mS/m)				re compens		pl	1
	Water temperature			,				
	at test							
Comments								
Part 9: Lab samp	oles							
Lab samples taken (Please attach)	☐ Yes T	DS (e.g. mg	ı/I)					o form if not ssion deadline

m Water cut at
o of casing (TOC) ground level (GL)
ner (specify)
ork
tary of a corporation that carried out the wor
of person making declaration) declare that the informa
of

Important information

- All information must be completed on the form unless otherwise indicated as optional for example; provision of
 the drillers licence number and classification fields are not mandatory and can be filled in at the drillers
 discretion. Provision of non-mandatory details would greatly assist the department in completion of its data set.
- Failure to complete all mandatory details and to submit the form to the department is an offence under the Rights in Water and Irrigation Act 1914.
- Under section 26E and regulation 39 within 1 month of completion of the construction of or deepening of the well, the person carrying out the work for a 26D licence must submit this form.
- Non-artesian wells in proclaimed areas require a licence unless exempted under the *Rights in Water and Irrigation Exemption (S26C) Order 2007.*

Where and how to submit this form

This form can be submitted by fax, post or in person to the appropriate Department of Water regional office. For assistance in completing this form contact your regional office.

Kimberley Region

Kununurra Regional Office 27 Victoria Hwy Kununurra WA 6743 Tel: 08 9166 4100 Fax: 08 9168 3174 PO Box 625 Kununurra WA 6743

Dort 40. Water levels

Midwest Gascoyne Region

Geraldton Regional Office 94 Sandford Street Geraldton WA 6531 Tel: 08 9965 7400 Fax: 08 9964 5983 Po Box 81 Geraldton WA 6531

Carnarvon

Carnarvon District Office 211 Robinson Street Carnarvon WA 6701 Tel: 08 9941 6100 Fax: 08 9941 4931 PO Box 81 Carnarvon WA 6701

Kwinana Peel Region

Mandurah Regional Office 107 Breakwater Parade Mandurah WA 6210 Tel: 08 9550 4222 Fax: 08 9581 4560 PO Box 332 Mandurah WA 6210

South West Region

Bunbury Regional Office 35-39 McCombe Road Bunbury WA 6230 Tel: 08 9726 4111 Fax: 08 9726 4100 PO Box 261 Bunbury WA 6231

Busselton

Busselton District Office Suite 2, 72 Duchess Street Busselton WA 6280 Tel: 08 9781 0188 Fax: 08 9754 4335 PO Box 269 Busselton WA 6280

South Coast Region

Albany Regional Office 5 Bevan Street Albany WA 6330 Tel: 08 9842 5760 Fax: 08 9842 1204 PO Box 525 Albany WA 6331

Pilbara Region

Karratha Regional Office Lot 4608 Cherratta Road Karratha Industrial Estate Karratha WA 6714 Tel: 08 9144 2000 Fax: 08 9144 2610 PO Box 836 Karratha WA 6714

Swan Avon Region

Victoria Park Regional Office 7 Ellam Street Victoria Park WA 6100 Tel: 08 6250 8000 Fax: 08 6250 8050

Warren Blackwood District

Manjimup Regional Office 52 Bath Street Manjimup WA 6528 Tel: 08 9771 1878 Fax: 08 9771 4335

Please retain a copy of this form for your records



Information to be provided on completion of a nonartesian well

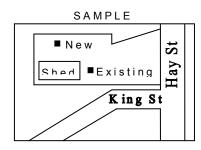
Information to be provided to the Department of Water under the *Water Agencies (Powers) Act 1984* and Section 26E of the *Rights in Water and Irrigation Act 1914* and Regulation 39 of the *Rights in Water and Irrigation Regulations 2000*

Please note:

- All information is to be written clearly and in block letters.
- If insufficient room please use a separate piece of paper.
- It is the responsibility of the person carrying out the works to fill out this form.

	,		, ,		
Part 1: Details of any	licence grante	for the wo	ork under the <i>Right</i> s	s in Water And Irrigation	Act 1914 section 26D
Licence number	CAW				
	☐ Indiv	ridual	Company		
Licensee's fu	II name				
Part 2: Details of per	son carrying ou	t the works	;		
	Company				
	Driller				
	cence number on-mandatory)			Driller classification (non-mandatory)	
F	ostal address -				
	Telephone			Facsimile	
	Email				
Part 3: Location of w	ell				
A 26D licence will list the premises on which well construction is to occur.	Property add	ess of well	l or other tenure det	ails	
If the physical address of the well is different from			Woll or	ordinates	ading ☐ Estimate
the property address listed on the licence, contact the Department of Water prior to the	Zone	Easting/ latitude	Well Co	Northing/ longitude	adding Estimate
commencement of construction.	(e.g. GDA94	Datum /WGS84)		GPS reliability	
andian plant in the base	اء ء مومام سامام	otob o nlow	ahawina naaitian a	fuell in volation to build:	ng boundaries road poerset

Location plan – in the box below please sketch a plan showing position of well in relation to building, boundaries, road, nearest cross road and any additional information to assist in locating the well.



In the box to the right, please sketch a plan showing: - location of all wetlands / watercourses / wells / soaks

- location of all wetlands / watercourses / wells / soaks (existing and proposed).
- major improvements (house, large sheds etc).
- shaded sections to indicate areas under development.



Part 4: C	onstructi	ion details	(All measurem	nents are	to be take	n from ground level)
	F	Production	casing detail			Please complete well construction diagram in box provided
	Nomina	Diamete	r Wall	De	epth	below. If insufficient room please attach on separate piece of paper.
Material	bore	O.D (mm)	thickness (mm)	From (m)	To (m)	
	•	Compan		•	•	
Screens/s (type)		Diameter O.D (mm)	Aperture (mm)	Top of screen (m)	Bottom of screen (m)	
		Gravel pa	ck details			
Gravel size	(mm) 1.6		From (m)	То	(m)	
		Annul	ar fill			
Material t	ype		From (m)	T	o (m)	
		Cementi	ng detail			-]
Casing d		re cement		remmie		
Casing d (mm		Fre	om (m)	To (m)	
<u> </u>						
Total depti (from grour			Geophysica as conditio	ıl log requ n of licen	uired [Geophysical log taken?] Yes □ No (attach log and contractor □ Yes □ No details)
	From (n	n)	To (m)		Strata de	escription (If insufficient room attach on separate page)
1			I	1		

Part 5: Particular	s of well								
	Well name / nu	<u></u>					-		
Drilling start date refers to the date drilling	Drilling	start			Drilli	ing completion			
begins. Do not include set up date. Drilling completion date	Drilling method used		Rotary air Cable tool Auger Rotary mud						
			Sludge Other (specify)						
includes well development and testing.	Final status of well		Ready to o	perate	☐ Deco	ommissioned			
			Other (specify)						
	Purpose (use) o	of well	☐ Production ☐ Investigation ☐ Monitoring ☐ Other (specify)						
Part 6: Well deve	elopment		1 Other (open	y/					
rait o. Well deve	-	ld/mm/yy)				Duration o			hours
	Meth	od 🗌	Airlift	☐ Pur	np	☐ Jetting	.t ☐ Su	rging	
					Develop	oment pump rat e.g. L/s, m³/da	te V)		
Part 7: Pump tes	ting (If applicable)						-		
	Date start (dd/mm/yy)		Date end (dd/mm/y			Duration	of test		hours
		☐ Step	test	☐ Consta	nt rate	Other			
	Constant rate - pump rate (e.g. m³/day)			Pump ty	ype (e.g	submersible)			
	iii /day)					ater rest level for to test (m)			
	Measurements ta	aken from	☐ top of cas	sina (TOC)	-	ound level (GL)			
			other (sp		•				
Final drawdown is the distance between the	Elevation of meas		☐ GP	S 🗌 Est	timate				
static water level measured prior to the test	(metres AHD)	riiowii	other (specify)						
and the water level measured at the end of the pumping test.	Final drawdown	ļ.	m Ro	Recommended supply (e.g. m³/day)					
Comments									
Part 8: Field sam	•								
Specify unit measurements.	Collection method (e.g	g. pump te airli							
	Conductivity (e.g. mS/m)			☐ Temperature compensated ☐ Temperature uncompensated			рН		
	Water temperature								
	at test								
Comments									
Dart 0: Lab come	Nos	·····	·····	·····					
Part 9: Lab samp									
Lab samples taken (Please attach)	☐ Yes ☐ No	ΓDS (e.g. m	ng/l)			bmit samples before the 1 m			

m Water cut at ☐ top of casing (TOC) ☐ ground level (GL)				
top of casing (TOC) ground level (GL)				
n other (specify)				
he work				
secretary of a corporation that carried out the work.				
name of person making declaration) declare that the information				
name				

Important information

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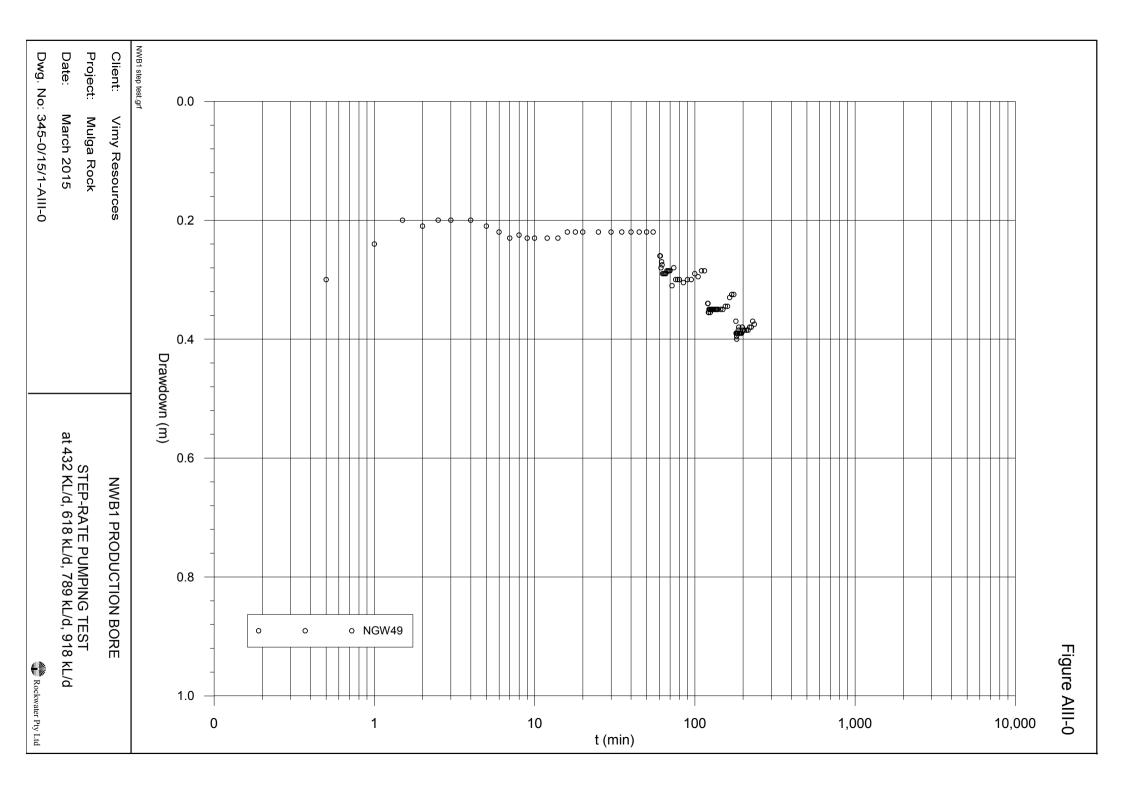
Swan Avon Region

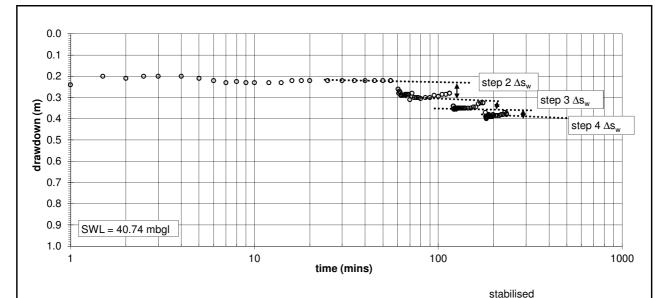
Victoria Park Regional Office 7 Ellam Street Victoria Park WA 6100 Tel: 08 6250 8000 Fax: 08 6250 8050

Warren Blackwood District

Manjimup Regional Office 52 Bath Street Manjimup WA 6528 Tel: 08 9771 1878 Fax: 08 9771 4335

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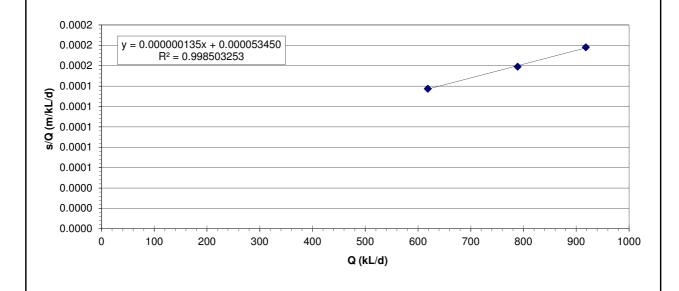


s=BQ+CQ², where:
BQ is drawdown due to laminar flow
CQ² is drawdown due to turbulent flow
s/Q=B+CQ, so in plot of s/Q v. Q, B is the intercept
& C is the slope

B = 5.3E-05 intercept C = 1.4E-07 slope

	Step	(Q	drawdo	s/Q		
		L/s	L/s kL/d		total (m)	m/kL/d	
•	1						
	2	7.16	618.62	0.085	0.085	0.00014	
	3	9.13	788.83	0.041	0.126	0.00016	
	4	10.63	918.43	0.038	0.164	0.00018	

predicted drawdown using B & C @ Q=14 L/s, = 0.26 m actual drawdown from CRT @ t=1320 mins & Q=14 L/s, = 0.49 m



Drawdown due to turbulent flow in aquifer and bore (Lt) $Lt=(CQ^2/(BQ+CQ^2))100$

Lt = 52.2 % at Q = 5 L/s Lt = 61.0 % at Q = 7 L/s Lt = 66.6 % at Q = 9 L/s Lt = 69.9 % at Q = 11 L/s

345.0\Data\Pumping Tests\step test - NWB3 Analysis.xls

Client: Vimy Resources

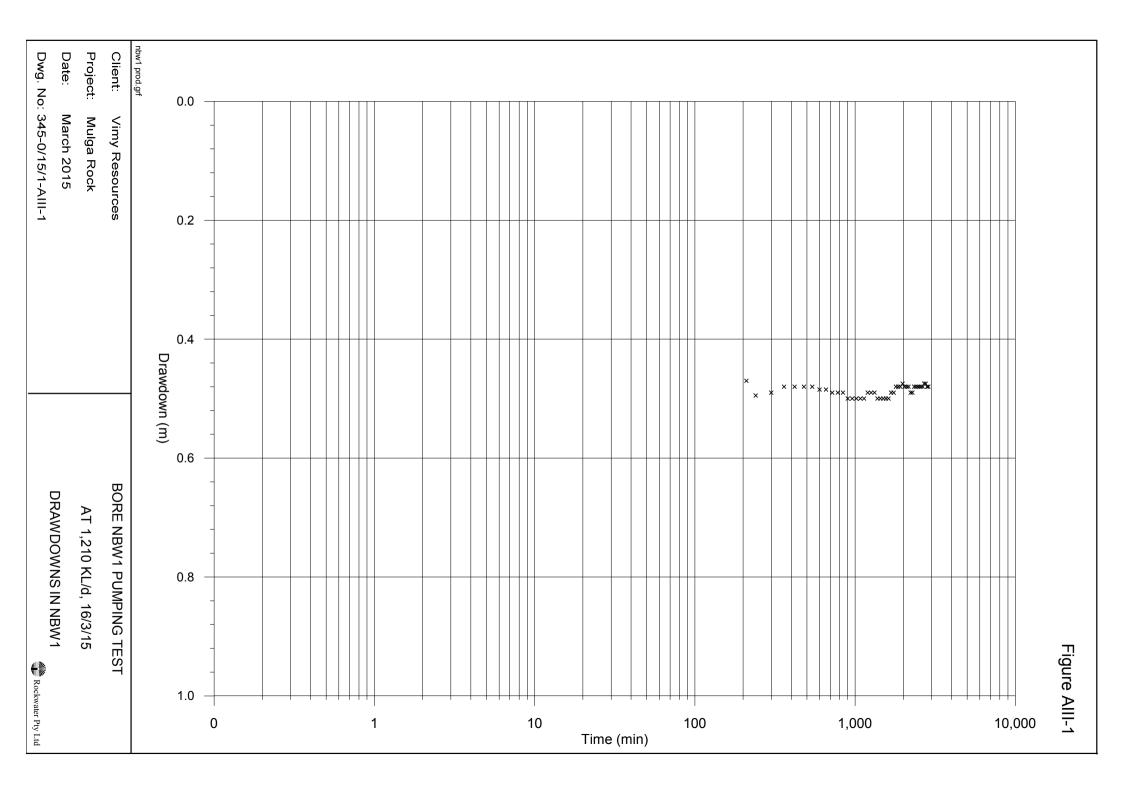
Project: 345-0

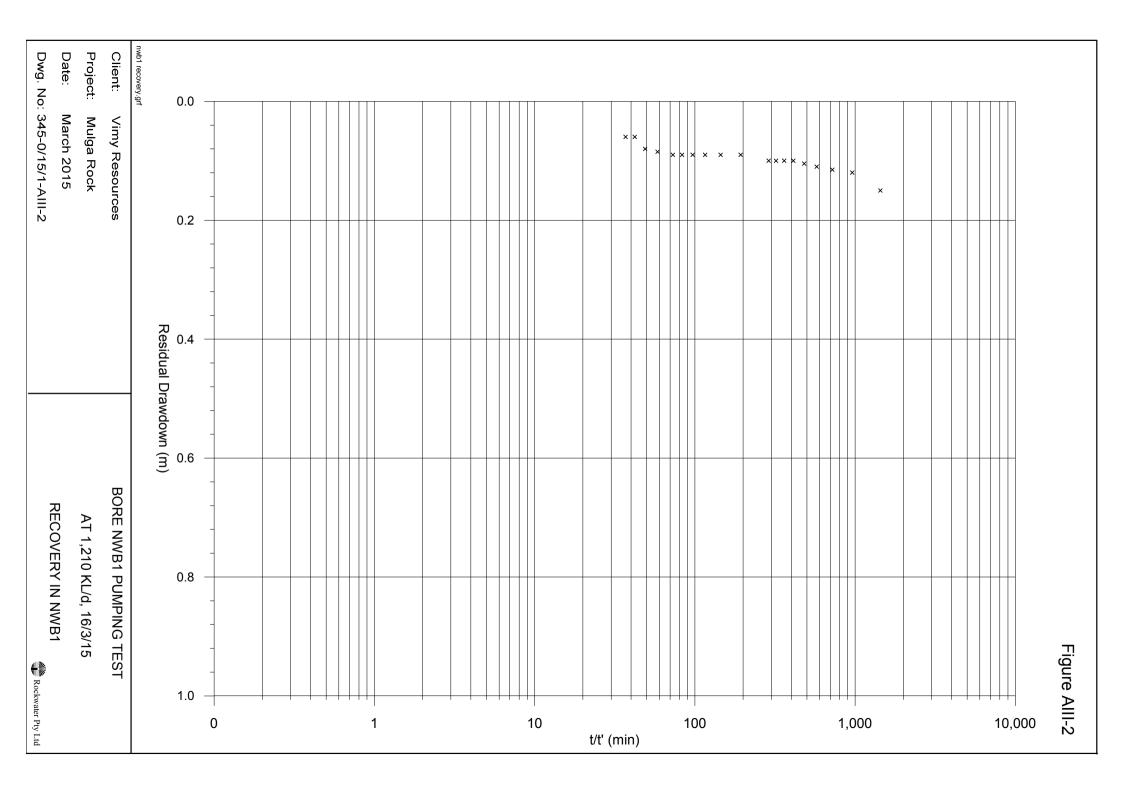
Date March 2015

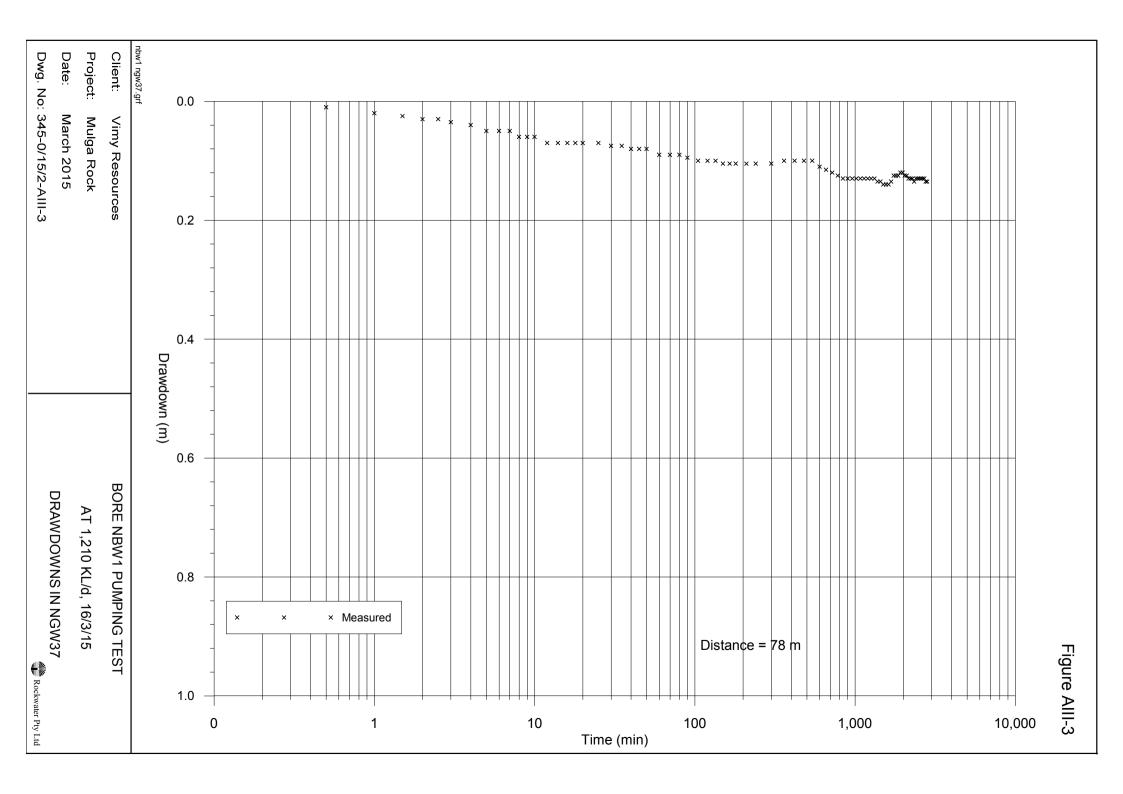
Dwg No. 345-0/15/1-AIII-0A

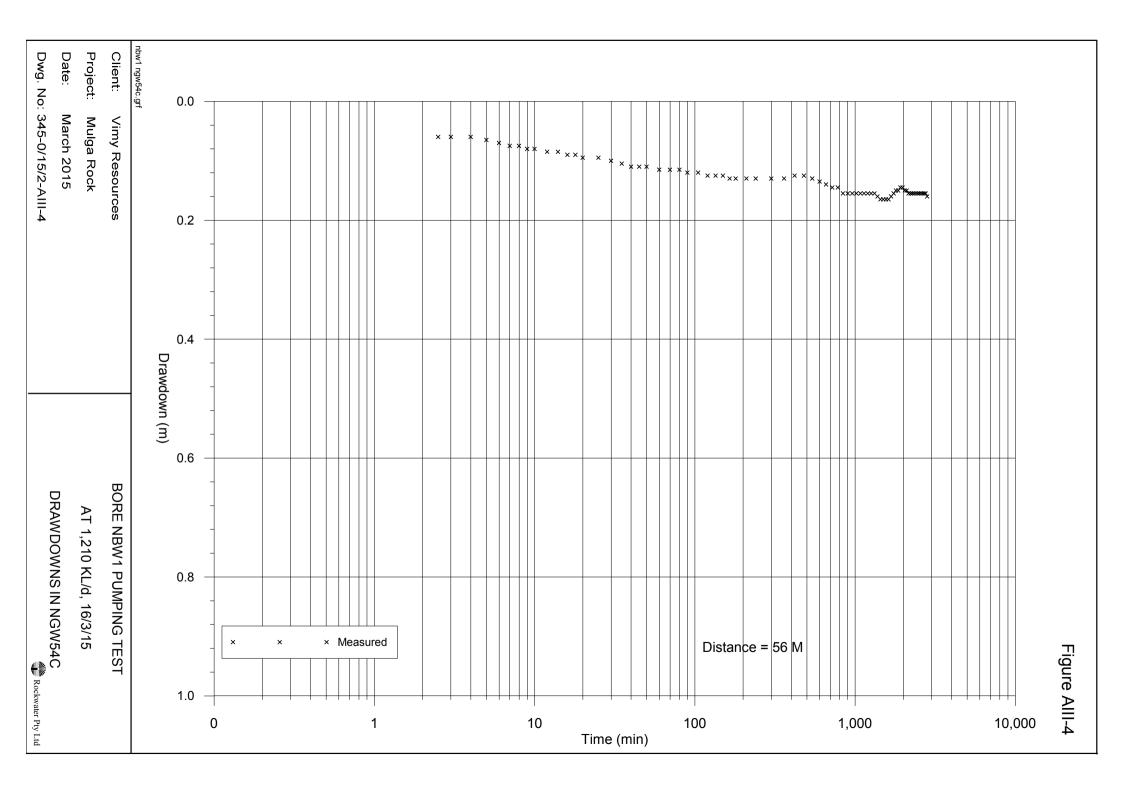
Bore NWB1 Step-rate Test Data with Analysis of Turbulent Flow

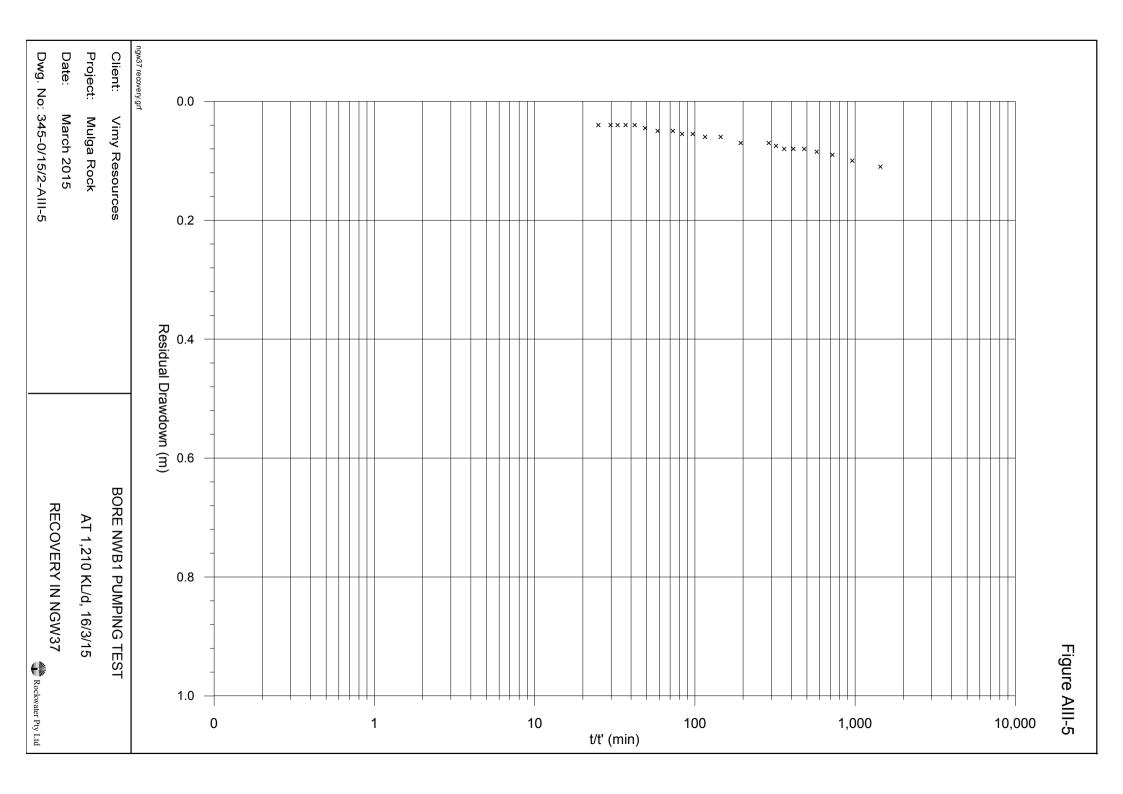


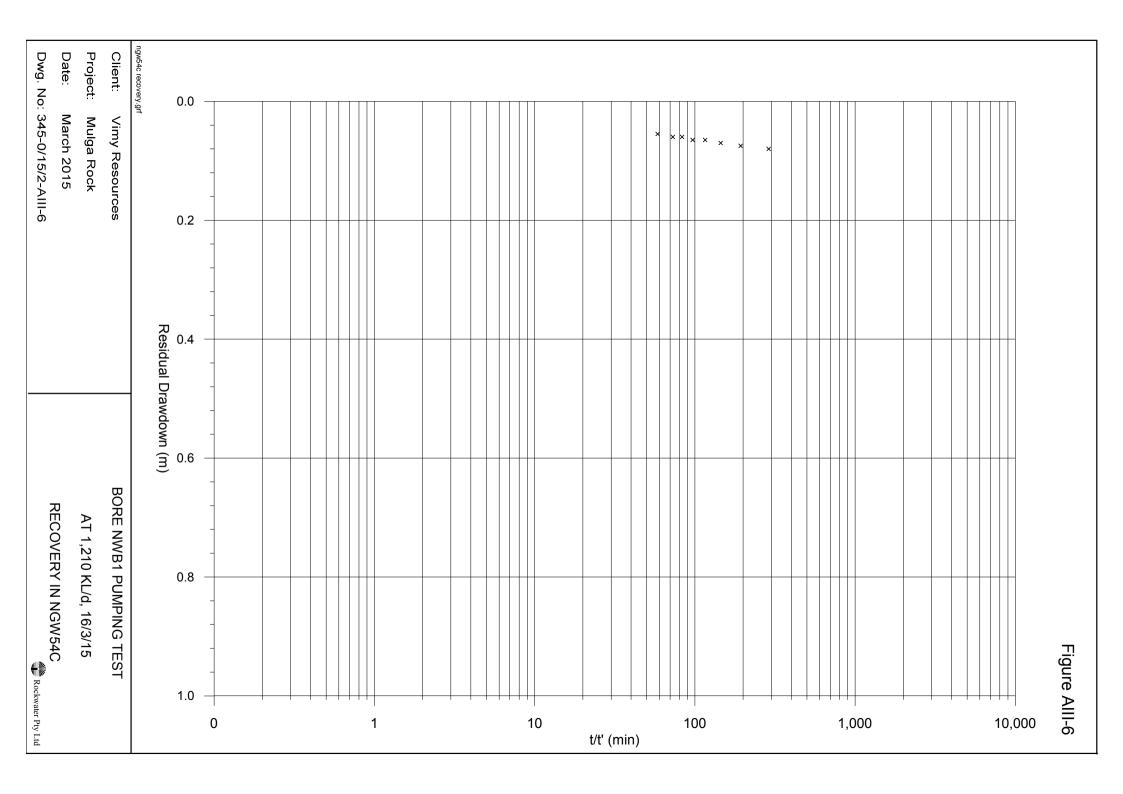


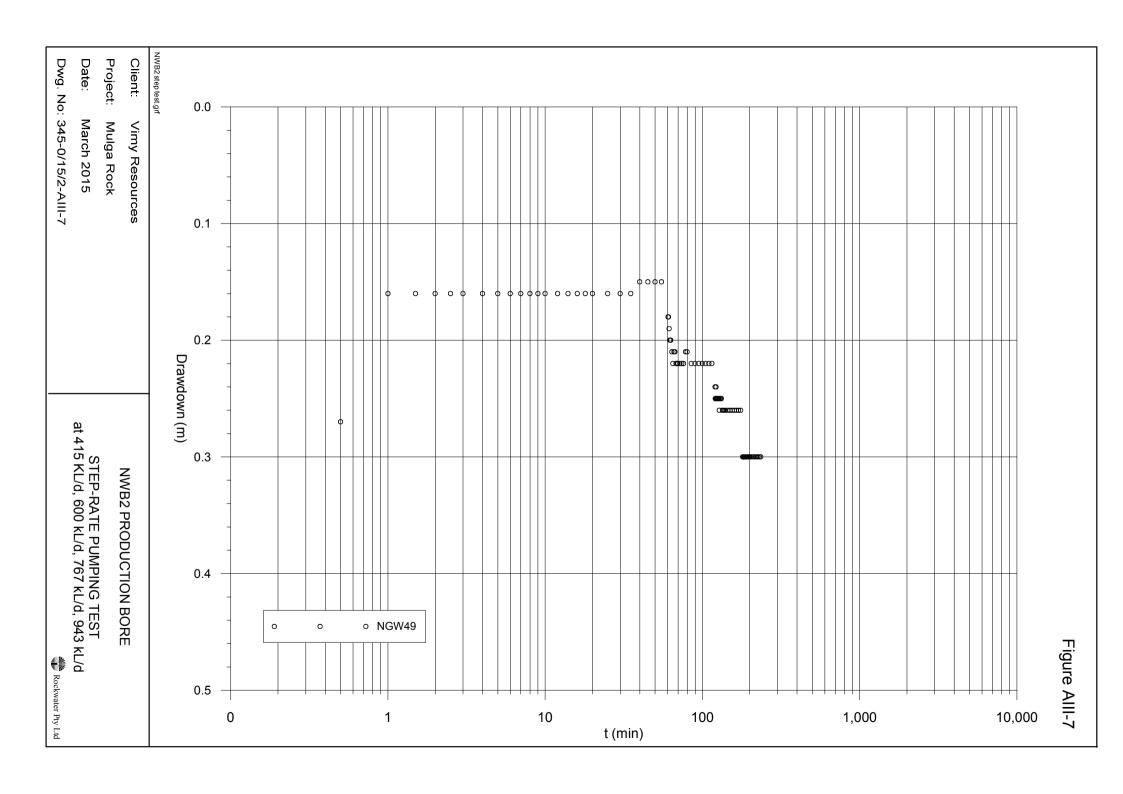


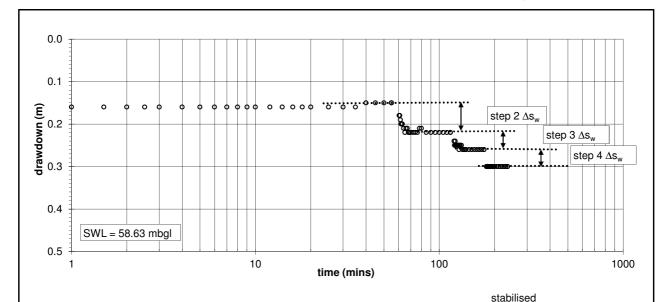












s=BQ+CQ2, where: BQ is drawdown due to laminar flow CQ2 is drawdown due to turbulent flow s/Q=B+CQ, so in plot of s/Q v. Q, B is the intercept & C is the slope

B =

0.00012 2 6.94 599.62 0.070 0.070 0.00014 3 8.88 767.23 0.040 0.110 0.00016 4.5E-05 intercept 4 10.91 942.62 0.040 0.150 1.2E-07 slope

Step

1

Q

kL/d

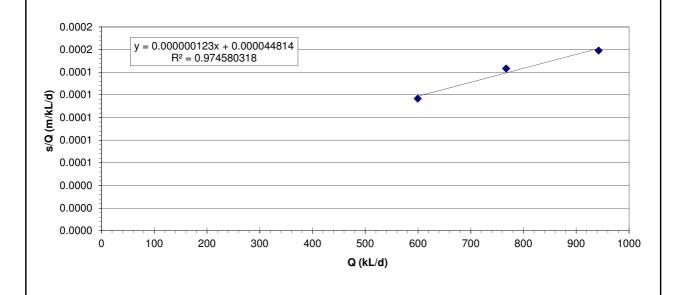
drawdown (s)

 Δs_w (m) total (m)

s/Q

m/kL/d

predicted drawdown using B & C @ Q=11 L/s, = 0.15 m actual drawdown from CRT @ t=2873 mins & Q=11 L/s, = 0.32 m



Drawdown due to turbulent flow in aquifer and bore (Lt) $Lt = (CQ^2/(BQ+CQ^2))100$

Lt = 49.2 % at Q = 4 L/s

Lt = 62.3 % at Q = 7 L/s

% at Q = 9 L/sLt = 67.9 % at Q = 11 L/s

345.0\Data\Pumping Tests\step test - NWB2 Analysis.xls

Client: Vimy Resources

345-0 Project: Date March 2015 Dwg No. 345-0/15/1-AIII-7A Bore NWB2 Step-rate Test Data with Analysis of Turbulent Flow



